ACKNOWLEDGEMENT

I would like to express my utmost gratitude to my main supervisor Prof. Ir. Dr. Wahid Bin Omar for his invaluable support, guidance and encouragement throughout the period of research. My sincere appreciation to Assoc. Prof. Dr. Redzuan Bin Abdullah for his continuous help, guidance and constructive comments. I would also like to thank Assoc. Prof. Dr. Lee Yee Loon for his helpful suggestion and advice.

My special thanks and acknowledgement are dedicated to the following individuals who have contributed to the research at various stages. I wish to thank the technical staff of Material and Structural Engineering Laboratory, UTHM, especially Affendi, for his continuous assistance in the experimental work. My appreciation to Koh Heng Boon and my other colleagues for sharing their research experiences and views. I would also like to thank Hafsah Khamis, Norwirdawati and Mohd Faizal for their help during the casting and testing processes.

Finally, I am most grateful to my husband, Abdul Aziz Bin Abdul Samad, and our children, Anis, Akmal, Afiqah and Alia, for their support and encouragement during my study. Special dedication to my late parents, Habibah Binti Dahalan and Mohamad Bin Adnan, whose love has been my inspiration.
ABSTRACT

Affordable quality housing is vital in developing countries to meet its growing population. Development of a new cost effective system is crucial to fulfill these demands. In view of this, a study is carried out to develop a Precast Lightweight Foamed Concrete Sandwich Panel (PLFP), as a new affordable building system. Experimental investigation and finite element analysis to study the structural behaviour of the PLFP panel under axial load is undertaken. The panel consists of two foamed concrete wythes and a polystyrene insulation layer in between the wythes. The wythes are reinforced with high tensile steel bars and tied up to each other through the polystyrene layer by steel shear connectors bent at an angle of 45°. The panels are loaded with axial load until failure. The ultimate load carrying capacity, load-lateral deflection profile, strain distributions, and the failure mode are recorded. Partial composite behaviour is observed in all specimens when the cracking load is achieved. Finite element analysis is also carried out to study the effect of slenderness ratio and shear connectors which are the major parameters that affect the strength and behaviour of the panels. An empirical equation to predict the maximum load carrying capacity of the panels is proposed. The PLFP system proposed in this research is able to achieve the intended strength for use in low rise building. Considering its lightweight and precast construction method, it is feasible to be developed further as a competitive IBS building system.
Perumahan yang berkualiti dan mampu dimiliki adalah perlu untuk negara yang sedang membangun bagi menampung jumlah penduduk yang kian bertambah. Penghasilan sistem baru yang lebih ekonomi adalah sangat diperlukan bagi memenuhi keperluan ini. Oleh itu, kajian telah dijalankan bagi menghasilkan panel pratuang sanwic yang diperbuat dari konkrit berbusa foam (PLFP), sebagai sistem bangunan baru yang mampu dimiliki. Penyiasatan eksperimen dan analisis unsur terhingga bagi mengkaji kelakuan struktur panel PLFP yang dikenakan beban paksi telah dijalankan bagi tujuan ini. Panel ini terdiri daripada lapisan perangkap haba iaitu polisterin yang terletak diantara dua lapisan dinding konkrit berbusa foam. Lapisan dinding dikuatkan dengan besi bertegasan tinggi yang diikat kepada besi penyambung ricih yang dibengkokkan 45° dan merentasi lapisan polisterin. Panel dibebankan dengan beban paksi sehingga gagal. Keupayaan maksima menanggung beban, profil hubungan beban dan pesongan sisi, penyebaran keterikan dan mod kegagalan telah direkodkan. Kelakuan komposit separa dapat dilihat dalam semua spesimen apabila ia mula mengalami retakan. Analisis unsur terhingga dijalankan bagi menentukan pengaruh nisbah kelangsingan dan penyambung ricih yang merupakan parameter utama yang mempengaruhi kekuatan dan kelakuan panel. Persamaan empirikal diterbitkan bagi menentukan keupayaan menanggung beban maksima panel. Sistem panel PLFP yang dicadangkan dalam kajian ini mampu mencapai kekuatan yang diinginkan bagi kegunaan di dalam bangunan rendah. Memandangkan panel ini ringan dan menggunakan kaedah pembinaan pratuang, ia boleh dibangunkan lagi kerana ia berpotensi sebagai sistem bangunan IBS yang berdaya saing.
TABLE OF CONTENTS

CHAPTER                TITLE                                                   PAGE

DECLARATION           ii
ACKNOWLEDGEMENT      iii
ABSTRACT             iv
ABSTRAK               v
TABLE OF CONTENTS    vi
LIST OF TABLES       x
LIST OF FIGURES       xiii
LIST OF ABBREVIATIONS xxii
LIST OF SYMBOLS      xxiii
LIST OF APPENDICES   xxvi

1 INTRODUCTION
1.1 Construction Industry in Malaysia  1
1.2 Precast Concrete Building System  3
1.3 Precast Sandwich Panel            6
1.4 Lightweight Foamed Concrete       8
    1.4.1 Materials                      9
    1.4.2 Characteristic properties of foamed concrete    9
    1.4.3 Advantages of Foam Concrete        10
1.5 Precast Lightweight Foamed Concrete Sandwic
    Sandy Panel, PLFP                     11
1.6 Problem Statement                12
1.7 Objectives                      12
1.8 Scope of Work                   13
1.9 Thesis Layout                   14

2 LITERATURE REVIEW
2.1 Introduction                  16
2.2 Review of Past Studies on Sandwich Panel  19
2.2.1 Materials
2.2.2 Structural Behaviour of Sandwich Panel
2.2.3 Lightweight Sandwich Panel
2.4 Foamed Concrete Fabrication
2.5 Precast Concrete Sandwich Panel as Structural Wall Elements
2.6 Finite Element Analysis
2.7 Conclusion

3 EXPERIMENTAL PROGRAMME
3.1 Introduction
3.2 Preliminary Experimental Investigation
3.2.1 Materials and Fabrication of Test Specimens
3.2.2 Test Set-up and Procedure
3.2.3 Preliminary Experimental Results
3.2.4 Observations and Further Enhancements
3.2.5 Discussion
3.3 Actual Experimental Programme
3.3.1 Materials and Fabrication of Test Specimens
3.3.2 Test Set-up and Procedure
3.4 Conclusion

