



Convective Boundary Conditions Effect on Cylindrical Media with Transient Heat Transfer

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ABSTRACT

Lattice Boltzmann method is used to solve inside a cylindrical cavity with convective boundary condition is highlighted in this paper. Because of its simple, stable, accurate, efficient and ease for parallelization, we use the thermal Single Relaxation Time Bhatnagar Gross Krook (SRT BGK) mesoscopic approach in order to solve the energy equation. Thermal fields are simulated using D2Q9 scheme. We introduce and demonstrate numerically some usual cases (Dirichlet, Neumann) of Boundary conditions (BCs). After validation, we extend the present work to the convective case. At the wall of the cavity, the unknown Thermal Distribution Functions (TDF) are exposed to the bounce back concept which is determined consistently by one of the imposed BCs. An in-house Fortran 90 code is used to analyze a variety of BCs inside a two-dimensional cavity. In validation, obtained results highlight a good agreement with literature. The present study is extended to deal with convective boundary condition for conduction transfer problems inside an axisymmetric cylindrical media subjected to heat generation and Newman boundary conditions.

1. Introduction

Countless physical models in the engineering applied science are simulated using nonlinear boundary conditions (BCs) value problems where it is usually difficult to obtain the exact analytical solution. Due of this difficulty, most of the researchers in the engineering and the applied sciences directly resort to the numerical codes in order to solve their physical models [1]. However, many other authors investigated their physical models by using analytical or semi-analytical methods [2-7]. Unfortunately, the accuracy of the numerical solutions derived from these analytical or semi-analytical methods cannot be checked without addressing the convergence issue.

In this paper, we use LBM to simulate convective boundary condition inside a cylindrical media. In fact, nowadays LBM is considered as bright numerical technique for simulating thermal and fluid flows associated with complex boundary conditions [8-20]. It is known that conventional numerical methods (CFD) discretize the macroscopic equations. However, LBM is based on simplified kinetic

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models integrating physics of microscopic processes where macroscopic properties obey the desired equations.

In the last decade, LBM was used to simulate heat transfer in different engineering applications such as thermal insulation, heat pipes, cooling of electronic components cooling, solar collectors (SC), heat exchangers, solar dryers air heating systems, storage technology, passive solar heating [21-26]. Owing to their accuracy and simplicity for studying confining cavities with mixed BCS, LBM is the suitable numerical choice when dealing with complex BCs.

In literature, few publications deal with LB studies that consider mixed Boundary conditions as Dirichlet, Newman, convective Boundary conditions. In validation, we consider two test cases for the solution of conduction problems in Cartesian geometry involving Dirichlet BCs and volumetric heat generation effect. For validation, two test benchmark problems are studied and good agreement is obtained. The present numerical approach can cope with more complex geometry and, thus, it will be particularly efficient in resolving transient conduction in axisymmetric cavity in the presence of heat generation effect with mixed boundary condition.

2. Numerical Approach

Heat transfer inside rectangular and axisymmetric enclosure is considered. Thermo-physical properties of the medium are assumed constant. For the problem under consideration, and in the absence of convection and radiation, the energy equation is given by

$$\frac{\partial T}{\partial t} = \alpha \nabla^2 T + Q \quad (1)$$

because the LBM is based on the discrete Boltzmann kinetic equation, heat transport problems are solved using the internal energy evolution equation of the nine-speed (D2Q9) Lattice Boltzmann model is given by [27-29]

$$\frac{\partial f_i(\vec{r}, t)}{\partial t} + \vec{e}_i \nabla f_i(\vec{r}, t) = \Omega_i, \quad i = 1, 2, 3, \dots, b \quad (2)$$

where,

b is the number of directions in a D2Q9 lattice

Ω_i is the collision operator defined as

$$\Omega_i = -\frac{1}{\tau} [f_i(\vec{r}, t) - f_i^{(0)}(\vec{r}, t)] \quad (3)$$

f_i is the particle distribution function denoting the number of particles at the lattice node \vec{r} at time t moving in direction i with velocity \vec{e}_i along the lattice link $\Delta \vec{r} = \vec{e}_i \Delta t$ connecting the nearest neighbours (Figure 1).

