

DIRECT CONTROL OF D-STATCOM BASED ON 23-LEVEL CASCADED
MULTILEVEL INVERTER USING HARMONICS ELIMINATION PULSE
WIDTH MODULATION

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*This thesis is first dedicated to my beloved, patient and struggling mother, **Huda Abdul-Raheem**. She has always been in the forefront of love, concern, Dua'a, advice and guidance to make sure we achieve the best of both worlds. May Allah preserve her in goodness and grant her happiness in both worlds. It is also dedicated to my wise and patient father, **Dr. Majed Ahmed**. This thesis is a testimony to his effort of how he advised, prayed and struggled for us to get the best things of both worlds. May Allah grant him happiness in both worlds. Also dedicated to my only sister, **Shaima'a**, the new baby gifted and bestowed to us by Allah while I was in the second semester of my Master-degree. Also dedicated to my 'treasure' beloved future wife, **Bushra**, for here patience and understanding. May Allah preserve her in goodness. To my lovely brothers, **Muhammad** and **Ehap**. I will never forget their support, encouragement, and understanding. They have released me from all family responsibilities just to come up with this thesis. Finally, to the brother from another mother, **Dr. Suleiman Zubair**. He has been a supporting pillar of encouragement and motivation throughout the work of this thesis. May Allah preserve them in goodness and give all, the best of this world and in the hereafter.*

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$\alpha_1, \alpha_2 \dots \alpha_N$	–	HEPWM switching angles
ε	–	Voltage drop coefficient
η	–	Ripple current coefficient
I_{RMS}	–	Rated RMS current
f_{sw}	–	Switching frequency
f	–	Fundamental frequency in Hz
ω	–	System frequency in rad/s
C_{dc}	–	dc capacitance for each H-bridge unit
V_{DC}	–	dc voltage across capacitors in each H-bridge unit
U_{DC}	–	Input dc voltage per phase
V_I	–	Voltage magnitude of the fundamental component
i_{Cq}^*	–	Reference reactive current
i_{CLL}	–	Line-to-line D-STATCOM current
V_{CLL}	–	Line-to-line output voltage of D-STATCOM
R_S	–	Source resistance
X_S	–	Source inductance
Z_S	–	Source impedance

CHAPTER 1

INTRODUCTION

1.1 Overview

Due to the depletion of fossil fuel resources and the environmental contamination by green-house gases, the utilization of renewable energy (RE) has been on a constant rise. It is envisaged that RE will play an important role in the future energy mix [1]. For instance, by 2020, it is expected that 12% of the world's electricity will be produced by RE [2]. Furthermore, the global awareness is increasing in many countries, while international communities are promoting the climate-friendly and clean energy sources. These concerns are reflected in the recent 21st Conference of Parties (COP21) on climate change which was held in Paris [3]. However, RE resources are naturally unstable and highly intermittent. The inter-connection of RE sources with various kinds of loads have imposed serious power quality (P-Q) issues to the electrical grid. The most common P-Q problems are the voltage sag, swell and harmonics [4]. This is more severe with the proliferation of loads that draw non-sinusoidal current.

Rapid development in power electronics and control offers P-Q improvement using flexible AC transmission system (FACTS) controllers [5]. At the electrical distribution level, the D-STATCOM, which is in the family of FACTS devices, has been frequently used for power factor correction, load balancing, voltage regulation and stabilization. These functions are achieved by means of the reactive power compensation [6-8]. Traditionally, the low cost, two-level voltage source inverter (VSI) with a series coupling inductor, is used as the main building block of the D-STATCOM [9, 10]. However, the output voltage of the VSI is characterized by high

harmonics that require bulky and costly filtering. Furthermore, for high and medium voltage interconnections, it is mandatory to use the line frequency (50 Hz) step-up transformer to match the output voltage of the VSI to the utility grid. This increases the cost, size, weight and power losses of the overall D-STATCOM. Thus, the multilevel VSI (MVSI) is being exploited to replace the two-level VSI [11-13].

Since the MVSI is sufficiently capable of providing high voltage, the use of step-up transformer can be avoided [14-16]. As a result, the weight and cost of the hardware are reduced significantly. For example, with the absence of the transformer, the weight of 3-phase cascaded MVSI, rated at 6.6 kV/1 MVA can be reduced three to four times compared to its transformer counterpart [14, 17]. In [17], it is reported that the transformer and its ac inductor is about half of a 360 kVA D-STATCOM weight. Additionally, the efficiency of the system can be increased; in a typical D-STATCOM system, approximately 70% of overall power loss per MVA rating is attributed to the transformer [16].

For a proper exchange of reactive power with the electrical grid, an efficient control of the D-STATCOM is crucial [8]. Two approaches, namely the direct and indirect control are widely used [18-21]. For the former, the phase angle of the VSI output voltage (δ) is the control variable, while the modulation index (M_I) is held constant at maximum value. Thus, the output voltage distortion (reflected by the THD value) can be kept minimum by imposing the maximum value of M_I . However, a rapid adjustment of reactive power is unachievable since the output voltage control using δ is restricted by the time constants of the capacitor charging and discharging within the VSI.