4 EXPERIMENTAL RESULTS AND ANALYSIS
4.1 Introduction
4.2 Objectives
4.3 Experimental Results
4.3.1 Ultimate Strength Capacity
4.3.2 Crack Pattern and Mode of Failure
4.3.3 Load-horizontal deflection Profile
4.3.4 Load-Strain Relationship
4.4 Conclusion

5 FINITE ELEMENT METHOD
5.1 Introduction
5.2 Objective
5.3 FEM Modeling
  5.3.1 Elements Used in FEM Modeling
  5.3.2 Material Model
5.4 Validation of the Finite Element Model
5.5 Parameters of Study
5.6 FEM Results
  5.6.1 Crack Pattern
  5.6.2 Load-lateral deflection Profiles
  5.6.3 Load-strain relationship
  5.6.4 Strain Distribution across Panel’s Thickness
  5.6.5 Optimum Diameters of Shear Truss Connectors
  5.6.6 Effects of Symmetrical Orientation of Shear Truss Connectors
  5.6.7 Effects of Various Heights and Overall Thickness of Panel
5.7 Conclusion

6 RESULTS AND DISCUSSION
6.1 Introduction
6.2 Lightweight Foamed Concrete Mixture For PLFP Panel with Strength of 17 MPa
6.3 PLFP Panel for Testing Under Axial Load
6.4 The effects of Slenderness Ratio
6.5 The effectiveness of shear connector and the extent of composite behaviour achieved
6.6 Suitability of PLFP Panel as Load Bearing Wall in Low Rise Building
6.7 Mathematical Modeling
6.8 Conclusion

7 SUMMARY, CONCLUSION AND RECOMMENDATIONS
7.1 Development of Precast Lightweight Foamed
Concrete Sandwich Panel (PLFP) 209

7.1.1 Summary of the Development and construction of the sandwich PLFP panel using the lightweight foamed concrete 209

7.1.2 Conclusion 210

7.2 Development of Foamed Concrete Material 211

7.2.1 Summary of finding the right mixture for foamed concrete of sufficient strength 211

7.2.2 Conclusion 212

7.3 Structural Behavior of the PLFP 212

7.3.1 Summary of the experiment and FEM analysis 213

7.3.2 Conclusion 213

7.4 Semi empirical expression to estimate the load carrying capacity of the PLFP panel 214

7.4.1 Summary on the determination of the new empirical equation 214

7.4.2 Conclusion 215

7.5 Recommendations 215

REFERENCES 217

APPENDICES A-H 224
# LIST OF TABLES

<table>
<thead>
<tr>
<th>TABLE NO.</th>
<th>TITLE</th>
<th>PAGE</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.1</td>
<td>Housing Targets from the Public and Private Sector, 2006 to 2010</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td>(Ministry of Housing and Local Government)</td>
<td></td>
</tr>
<tr>
<td>2.1</td>
<td>Measured Properties for FRC, PVC Foam and Balsa Core</td>
<td>23</td>
</tr>
<tr>
<td></td>
<td>(Stoll F. et al., 2004)</td>
<td></td>
</tr>
<tr>
<td>2.2</td>
<td>Crack and Failure Loads for Panel Specimens</td>
<td>31</td>
</tr>
<tr>
<td></td>
<td>(Benayoune et al., 2006)</td>
<td></td>
</tr>
<tr>
<td>2.3</td>
<td>Ultimate load and maximum deflection at mid-height in Panel Specimens</td>
<td>41</td>
</tr>
<tr>
<td></td>
<td>(Mohammed and Nasim, 2009)</td>
<td></td>
</tr>
<tr>
<td>2.4</td>
<td>Typical mix details for foamed concrete (BCA, 1994)</td>
<td>53</td>
</tr>
<tr>
<td>2.5</td>
<td>Typical Properties of Foamed Concrete (BCA, 1994)</td>
<td>54</td>
</tr>
<tr>
<td>2.6</td>
<td>Comparison of ultimate loads (Sulaiman et al., 2008)</td>
<td>60</td>
</tr>
<tr>
<td>3.1</td>
<td>Dimension and Properties of Pilot Test Specimens</td>
<td>70</td>
</tr>
<tr>
<td>3.2</td>
<td>Ratio of material and characteristic properties for trial mix</td>
<td>74</td>
</tr>
<tr>
<td>3.3</td>
<td>Foamed Concrete Properties</td>
<td>78</td>
</tr>
<tr>
<td>3.4</td>
<td>Properties of Steel</td>
<td>78</td>
</tr>
<tr>
<td>3.5</td>
<td>Ultimate Strength Results of Pilot Test Specimens</td>
<td>89</td>
</tr>
<tr>
<td>3.6</td>
<td>Foamed Concrete Properties for Panels PLFP-5 and PLFP-6</td>
<td>93</td>
</tr>
<tr>
<td>3.7</td>
<td>Ultimate Strength Results of PLFP-5 and PLFP-6</td>
<td>94</td>
</tr>
<tr>
<td>3.8</td>
<td>Dimensions and details of specimens for actual experimental programme</td>
<td>96</td>
</tr>
<tr>
<td>Section</td>
<td>Title</td>
<td>Page</td>
</tr>
<tr>
<td>---------</td>
<td>----------------------------------------------------------------------</td>
<td>------</td>
</tr>
<tr>
<td>3.9</td>
<td>Mixture Ratio for Casting of Foamed Concrete Panel</td>
<td>103</td>
</tr>
<tr>
<td>3.10</td>
<td>Foamed Concrete Properties</td>
<td>104</td>
</tr>
<tr>
<td>3.11</td>
<td>Mixture ratio for foamed concrete with strength 12 MPa to 17 MPa</td>
<td>110</td>
</tr>
<tr>
<td>4.1</td>
<td>Dimensions and Properties of PLFC Panel Specimens</td>
<td>115</td>
</tr>
<tr>
<td>4.2</td>
<td>Ultimate Failure Load for PLFC Panels</td>
<td>117</td>
</tr>
<tr>
<td>4.3</td>
<td>Crack Pattern and Mode of Failure for All Panels</td>
<td>121</td>
</tr>
<tr>
<td>4.4</td>
<td>Surface Strain Distribution</td>
<td>136</td>
</tr>
<tr>
<td>4.5</td>
<td>Maximum surface strain values from experiment</td>
<td>137</td>
</tr>
<tr>
<td>4.6</td>
<td>Maximum shear strain at mid-height of panel PA-7 to PA-14</td>
<td>140</td>
</tr>
<tr>
<td>5.1</td>
<td>Properties of Foamed Concrete used in the PLFP FE Model</td>
<td>147</td>
</tr>
<tr>
<td>5.2</td>
<td>Plastic Properties of Foamed Concrete Wythes</td>
<td>148</td>
</tr>
<tr>
<td>5.3</td>
<td>Properties of Steel used as Reinforcement and Shear</td>
<td>149</td>
</tr>
<tr>
<td>5.4</td>
<td>Properties of Normal Concrete used in the PLFP FE Model</td>
<td>150</td>
</tr>
<tr>
<td>5.5</td>
<td>Ultimate Loads of PA-1 to PA-14 from experiment and FEM Analysis</td>
<td>153</td>
</tr>
<tr>
<td>5.6</td>
<td>First Crack Load and Failure Load of Panel PA-1 to PA-14 As Obtained From FEM</td>
<td>157</td>
</tr>
<tr>
<td>5.7</td>
<td>Crack Pattern for Various Slenderness Ratios</td>
<td>158</td>
</tr>
<tr>
<td>5.8</td>
<td>Ultimate strength, Pu, for panel PA-10 with various truss diameters</td>
<td>166</td>
</tr>
<tr>
<td>5.9</td>
<td>Comparison of ultimate load achieved for single and double shear truss connectors in panel PA-6</td>
<td>172</td>
</tr>
<tr>
<td>5.10</td>
<td>Effects of various height of panel on ultimate strength and</td>
<td></td>
</tr>
</tbody>
</table>
5.11 Ultimate load, deflection and strain distribution for various thicknesses of panel at mid-height