The temperature $T(\vec{r}, t)$ is defined as

$$T(\vec{r}, t) = \sum_{i=0}^b f_i(\vec{r}, t) \quad (4)$$

where the observed flux is expressed by

$$\sum_{i=0}^b f_i(\vec{r}, t) \vec{e}_i \quad (5)$$

In BGK model, the discrete evolution equation is given as

$$\frac{\partial f_i(\vec{r}, t)}{\partial t} + \vec{e}_i \nabla f_i(\vec{r}, t) = -\frac{1}{\tau} [f_i(\vec{r}, t) - f_i^{(0)}(\vec{r}, t)] \quad (6)$$

$f_i^{(0)}$ is the equilibrium distribution function.

Based on SRT model, the relaxation time can be related with the thermal diffusivity α , the lattice velocity C and the time step Δt by the following relation [29]

$$\tau = \frac{3\alpha}{|C|^2} + \frac{\Delta t}{2} \quad (7)$$

The nine velocities \vec{e}_i in the D2Q9 (Figure 1) and their corresponding weights w_i are the following

$$\vec{e}_0 = (0, 0) \quad (8)$$

$$\vec{e}_i = (\cos(\varphi_i), \sin(\varphi_i)) \cdot C \quad \text{for } \varphi_i = (i-1)\pi/2 \quad i = 1, 2, 3, 4 \quad (9)$$

$$\vec{e}_i = \sqrt{2}(\cos(\varphi_i), \sin(\varphi_i)) \cdot C \quad \text{for } \varphi_i = (i-5)\pi/2 + \pi \quad i = 5, 6, 7, 8 \quad (10)$$

$$w_i = \frac{4}{9} \quad (11)$$

$$w_i = \frac{1}{9} \quad \text{for } i = 1, 2, 3, 4 \quad (12)$$

$$w_i = \frac{1}{36} \quad \text{for } i = 5, 6, 7, 8 \quad (13)$$

In the presence of volumetric heat generation, Eq. (6) can be written as

$$f_i(\vec{r} + \vec{e}_i \Delta t, t + \Delta t) = f_i(\vec{r}, t) - \frac{\Delta t}{\tau} [f_i(\vec{r}, t) - f_i^{(0)}(\vec{r}, t)] + w_i \Delta t Q^* \quad (14)$$

where,

Q^* is the non-dimensional heat generation.

For heat conduction problems, the equilibrium distribution function is given as

$$f_i^{(0)}(\vec{r}, t) = w_i T(\vec{r}, t) \quad (15)$$

In LBM boundary condition, BCs properties of the known and unknown populations on each side as shown on Figure 1.

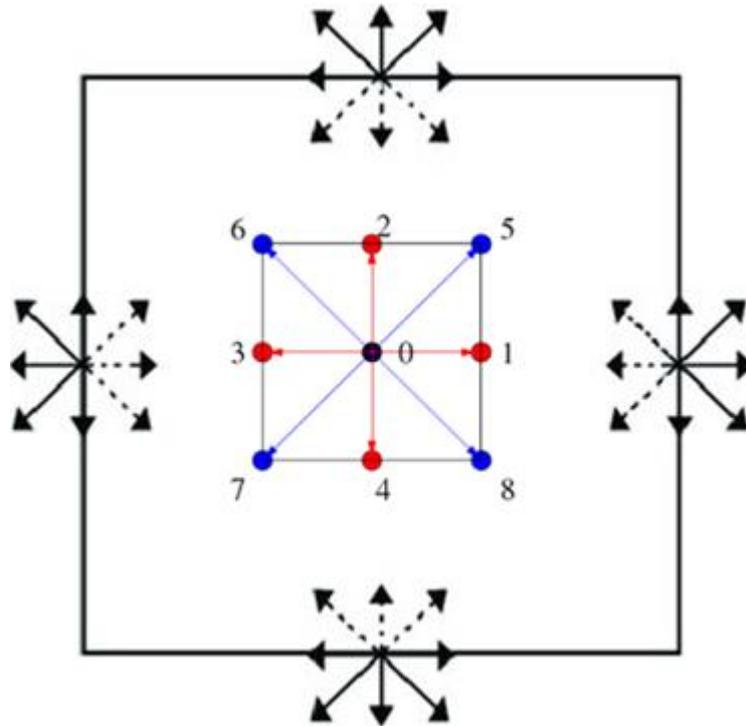


Fig. 1. BGK D2Q9 LBM Basic lattice and known and unknown populations in the computational domain