This speed limitation is addressed by the direct control approach [15, 20, 22]. In this scheme, the capacitor voltages are fixed, while the control of reactive power is obtained by varying the amplitude of the VSI output voltage. The rapid response to the reactive power demand is achieved by changing the M_I of the pulse width modulation (PWM) switching scheme [20]. Despite the improved performance, two problems are inherent for the direct control. First, the THD changes with the variation of M_I . At low

M_I , the harmonics profile of the output voltage is poor. Second, the high switching frequency of the PWM scheme increases the losses of the D-STATCOM [12].

The most popular modulation technique is the phase shifted PWM (PS-PWM) [23-25]. The concept is similar to the conventional sinusoidal PWM, whereby the switching pulses are generated by comparing a modulating and multiple carrier signals [16, 25]. For the MVSI topology, the PS-PWM switching is very complex due to the number of carriers that need to be phase-shifted in the correct sequence. For instance, to trigger the switches of a 3-phase 15-level MVSI, 29 carrier signals are required. In addition, the PS-PWM cannot directly eliminate the harmonics; thus it needs to be operated with high switching frequency to maintain the THD below the IEEE-519 Standard (5%). Another modulation method that is used in the direct control of the D-STATCOM is the space vector modulation (SVM) [26, 27]. The scheme is based on vector calculation and switching states selection to achieve certain desired performance [27]. Despite the comparatively lower switching frequency that can be attained, the process of selecting switching states becomes increasingly complicated as the level of MVSI becomes higher [16].

On the other hand, the harmonic elimination PWM (HEPWM) [22, 28] is known for its superior harmonics profile and lower switching losses. Despite being an off-line technique (i.e. the angles are computed prior to execution and stored in a look-up table), it is becoming a popular choice, particularly for high power applications. The difficulty of storing the angles in look-up table does not arise due to availability of low-cost memories. Therefore, HEPWM is a competitive alternative for the direct control scheme of the D-STATCOM especially when the MVSI topology is utilized. However, to implement HEPWM for high output voltage, a wide range of M_I is necessary which in turn, requires more switching angles to be obtained. This is where the challenge in HEPWM is noted. The problem that arises in solving for the HEPWM angles for a wide M_I range is due to the large number of non-linear transcendental equations that govern them [23, 29]. In spite of this, several works that utilize HEPWM for direct control albeit for a lower number of angles, are reported [16, 21, 22, 30]. For example, a direct control scheme based HEPWM technique was proposed in [22] for 10 MVar /12 kV, 11-level (five angles) MVSI. In [30], authors presented a HEPWM

strategy to minimize the THD of the output voltage of MVSI D-STATCOM. Furthermore, dc-dc converters have been used with HEPWM technique to control output voltage of single-phase five-level cascaded D-STATCOM [16]. However, in these methods [22, 30], the M_l values are calculated for a maximum levels of 11-levels and for limited operation range; and for [16], a dc-dc converter is used for each H-bridge to produce a controllable dc input voltage, resulting in a complex and bulky system especially for high levels MVSI.

Understandably, due to the complexity in solving the equations for the HEPWM angles, no work is reported on the direct control for a MVSI D-STATCOM for more than 15-level. However, even with the 15-level, it is not possible to achieve the desired THD values below 5% over the entire modulation range. Thus, one of the objectives of this work is to increase the MVSI level in order to produce wider M_l range, while keeping the THD below the desired value.

1.2 Motivation

From the above overview, it is clear that the direct control strategy is favored for D-STATCOM due to its ability to compensate for the reactive power rapidly. Commonly, PS-PWM switching is used in the direct control of the MVSI D-STATCOM. However, to obtain a low THD of the output voltage of the D-STATCOM, the PS-PWM needs to be operated at high switching frequency. This results in high switching losses, hence lower efficiency. To overcome these limitations, the direct control scheme based on HEPWM is proposed. The main advantage of using HEPWM is the low THD; using a sufficiently high level MVSI, the THD below 5% over the entire operating range can be achieved. Furthermore, due to the lower switching frequency, HEPWM exhibits much lower switching loss compared to PS-PWM. In addition, for the available rating of power semiconductor switches, it is not difficult to realize D-STATCOM for direct connection to 11 kV distribution network (or higher voltage) using MVSI. This eliminates the bulky and lossy step-up transformer.

1.3 Objectives of the Research

By considering the aforementioned background and motivation, the objectives of this research are formulated as follows:

- i) to propose a direct control scheme, which is based on HEPWM switching for 23-level MVSI D-STATCOM.
- ii) to evaluate the performance of the proposed control scheme in terms of harmonics and power losses against the PS-PWM methods.
- iii) to test the dynamic performance of the HEPWM based D-STATCOM under sag and swell problems.