6.1 Ultimate Loads of PA-1 to PA-14
(Experimental, FEM and ACI318-89)

6.2 a) Ultimate Strength for Various Slenderness Ratio from Experiment

b) Ultimate Strength for Various Slenderness Ratios from FEM Simulation
## LIST OF FIGURES

<table>
<thead>
<tr>
<th>FIGURE NO.</th>
<th>TITLE</th>
<th>PAGE</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.1</td>
<td>Precast Structure Systems (Bohdan, 1966)</td>
<td></td>
</tr>
<tr>
<td></td>
<td>a) Bearing Wall Structure</td>
<td>4</td>
</tr>
<tr>
<td></td>
<td>b) Frame and skeletal Structure</td>
<td>4</td>
</tr>
<tr>
<td>1.2</td>
<td>Various types of architectural load-bearing wall panels</td>
<td></td>
</tr>
<tr>
<td></td>
<td>(Freedman, 1999)</td>
<td>5</td>
</tr>
<tr>
<td>1.3</td>
<td>Typical Precast Concrete Sandwich Panel with Its Components</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>7</td>
</tr>
<tr>
<td>1.4</td>
<td>Precast Concrete Sandwich Panel in 3-D</td>
<td></td>
</tr>
<tr>
<td></td>
<td>(Benayoune et al., 2006)</td>
<td>7</td>
</tr>
<tr>
<td>2.1</td>
<td>Types of Compositeness of pre-cast concrete sandwich panel</td>
<td></td>
</tr>
<tr>
<td></td>
<td>(Shutt, 1997)</td>
<td>18</td>
</tr>
<tr>
<td>2.2</td>
<td>Honeycomb-cored sandwich panel (Jeom et al., 1999)</td>
<td>20</td>
</tr>
<tr>
<td>2.3</td>
<td>Foam board strip wrapped by E-glass fabric</td>
<td></td>
</tr>
<tr>
<td></td>
<td>(Stoll et al., 2004)</td>
<td>21</td>
</tr>
<tr>
<td>2.4</td>
<td>Core Preform (Stoll et al., 2004)</td>
<td>22</td>
</tr>
<tr>
<td>2.5</td>
<td>Molded panel with foam removed, showing composite webs and resin ridge (Stoll et al., 2004)</td>
<td>22</td>
</tr>
<tr>
<td>2.6</td>
<td>EPS Embedded With Trusses (Lee et al., 2006)</td>
<td>24</td>
</tr>
<tr>
<td>2.7</td>
<td>Cellulose Fiber Cement Board Panel (Lee et al., 2006)</td>
<td>25</td>
</tr>
<tr>
<td>2.8</td>
<td>Fiber-reinforced Composite Panel (Lee et al., 2006)</td>
<td>25</td>
</tr>
<tr>
<td>Section</td>
<td>Description</td>
<td></td>
</tr>
<tr>
<td>---------</td>
<td>-------------</td>
<td></td>
</tr>
<tr>
<td>2.9</td>
<td>Floor and wall sandwich panels used in the panelized building model (Rizzo et al., 1979)</td>
<td></td>
</tr>
<tr>
<td>2.10</td>
<td>Half-scale sandwich panel building model (Rizzo et al., 1979)</td>
<td></td>
</tr>
<tr>
<td>2.11</td>
<td>Critical b/t ratios of profiled sandwich panel for local buckling (Pokharel and Mahendran, 2003)</td>
<td></td>
</tr>
<tr>
<td>2.12</td>
<td>Typical failure modes (a) local buckle (b) local plastic mechanism (Pokharel and Mahendran, 2003)</td>
<td></td>
</tr>
<tr>
<td>2.13</td>
<td>Influence of slenderness ratio on ultimate load (Benayoune et al., 2006)</td>
<td></td>
</tr>
<tr>
<td>2.14</td>
<td>Loading set up for walls (Pillai and Parthasarathy, 1977)</td>
<td></td>
</tr>
<tr>
<td>2.15</td>
<td>Comparison of load capacities of wall as obtained from experiment and theory (Pillai and Parthasarathy, 1977)</td>
<td></td>
</tr>
<tr>
<td>2.16</td>
<td>Details of truss girder connectors (Bush and Stine, 1994)</td>
<td></td>
</tr>
<tr>
<td>2.17</td>
<td>Diagonal Truss Connectors (Benayoune et al., 2006)</td>
<td></td>
</tr>
<tr>
<td>2.18</td>
<td>Front view and cross section of a multilayer wall specimen (Rosenthal, 1984)</td>
<td></td>
</tr>
<tr>
<td>2.19</td>
<td>Failure mode for Panel W1600 and W1400 (Sulaiman et al., 2009)</td>
<td></td>
</tr>
<tr>
<td>2.20</td>
<td>Applied Axial Load versus Displacement (Sulaiman et al., 2009)</td>
<td></td>
</tr>
<tr>
<td>2.21</td>
<td>Schematic diagram for Four-point bending test set-up (Mohammed and Nasim, 2009)</td>
<td></td>
</tr>
<tr>
<td>2.2.2</td>
<td>Schematic diagrams for the panels used in the experimental work (Mohammed and Nasim, 2009)</td>
<td></td>
</tr>
<tr>
<td>2.23</td>
<td>Comparison between AAC and FRP/AAC shear strength</td>
<td></td>
</tr>
</tbody>
</table>
2.24 Shotcrete sandwich panel (Kabir, 2005) 42
2.25 Installed shotcrete sandwich panel (Rezaifar et al., 2008) 43
2.26 Dimensional view of the cross-section of the specimens (Memon et al., 2007) 45
2.27 Comparison of various properties of sandwich composite with control (Memon et al., 2007) 45
2.28 Failure mode of various specimens after tests (Memon et al., 2007) 46
2.29 Young Modulus versus Density (Tonyan and Gibson, 1992) 48
2.30 Compressive strength versus Density (Tonyan and Gibson, 1992) 48
2.31 Variation of flow of foam concrete with foam cement (Nambiar and Ramamurthy, 2006) 49
2.32 Strength density variation for mixes with sand of different fineness (Nambiar and Ramamurthy, 2006) 50
2.33 Strength density variation for mixes with different filler type (Nambiar and Ramamurthy, 2006) 50
2.34 Cross-sectional Dimensions of Test Specimens:
   (a) Concrete-filled CHS (b) Concrete-filled SH (Yasser, 1997) 51
2.35 Details of Loading System for Beam Specimens (Yasser, 1997) 52
2.36 Relationship between 7-day compressive strength and dry density for foamed concrete (BCA, 1999) 54
2.37 Schematic diagram for testing (Pokharel N. et al.) 62
2.38 (a) Half-length FEM model (b) Buckling shape of panel
2.39 Load-deflection curves for horizontal slab bending test