3. Results and Discussion

For validation, we deal with transient heat conduction problems in two-dimensional Cartesian enclosure with the four boundaries at isothermal temperatures. Initial and the boundary conditions are written as

Initial condition

$$T(x, y, 0) = T_{ref} \tag{16}$$

Boundary conditions

$$T(x, 0, t) = 0.25T_{ref} \tag{17}$$

$$T(x, Y, t) = T(0, y, t) = T(X, y, t) = T_{ref} \tag{18}$$

For this case, $\xi = \alpha t / L^2$ is the non-dimensional time and L is the characteristic length. $\Delta\xi$ was taken as 10^{-4} . Besides, transient and steady state conditions were highlighted. Convergence criteria assume that temperature difference between two consecutive time levels at each lattice centre did not exceed 10^{-6} . The same configuration is simulated, also, using the Finite Volume Method (FVM). The two numerical results are compared with literature. Figure 2 display non dimensional centreline ($x/X=0.5$) temperature at different instants ξ and good concordance is highlighted.

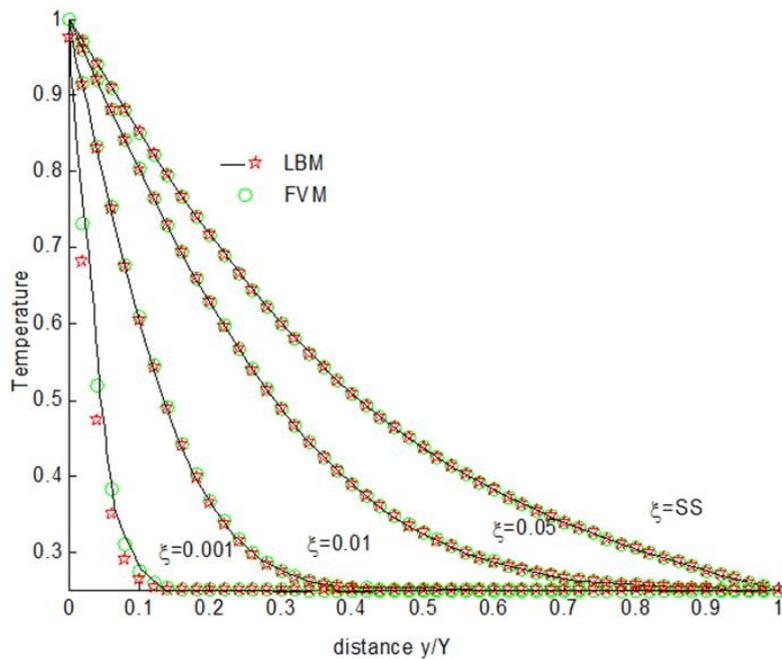


Fig. 2. Dimensionless mid-plane ($x/X=0.5$) temperature evolution for different dimensionless instants

Then, the effect of volumetric heat generation is studied. With a unity non dimensional volumetric heat generation, the four walls of the Cartesian cavity are subjected to a specified temperature (Dirichlet boundary condition). We notice that effect of heat generation is very less in the beginning compared to steady state because it takes some time to influence the temperature profile.

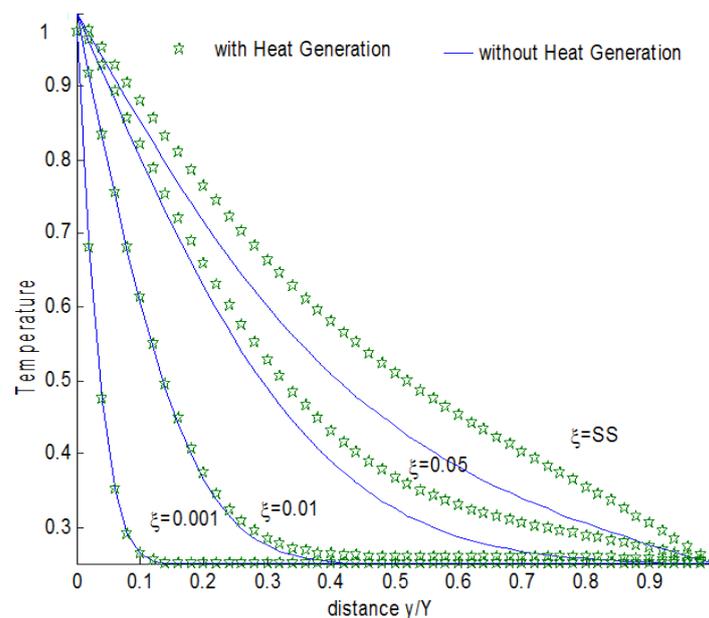


Fig. 3. Effect of volumetric heat generation on dimensionless mid-plane ($x/X=0.5$) temperature