The HEPWM angles are computed using a soft computing method, known as the differential evolution (DE). It is a powerful search and optimization method used to solve highly correlated and complicated non-linear problems. For validation, a ± 6.5 MVA_r/11 kV D-STATCOM system, modelled in Simulink and PLECS software is used.

1.4 Scope of the Research

The scope and limitations of this research are as follows:

- i) The angles trajectories are computed offline for wide range of M_I using DE.

To ensure that the THD is kept below 5%, a 23-level MVSI is required, which in turn, requires the number of HEPWM angles to be increased to eleven. The maximum achievable range of M_I is $5.40 \leq M_I \leq 8.15$ (i.e. HEPWM allows over modulation operation), with an incremental step of 0.01. The 0.01 step for M_I can be considered very accurate; it gives a total of 273 values for the given range of M_I .

- ii) The voltages across the capacitors are fixed by using floating dc sources.

In a normal STATCOM, a capacitor bank is used to maintain the dc voltage of the VSI. For cascaded multilevel VSI, the number of the capacitors is proportional to the number of the synthesized levels. Due to different losses of H-bridge units, measurement error in the voltage and current sensors and the tolerance of the passive elements, the capacitor voltages may be unbalanced. Improper balancing among the capacitors affects the operation of the HEPWM method. In this work, for simplicity, the capacitor voltages are kept constant using floating dc sources similar to [31].

- iii) Simulation using Simulink/Matlab and PLECS software.

To validate the effectiveness of the proposed control scheme, the D-STATCOM is modelled in Simulink/MATLAB. The pre-calculated switching angles are stored in look-up table. In addition, the PLECS software (which is integrated with Simulink) is used for the calculation of the thermal losses.

- iv) Performance validation: comparison between HEPWM and PS-PWM

To validate the performance of the proposed HEPWM switching, a comparison is made with PS-PWM for the same 23-level MVSI D-STATCOM was steady state. In addition, the dynamics performance of the HEPWM based direct control is tested under sag and swell problems.

1.5 Significance of the Research

The advantages of the proposed HEPWM D-STATCOM can be summarized as:

- i) Fast reactive power compensation.

The utilization of direct control scheme instead of the indirect control scheme allows for fast compensation of the reactive power [9, 18]. The control

of reactive power is achieved by using HEPWM switching to vary the amplitude of the VSI output voltage using M_I .

- ii) Superior harmonic performance and low switching losses.

The proposed HEPWM switching for 23-level MVSI D-STATCOM allows the elimination of the lower order and the triplens harmonics from the line-to-line output voltage. Thus, very low THD of the output voltage waveform is obtained. In addition, due to the low switching frequency of the HEPWM, lower switching loss results.

- iii) Reduction in the size and cost of the D-STATCOM.

This work presents a D-STATCOM based on 23-level cascaded MVSI which allow the elimination of the bulky and costly step up transformer used to connect the D-STATCOM to distribution level. In addition, due to the good harmonics performance of the output voltage of the proposed D-STATCOM, a smaller series-coupling inductor can be used, hence the lower size of the overall system.

1.6 Thesis Outline

The thesis is comprised of five chapters. The remaining chapters are organized as follows:

- i) Chapter 2 is a review on the topologies, control and modulation methods used for D-STATCOM. It provides the important background knowledge regarding the research. The chapter starts by comparing the STATCOM to the other types of FACTS devices. Then, the MVSI topologies, control strategies and modulation techniques utilized for STATCOM are presented alongside a comparative analysis between them. The common PWM methods (i.e. PS-PWM and HEPWM) used for the direct control of STATCOM are presented alongside a critical

discussion between them. It is shown that HEPWM is a competitive alternative for the direct control scheme of the D-STATCOM.

- ii) Chapter 3 begins by introducing the concept of a direct control scheme based on HEPWM switching for a 23-level MVSI D-STATCOM. Then a detailed outline of the design considerations and control of the proposed system is provided. The methods for solving the HEPWM equations, the formulation of HEPWM equations, the concept of DE and its application on solving the eleven switching angles (to achieve 5.40 – 8.15 p.u. M_I range) are discussed and the angles trajectories for 23-level MVSI are shown. In addition, the selection of the passive elements is explained alongside a discussion about its effect on the operation of the STATCOM. The simulation of the direct control based PS-PWM switching for 23-level MVSI D-STATCOM is also presented. For both systems (i.e. HEPWM and PS-PWM), the generation of the switching pulses is described in details.
- iii) Chapter 4 examines the performance of the HEPWM based direct control scheme alongside a detailed comparison with the traditional PS-PWM switching in steady state. Their performance is benchmarked using ± 6.5 MVar/11 kV D-STATCOM modelled in MATLAB-Simulink and PLECS software. Furthermore, dynamic performance of the proposed HEPWM D-STATCOM is tested under voltage sag and swell cases and a comparative discussion is made with the indirect control scheme.
- iv) Chapter 5 concludes the work and provides a suggestions and directions for the future work.

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