(Kabir, 2005)

2.40 Influence of shear connector’s diameter on flexural loading

(Kabir, 2005)

2.41 Specimen model by FEM (Rezaifar et al., 2008)

3.1 Mild steel BRC mesh and the truss connectors placed in the steel Formwork

3.2 Fine sand sieved from no. 5 sieve

3.3 Foam generator

3.4 Foam right after being discharged from the generator

3.5 Specimen positioned in a testing machine for split tensile test

3.6 Specimen positioned in UTM machine with attachment of compressometer to determine the Modulus Young, \( E \)

3.7 (a) BRC and Shear Connectors placed horizontally in the formwork

(b) The polystyrene was cut and placed on top of the lower wythe

(c) Foamed concrete poured on the top of polystyrene layer as the upper wythe

(d) Finish of the PLFP panel specimen

3.8 Details of PLFP specimens for Pilot Test

3.9 Set-up of specimen and test frame

3.10 Magnus Frame

3.11 (a) Bottom end condition of panel (Detail A)
(b) Top end condition for panel (Detail B) and arrangement for applying pure axial load

3.12 Locations of LVDT at middle front and rear surface of all panels

3.13 (a) Crushing and cracking at top part of panel PLFP-3
(b) Crushing and cracking at bottom part of panel PLFP-3

3.14 Load-deflection profile for panels PLFP-1 to PLFP-4

3.15 Fabrication of Panel PLFP-5 and PLFP-6
(a) (b) and (c) Bars and links for the end capping
(d) and (e) BRC and shear truss were placed in the formwork before foamed concrete for the bottom layer is poured
(f) polystyrene were cut and placed on the bottom layer
(g) top BRC was placed before the top concrete layer is poured
(h) top layer of foamed concrete is poured

3.16 Failure mode in panel PLFP-5 and PLFP-6

3.17 Load-deflection profile for panels PLFP-5 and PLFP-6

3.18 (a) and (b): High tensile steel of 9 mm diameter bars reinforcement

3.19 Continuous truss-shaped connectors running the full height of the panels used to tie the lower and upper wythes

3.20 (a) Shear connectors for 100 mm thick PLFP panel
(b) Shear connectors for 125 mm thick PLFP panel
(c) Shear connectors for 200 mm thick PLFP panels

3.21 Details of PLFP panel with capping at both ends

3.22 Fabrication of panel PA-1 to PA-14 for experimental Programme

(a) & (b): Reinforcement and Shear Connectors placed in the formwork of the specimen with capping at both ends

(c) Normal concrete capping

(d) Casting of lower wythe

(e) Finish of PLFP with capping at both ends

3.23 Locations of Strain Gauges

3.24 Locations of LVDT at top front surface of panels PA-10, PA-11, PA-13, and PA-14

4.1 Ultimate Strength versus Slenderness Ratio for Panels PA-1 to PA-14 for 6 mm and 9 mm shear connectors

4.2 Curve fitting line which fall between the curves for 6 mm and 9 mm shear connectors

4.3 Crack and crush at the top and bottom half of panel of panel PA-10

4.4 Crushing at mid-height of panel PA-9 due to buckling in the middle zone of panel

4.5 Crack and crush at mid-height of panel PA-12

4.6 Load-horizontal deflection curves at mid-height of panels

4.7 Deflection along the height of panel PA-10

4.8 Deflection along the height of panel PA-13

4.9 (a) Load-strain curves for panel PA-6 under axial load
(b) Load-strain curve for PLFP panel PA-4

(c) Load-strain curve for PLFP panel PA-14

4.10 Shear strain distribution across the mid-height of panel PA-10

4.11 Load versus Strain at mid-height of panel PA-9

4.12 Load versus Strain at mid-height of panel PA-12

5.1 2-D plane stress element model of PLFP panel

5.2 2-D plane stress element model of PLFP in which nodes on steel shear truss connectors and wythe surface met