This section deals with transient heat conduction equation in cylindrical coordinates. When Heat conduction in an infinite solid with a long cylindrical cavity is discussed, axisymmetric treatment is investigated. For this case (Figure 4), the system is initially at temperature

$$T(x, y, 0) = T_0 \tag{19}$$

For time $t > 0$, the bottom and top boundaries are at prescribed fluxes, respectively.

$$\frac{\partial T}{\partial y} = Q_s \tag{20}$$

$$-\frac{\partial T}{\partial y} = Q_N \tag{21}$$

For the physical problem addressed in this section (Figure 4), the thermal boundary condition at the lateral surface is subjected to convective heat flux boundary condition with non dimensional volumetric heat generation ($Q^* = 2$) written as

$$-k \frac{\partial T}{\partial x} = Q + h(T - T_\infty) \tag{22}$$

where,

h is the convective heat transfer coefficient.

x, y is the direction of outward normal to the surface concerned.

k Thermal conductivity

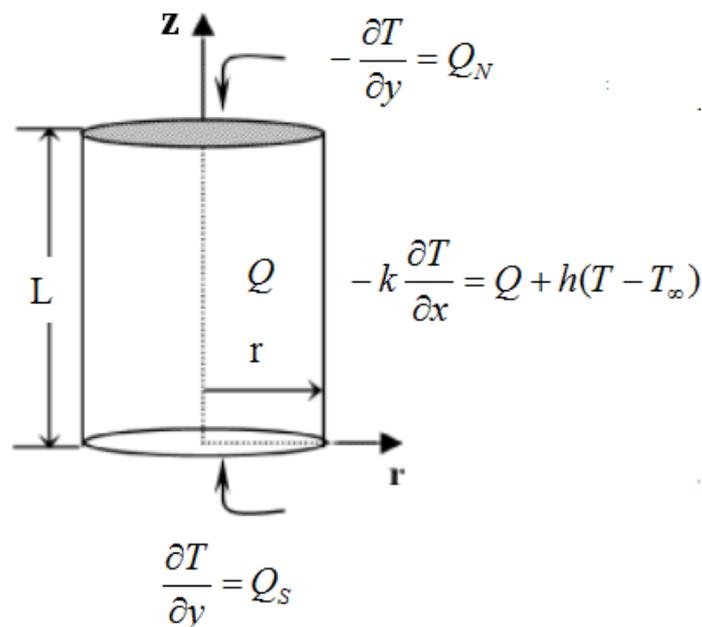


Fig. 4. Cylindrical boundary conditions

In non-dimensional equations model, we define Biot number as

$$Bi = \frac{hL}{k} \tag{23}$$

The distributions of isotherms inside cylindrical media are plotted in the Figure 5 for different where the axisymmetric is subjected to a volumetric heat generation condition ($Q^* = 2$) with Biot number of 20 in a 100x100 grid (Figure 5).