5.3 Load-lateral deflection curve for panel PA-10 measured at mid-height

5.4 Crack pattern of Panel PA-6 at failure load

5.5 FEM Result of Load versus Lateral Deflection for Panels PA-1 to PA-14 at mid-height

5.6 Deflection of wythe in PLFP panel PA-10

5.7 Deflection along the height of panel PA-10 at ultimate load

5.8 Deflection along the height of panel PA-10 as obtained from experiment and FEM at ultimate load

5.9 Load versus surface strain at mid-height of panels PA-2, PA-5 and PA-9

5.10 Strain distribution across thickness of panels PA-2, PA-5 and PA-10 at mid-height at ultimate load

5.11 Ultimate load versus bar diameter for panel PA-10 with reinforcement size of 9 mm

5.12 Strain across the thickness of panel PA-10 at ultimate load
measured at mid-height as obtained from FE analysis

5.13  
(a) Strain across thickness of Panel PA-10 at mid-height with truss diameter 9 mm at ultimate load
(b) Strain across thickness of Panel PA-10 at mid-height with truss diameter 10 mm at ultimate load
(c) Strain across thickness of Panel PA-10 at mid-height with truss diameter 12 mm at ultimate load

5.14  Symmetrical orientation of shear truss connectors

5.15  Strain distribution across panel thickness with shear connector’s diameter of 10 mm measured at mid-height

5.16  Strain distribution across panel thickness with shear connector’s diameter of 12 mm measured at mid-height

5.17  Ultimate Load (Pu) for various Height of Panel (H)

5.18  Maximum lateral deflection values for different height of panel

5.19  Strain distribution across the panel’s thickness for various heights

5.20  Ultimate Load versus Thickness for Panel 2800 mm

5.21  Deflection versus Overall Thickness

5.22  Strain distribution across the panel’s thickness for various overall thicknesses of panels at mid-height

5.23  Strain distribution across the panel’s thickness for 110 mm overall thickness of panel at mid-height

6.1  Percentage difference between ultimate strength from experiment and FEM
6.2 Relationship between ultimate strength and slenderness ratio from experiment and FEM 190
6.3 Deflection of wythe in PLFP panels with different slenderness ratio 191
6.4 Strain distribution across the thickness of PLFP panel PA-5 194
6.5 Strain distribution across the thickness of panel PA-6 195
6.6 Stress-strain Curve for Steel 196
6.7 Ultimate strength vs slenderness ratio as obtained from experiment, FEM, Equation 6.2 and Equation 6.3 200
6.8 Comparison between ultimate strength from full-scaled test and using Equation 6.3 201
6.9 Comparison between ultimate strength from full-scaled test and using equation 6.4 202
6.10 Comparison between ultimate strength from experiment and using equation 6.5 204
6.11 Relationship between Ultimate Strength and Slenderness Ratio from Experiment, FEM, Equation 6.2, Equation 6.3 and Proposed Equation 6.5 205
**LIST OF ABBREVIATION**

<table>
<thead>
<tr>
<th>Abbreviation</th>
<th>Full Form</th>
</tr>
</thead>
<tbody>
<tr>
<td>CIDB</td>
<td>Construction Industry Development Board of Malaysia</td>
</tr>
<tr>
<td>IBS</td>
<td>Industrial Building System</td>
</tr>
<tr>
<td>PLFP</td>
<td>Precast Lightweight Foamed Concrete Sandwich Panel</td>
</tr>
<tr>
<td>FEM</td>
<td>Finite Element Method</td>
</tr>
<tr>
<td>PCSP</td>
<td>Precast Concrete Sandwich Panel</td>
</tr>
<tr>
<td>FRC</td>
<td>Fiber-Reinforced Composite</td>
</tr>
<tr>
<td>EPS</td>
<td>Expanded Polystyrene Panel System</td>
</tr>
<tr>
<td>PAC</td>
<td>Pumice Aggregate Concrete</td>
</tr>
<tr>
<td>HPC</td>
<td>High Performance Concrete</td>
</tr>
<tr>
<td>FRP</td>
<td>Fiber Reinforced Polymer</td>
</tr>
<tr>
<td>AAC</td>
<td>Autoclaved Aerated Concrete</td>
</tr>
<tr>
<td>BCA</td>
<td>British Cement Association</td>
</tr>
<tr>
<td>ASTM</td>
<td>American Standard Testing Method</td>
</tr>
<tr>
<td>BS</td>
<td>British Standard</td>
</tr>
<tr>
<td>UTM</td>
<td>Universal Testing Machine</td>
</tr>
<tr>
<td>E</td>
<td>Modulus Young</td>
</tr>
<tr>
<td>LVDT</td>
<td>Linear Voltage Displacement Transducer</td>
</tr>
<tr>
<td>ESG</td>
<td>Electrical Strain Gauge</td>
</tr>
</tbody>
</table>
LIST OF SYMBOLS

\( H \) - Height of panel
\( H/t \) - Slenderness ratio
\( EI \) - Stiffness
\( EcIg \) - Gross uncracked stiffness
\( P_u \) - Ultimate strength of panel
\( \varnothing \) - Strength reduction factor
\( f_{cu} \) - Compressive strength of foamed concrete
\( A \) - Gross area of section
\( k \) - Slenderness Factor
\( t \) - Overall thickness of member
\( N \) - Ultimate axial load
\( N_{sc} \) - Design ultimate capacity
\( N_{bal} \) - Design axial load capacity for symmetrically reinforced rectangular section
\( k \) - Reduction Factor
\( A_{sc} \) - Area of steel
\( f_y \) - Tensile strength of steel
\( P_u \) - Ultimate axial load
\( A_c \) - Gross area of panel section
\( f_y \) - Yield strength of steel
\( L \) - Width of the panel
\( A_c \) - Gross area of the wall panel section (equal to the gross concrete area)

\( t_1 \) - Thickness of wythe

\( t_2 \) - Thickness of core layer

\( c \) - Concrete cover

\( f_t \) - Tensile Strength of foamed concrete

\( \varepsilon_c \) - Strain at peak uniaxial compression

\( \varepsilon_o \) - Strain at end of softening curve

\( G_f \) - Fracture energy per unit area

\( \beta_r \) - Biaxial to uniaxial stress ratio

\( Z_o \) - Initial relative position of yield surface

\( \psi \) - Dilatancy factor

\( m_g \) - Constant in interlock state function

\( m_{hi} \) - Contact multiplier on \( \varepsilon_o \)

\( m_{ful} \) - Final contact multiplier on \( \varepsilon_o \)

\( r_\sigma \) - Shear intercept on tensile strength

\( \mu \) - Slope of friction asymptote for damage

\( \sigma_y \) - Initial yield stress

\( Pt \) - Stress at ultimate

\( \varepsilon \) - Strain at Failure

\( E \) - Modulus Young of Steel

\( \rho_{wet} \) - Wet density of foamed concrete

\( \rho_{dry} \) - Dry density of foamed concrete

\( v \) - Poisson’s Ratio

\( \alpha \) - Coefficient of thermal expansion
$e$ - Eccentricity
## LIST OF APPENDICES

<table>
<thead>
<tr>
<th>APPENDIX</th>
<th>TITLE</th>
<th>PAGE</th>
</tr>
</thead>
<tbody>
<tr>
<td>A</td>
<td>Foamed Concrete Properties</td>
<td>224</td>
</tr>
<tr>
<td>B</td>
<td>Steel Properties</td>
<td>232</td>
</tr>
<tr>
<td>C</td>
<td>Crack Pattern and Failure Mode for PLFP Panels</td>
<td>233</td>
</tr>
<tr>
<td>D</td>
<td>Load-Strain Graphs for PLFP Panels</td>
<td>242</td>
</tr>
<tr>
<td>E</td>
<td>Data for Deflection of PLFP Panels</td>
<td>256</td>
</tr>
<tr>
<td>F</td>
<td>Surface Strain Readings</td>
<td>265</td>
</tr>
<tr>
<td>G</td>
<td>Maximum Strain in Main Bar and Shear Connector</td>
<td>272</td>
</tr>
<tr>
<td>H</td>
<td>Calculation of Loading for 5-Storeys Residential</td>
<td>273</td>
</tr>
<tr>
<td></td>
<td>Building</td>
<td></td>
</tr>
</tbody>
</table>
CHAPTER 1

INTRODUCTION

1.1 Construction Industry in Malaysia

Housing remains a major issue in Malaysia as in many other developing countries in the world. The problem is raised due to the increasing population, demands of affordable and quality houses, migration of rural masses into the city and industrial centers and also demands due to higher quality of life. The increase in housing demand during the Ninth Malaysia Plan (2006 to 2010) from the public and private sector is shown in Table 1.1. It is observed from this table that approximately 709,400 houses are targeted for different user-groups during the 5 years period.

Table 1.1: Housing Targets from the Public and Private Sector, 2006 to 2010
(Construction Industry Development Board, 2007)

<table>
<thead>
<tr>
<th>Programme</th>
<th>Number of houses</th>
<th>Total</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Housing for the poor (PPRT)</td>
<td>Low Cost</td>
</tr>
<tr>
<td>Public sector</td>
<td>20,000</td>
<td>85,000</td>
</tr>
<tr>
<td>Private sector</td>
<td>80,400</td>
<td>48,500</td>
</tr>
<tr>
<td>Total</td>
<td>20,000</td>
<td>165,400</td>
</tr>
<tr>
<td>%</td>
<td>2.8</td>
<td>23.3</td>
</tr>
</tbody>
</table>
It is difficult to provide solutions to this problem with the present traditional building construction systems because the traditional system is unable to meet the housing demand in a short time without sacrificing quality. Due to this inadequacy of traditional building construction systems, new technology is needed in the construction industries which can meet this requirement. Meeting the demands for higher performance, lower cost and faster projects requires transition from traditional building techniques to innovative construction methods.

Construction Industry Development Board of Malaysia, (CIDB), has produced a 10-year master plan for Malaysian construction industry for a period from 2006 to 2015. It is a comprehensive plan charting the strategic position and future direction of the Malaysian construction (CIDB, 2007). It is also aimed at supporting the nation’s economic growth as well as increasing accessibility to adequate, affordable and quality houses for all income groups, particularly the lower ones.

The planning does not only focus on improving the living standard of Malaysians, but also on harvesting the development of caring society. There are seven strategic thrusts in the Master Plan which are inter-related and together serve to achieve the overall vision. The fifth strategic thrust in the Plan is innovation through research and development and adoption of new construction method. This thrust is aimed at addressing the polemic of the local construction industry which has been characterized as labour intensive and dependent on foreign unskilled workers. As such, the construction industry needs to progress towards one that is more focused in innovation.

Industrial Building Systems or IBS is one of the innovations and is seen as one solution in the development of new technology in the construction industries. IBS utilizes techniques, products, components, or building systems which involve prefabricated components and on-site installation. It has been in existence since the 1960's (Thanoon et al., 2003). However, according to the CIDB IBS Survey, less than one third of completed projects up to 2002 utilized IBS. IBS should be utilized more aggressively in the local industry because it helps to overcome problems imposed by the traditional labour intensive methods.
IBS promises numerous benefits compared to the conventional method. Its usage is usually more economical than the conventional construction system due to the following advantages (Junid, 1986, Esa and Nurudin, 1998, Lessing et al., 2005):

a) Standardization of sizes and materials allows faster and more accurate production with less waste.

b) More accurate scheduling can be obtained because of more predictable production.

c) The use of unskilled or semi skilled labour is possible by the simplicity and standardization of the construction technique.

d) With the use of standardization of building components, the use of Information Technology (IT) in construction can further be enhanced. IT will speed up the networking between the consultants, architects, contractors and most importantly, the clients.

In general IBS construction method leads to increased efficiency and productivity. This chapter discusses precast lightweight sandwich technology as an IBS system that has great potential to be further studied and developed in Malaysian’s construction industry.

1.2 Precast Concrete Building System

Precast building system is a system where parts, members and elements of structures are produced either on-site or at the factory, and transported to the site of construction. Using concrete material, the precast component may be cast in a formwork in a position other than the actual one. After the concrete has matured, the forms are removed and the component are installed and fixed in the actual position. The benefits of precast concrete as compared to conventional system include its better quality control and, fast delivery and installation. In most cases, precast panels are cast with high quality concrete and therefore results in smooth surface appearance.
The precast building systems are mainly categorized into load bearing wall structure system (Figure 1.1(a)), and frame and skeletal structure system (Figure 1.1(b)). The structural elements of load-bearing wall structure systems consist of load-bearing walls and floors while the structural elements of frame and skeletal structure systems consist of columns, beams and floors. The frame and skeletal structure systems are utilized mainly for industrial buildings, shopping malls, car parks, sporting facilities and office buildings, whereas the load-bearing wall structures are suitable for apartment buildings, nursing homes, dormitories, and hotels (Bohdan, 1966).