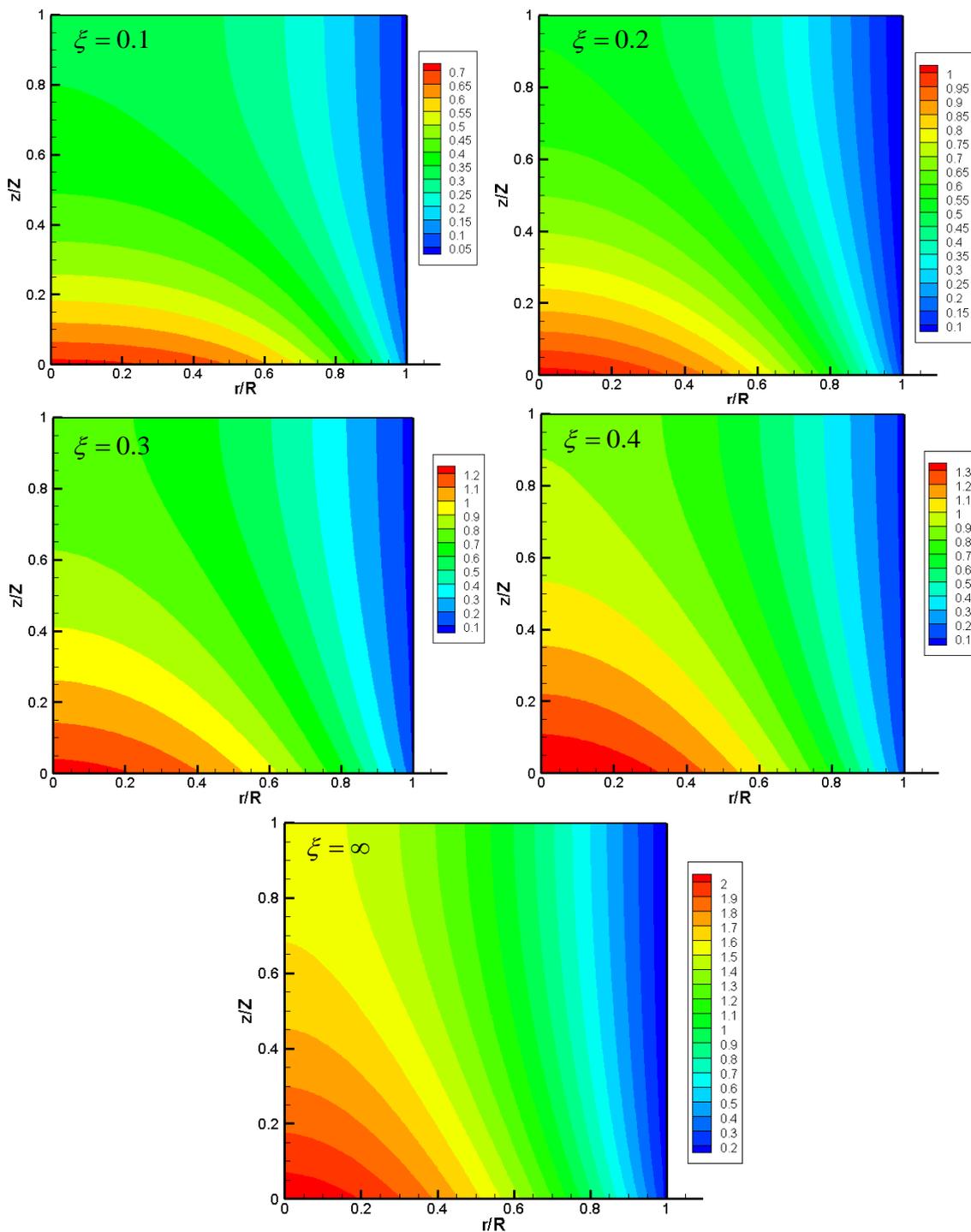


Fig. 5. Transient dimensionless isotherms in the presence of non-dimensional volumetric heat generation source ($Q^* = 2$) for different instants ξ (Cylindrical case)

In order to analyze the effect of the non-dimensional Biot number, steady state non dimensional temperature radial (Figure 6) and axial (Figure 7) is plotted for the case of axisymmetric geometry with BCs of Figure 4. We notice that radial and axial are more enhanced in presence of smallest Biot number.

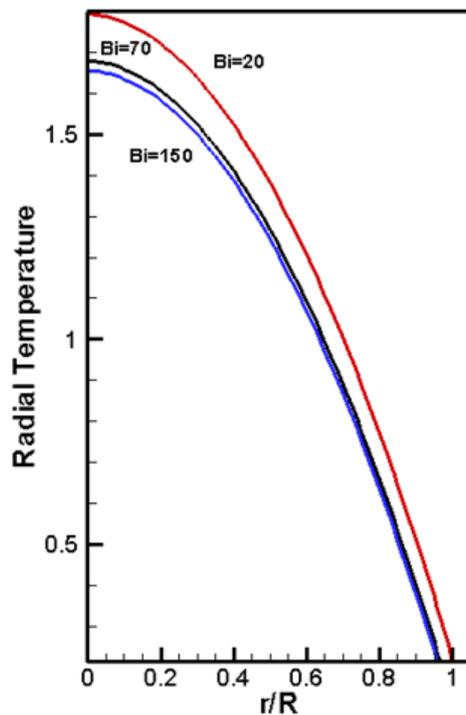


Fig. 6. Steady state dimensionless radial temperatures in the presence of non-dimensional volumetric heat generation source ($Q^* = 2$) for different Biot numbers (Cylindrical case)