Wall element of a building can be constructed using precast system. A precast wall system can be comprised of flat or curved panels (solid, hollow-core, or insulated), window or mullion panels, ribbed panels, or a double-tee as shown in Figure 1.2. These precast elements are normally used as cladding material which is non-load bearing (Freeman, 1999). This is due to their structural capability as load bearing elements are often overlooked. For instance, in the case of low or medium rise buildings, the amount of reinforcements required in handling and erecting cladding panels such as wall and window panels are often more than necessary for carrying imposed loads. Thus, with relatively few modifications, these panels can function as load bearing members especially in the low to medium rise buildings.
Figure 1.2: Various types of architectural load-bearing wall panels.
(Freeman, 1999)
1.3 Precast Sandwich Panel

Precast sandwich panel is a layered structural system composed of low density core material which acts integrally with the high strength facing material. Structures made of precast sandwich panels can be remarkably strong and lighter in weight. The trend for “stronger-lighter” product is becoming increasingly important in the construction industry.

Various forms of sandwich construction may be obtained by combining different wythe and core or insulation materials. The wythes may be constructed out of varieties of materials such as concrete, steel, aluminium, or carbon fiber material (Lee and Pessiki, 2006, Benayoune et al., 2006, Liew and Sohel, 2009, Jeom et al., 1999, Rice et al., 2006). The core layers are often composed of lightweight concrete, fibre reinforced composite, balsa wood, foam, polymer foam and structural honeycomb material such as aluminium honeycomb concrete (Liew and Sohel, 2009, Jeom et al., 1999, Stoll et al., 2004, Scudamore and Cantwell, 2002). These materials can be combined to form composite panels which enable the optimum design to be produced for particular applications.

A typical concrete sandwich panel is shown in Figure 1.3. It consists of an insulation layer which is enclosed by inner and outer concrete wythes. The concrete wythes may be of a standard shape, such as a flat slab, hollow-core section or double tee. The wythes can be connected together using shear connectors through the insulation layer to promote composite action so that the system can be used as structural element. Figure 1.4 shows a typical 3-D view of sandwich panel with truss shaped shear connectors.

Structural sandwich panels provide the dual functions of transferring load and insulating the structure. They may be used solely for cladding, or they may act as beams, bearing walls, or shear walls. Interest in sandwich panels as load-bearing wall panels has been growing over the past few years because manufacturers are looking for more viable products and are pleased with their structural efficiency, insulation property, light weight and aesthetics values. Sandwich panels are similar to other precast concrete members with regard to design, detailing, manufacturing, handling,
shipping and erection; however, because of the presence of insulation layer, they do exhibit some unique characteristics and behavior.

Figure 1.3: Typical Precast Concrete Sandwich Panel with Its Components

Figure 1.4: Precast Concrete Sandwich Panel in 3-D
(Benayoune et al., 2006)
1.4 Lightweight Foamed Concrete

Foamed concrete has been widely used especially in the western countries. It is originated from Scandinavia some thirty years ago. Nowadays, foam concrete technology has been widely used in construction industries. It is considered as an attractive material for its lightweight, better thermal properties and ease of construction. In the United States for instance, foamed concrete are used in an increasing number of applications. Cast-in-place foamed concrete are used for insulating roof-deck systems and for engineered fills for geotechnical applications while precast auto-claved products are widely used as load-bearing blocks, reinforced wall, roof and floor units and as non load-bearing cladding panels over a primary structural frame (Tonyan and Gibson, 1992).

Foam concrete is a low density hardened Portland cement paste, containing a large number of small bubbles. Cement foam can be manufactured either by a chemical or a mechanical foaming process. In the chemical process, a powdered metal (usually aluminum) is added to slurry composed of cement and lime. Most of the aerated concrete produce with this method have densities between 480 and 960 kg/m$^3$ (Tonyan and Gibson, 1992).

In a mechanical foaming process, foaming agent is added into the cement slurry either directly or in a form of perform foam. The presence of cement causes the material to be cohesive after the hydration of the cement. The entrapped air bubbles increases the volume and thereby reduces the densities of a concrete. This volume between the slurry and the foam determine the density of the foam concrete. The preform foam provides better control of density and foam cell structure. The foamed concrete’s materials and characteristic properties are described in the following sections. In both the chemical and mechanical processes described above, the cement foam is usually cured in a moist environment at ambient temperature.
1.4.1 Materials

Foam concrete is a mixture of cement, fine sand, water and special foam, which produces a strong, lightweight concrete containing millions of evenly distributed and consistently sized air bubbles or cells. The density of foam concrete is determined by the amount of foam added to the basic cement, sand and the water mixed together.

1.4.2 Characteristic properties of foamed concrete

The characteristic properties of foamed concrete includes its compressive strength, tensile strength, shear strength, shrinkage, coefficient of linear expansion, acoustic and thermal insulation, and fire resistance. The characteristic properties of foamed concrete will be presented in the following paragraphs according to the report on Foamed Concrete Composition and Properties (British Cement Association, 1994).

The compressive strength of foam concrete is influenced by many features like density, age, moisture content, and the physical and chemical characteristics of its component materials and mix proportions. A relationship exists between the density and the strength where it is found that the higher the density of the mixture, the greater the strength of the end product. For foamed concrete with densities ranging from 300 to 1600 kg/m³, the compressive strength at 28 days is from 0.2 to 12 N/mm². The compressive strength will continue to increase indefinitely due to the reaction with carbon dioxide, CO₂, present in the surrounding air.

Depending on the method of curing, the tensile strength of foam concrete can be as high as 0.25 of its compressive strength with a strain around 0.1% at the time of rupture. Meanwhile, the shear strength varies between 6% and 10% of the compressive strength.

Shrinkage property in foamed concrete is a phenomenon during the setting stage. The amount of shrinkage is dependent on the type of cement used, type of curing, the size and quality of the sand, the amount of cement in the mix, density of
the concrete, and the water cement ratio. The greater extent of shrinkage occurs during the first 28 days of the concrete’s age.

The coefficient of linear thermal expansion for foam concrete is of the same order as that of normal concrete. Foam concrete has high sound absorption capacity and a very low transmission of heat. It is also extremely fire resistant where the level of resistance is greatly superior to normal concrete.

1.4.3 Advantages of Foamed Concrete

Foamed concrete has many advantages. However, the most important are its compressive strength and its low density. Foamed concrete in general has good mechanical strength combined with lightweight and low thermal conductivity. Good thermal insulation properties give energy conservation advantages which reduce the operating cost. Besides, it can be produced in a wide range of densities and properties that can suit any particular requirements. Like normal concrete, it can easily be mould to any desired shapes or sizes.