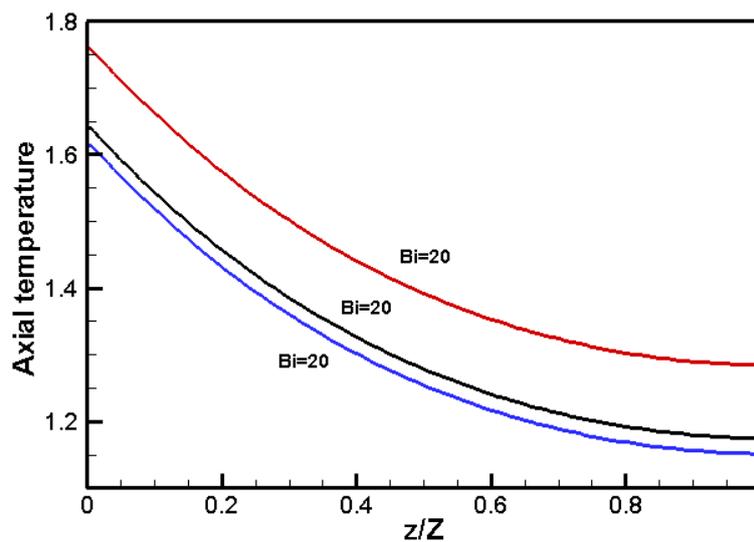


Fig. 7. Steady state dimensionless axial temperatures in the presence of non-dimensional volumetric heat generation source ($Q^* = 2$) for different Biot numbers (Cylindrical case)

Because LBM is time varying mesoscopic approach, we highlight in Figure 8, the time evolution of the dimensionless temperature at $(r/2R, z/2Z)$. We notice that temperature increases with time. The steady state temperature is reached at roughly time=15000.

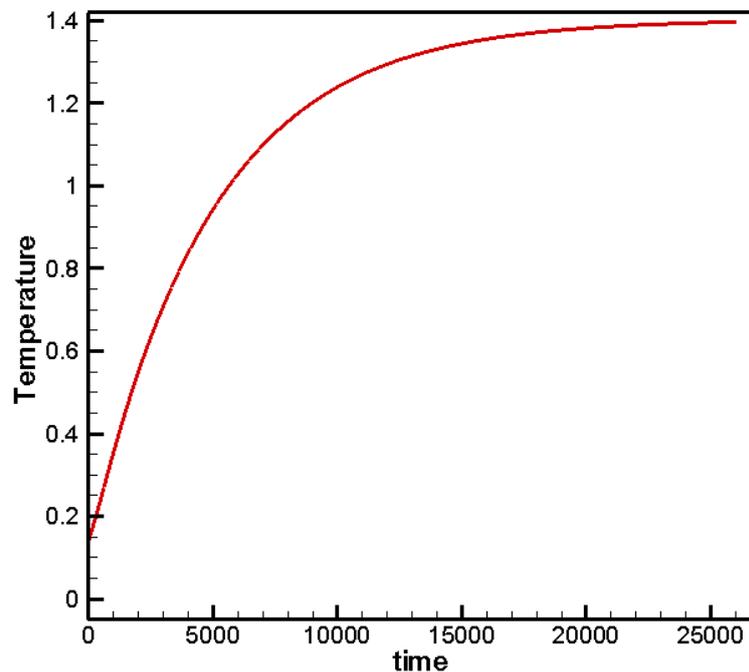


Fig. 8. Time evolution of the temperature at the centerline of the axisymmetric cavity

5. Conclusions

After good validation, LBM is extended to simulate numerically a complex geometry with mixed BCs in order to solve transient heat conduction problems in cylindrical media in the presence of heat generation effect subjected to convective boundary condition in lateral surface. Bottom wall is subjected to hot heat flux and top one is at cold heat flux. The present code shows a great stability to deal with different sets of mixed BCs; namely constant temperature, flux boundary conditions and convective boundary conditions. The effect of volumetric heat source in the cylindrical cavity is highlighted. The present numerical code achieves an efficient stability, that make it a crucial future tool to predict heat transfer and fluid flow characteristics for convection radiation engineering energy problems

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