Foamed concrete is also an economical solution, particularly in large volume applications. It is self-compacting; as such, the casting process is much easier. Due to its lighter weight, lower crane capacity is required and lesser number in manpower is needed during the erection process. Its rapid installation contributes to the total cost saving. Placement of foamed concrete is a continuous operation from the mobile central plant where it pumps easily with relatively low pressure. The maintenance cost is also low because of its durability. It is also fire resistant and its surface texture makes it a good sound absorbent.
1.5 Precast Lightweight Foamed Concrete Sandwich Panel, PLFP

Lightweight foamed concrete can be produced by mixing sand, cement, water and stable foam using a mechanical air-entraining admixture. The product is a cementitious paste of cement and fine sand with micro discrete air cells uniformly distributed throughout the mixture to create a lightweight concrete. The density of the foamed concrete is controlled by the amount of tiny air pockets added into the mixture via foaming process. Lightweight foamed concrete has been used in construction for non-structural building wall panels or as partitions. It is considered as an attractive material because of its lightweight, better thermal properties and ease of construction.

Lightweight foamed concrete mixture can be designed to have higher strength which is close to the strength of the normal concrete. In order for lightweight concrete to be used as structural element, it must have the density of 1440 to 1840 kg/m³. Higher density results with higher strength of concrete. For structural application, the concrete strength should be 17 MPa or above (American Concrete Institute, 1989).

Precast Lightweight Foamed Concrete Sandwich Panel or PLFP is proposed in this study as an alternative structural sandwich component that can meet the rapid housing demand in this country. It consists of lightweight foamed concrete as the wythes which enclose the polystyrene which act as the insulation layer. Shear connectors are embedded across each layer to allow load shearing between wythes. The strength and stability of the PLFP rely a lot on the stiffness of these shear connectors and its ability to transfer load between wythes. The primary use of structural lightweight concrete is to reduce the dead load of a building. Structural lightweight concrete provides a most efficient strength-to-weight ratio in structural elements. Reduction of weight will result in easy construction, reduction of transportation cost and reduced of foundations, which eventually will reduce the overall cost.
1.6 Problem Statement

The demands from the growing population and migration of people to urban areas require this country to look for alternative construction method to provide fast and affordable quality housing to its citizens. Efforts have been taken to move from the traditional building construction technique to a more innovative construction method to meet these demands. As a part of this effort, an extensive investigation to develop a Precast Lightweight Foamed Concrete Sandwich Panel or PLFP as a load bearing wall system is undertaken.

1.7 Objectives

The aim of this study is to develop a load-bearing Precast Lightweight Foamed Concrete Sandwich Panel (PLFP) for use as structural component in low rise building construction. In order to achieve this aim, several objectives are set out:

1. To develop and construct the sandwich PLFP panel using the lightweight foamed concrete.

2. To propose the right mixture for lightweight foamed concrete of sufficient strength and density suitable for use as structural component.

3. To study the structural behaviour of the proposed sandwich PLFP panel by means of experimental work and finite element method, FEM.

4. To develop a semi-empirical expression to estimate the load carrying capacity of the PLFP panel.
1.8 Scope of Work

In order to develop and construct the sandwich PLFP panel using lightweight foamed concrete, an experimental programme which includes fourteen full-scaled specimens was conducted to study its behaviour and axial load carrying capacity. Finite element study was further conducted to examine the effect of various parameters which dictate the panel’s strength and behaviour.

The experimental work started out with the pilot testing which includes trial mixing of lightweight foamed concrete to get the suitable density for the targeted compressive strength. The process of mixing was based on the typical mixture details for foamed concrete as given in British Cement Association. From the trial mixtures and the mixtures during the pilot testing and experimental programme, the right mixture for lightweight foamed concrete of sufficient strength and suitable density for use as a structural component is proposed.

The fourteen PLFP specimens in the experimental programme were tested under axial load to investigate its structural behaviour. The results were studied in term of its load carrying capacity, load-deflection profiles, strain distribution and efficiency of the shear connectors. Various height, thickness and diameters of shear connector were used in the FEM simulations to study the influence of slenderness ratio and to find the optimum shear connector’s size which ensures the stability of the panel in term of its ultimate strength and degree of compositeness achieved. The strain distribution across the panel’s thickness was used to study the efficiency and role of the shear connectors in transferring loads and to evaluate the extent of composite action achieved.

The results from the proposed FEM model and from the experimental work were analysed and compared. A semi-empirical expression was proposed to estimate the load carrying capacity of the PLFP panel. It was validated on the basis of the test data made available by previous research works.
1.9 Thesis Layout

The thesis consists of seven (7) chapters. The content of each chapter is described below:

Chapter I

This chapter presents an introduction of the Precast Lightweight Foamed Concrete Sandwich Panel, or PLFP, as an alternative building system which meets the challenge in the construction industry in Malaysia today. This chapter also discusses the objectives and the scope of work of the research.

Chapter II

This chapter presents the relevant literature review on the structural performance of the PLFP as sandwich wall panel. It also contains a review of the studies on lightweight foamed concrete and its properties. An overview of previous research works on sandwich wall panel of different material is also discussed with critical comments.

Chapter III

This chapter presents the methodology of the research, including the details on the actual and preliminary experimental work carried out to achieve the objectives as defined earlier. Fabrications and construction details of the test specimens and the materials used together with the test set up are described.

Chapter IV

This chapter contains presentation of results from the test data obtained from axial load tests on PLFP conducted experimentally in the present study. The observations are related to axial load bearing capacity, cracking patterns and mode of failure, load-deformation profiles, load-strain curves, and strain distribution across the panel’s thickness. The observations were made to verify the FEM model and
facilitate interpretation of the theoretical results as described in Chapter V and Chapter VI.

Chapter V

This chapter describes the modeling and type of analysis used in the non-linear finite element study. It also presents the response of PLFP under axial load as determined by the FEM model. The applicability of the adopted FEM model was first validated on the basis of axial test data presented in Chapter IV. The results from the FE analysis are used in discussing the achievement of objectives and further drawing conclusions on the behaviour of PLFP panels as load-bearing wall element.

Chapter VI

This chapter presents the discussion of the results obtained from the experimental work and FEM. A semi-empirical expression is developed to estimate the strength capacity of PLFP panels using conventional approach based on reinforced concrete principles and data from previous research.

Chapter VII

A summary of the major findings of the study together with some recommendations for further work is given in this chapter.