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ORIGINAL ARTICLE

Physicochemical characteristic of neodymium oxide-based catalyst for *in-situ* $CO₂/H₂$ methanation reaction

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Abstract Carbon dioxide emission to the atmosphere is worsened as all the industries emit greenhouse gases (GHGs) to the atmosphere, particularly from refinery industries. The catalytic chemical conversion through methanation reaction is the most promising technology to convert this harmful CO2 gas to wealth CH4 gas for the combustion. Thus, supported neodymium oxide based catalyst doped with manganese and ruthenium was prepared via wet impregnation route. The screening was initiated with a series of Nd/Al_2O_3 catalysts calcined at 400 °C followed by optimization with respect to calcination temperatures, based ratios loading and various Ru loading. The Ru/Mn/ Nd $(5:20:75)/A₁O₃$ calcined at 1000 °C was the potential catalyst, attaining a complete CO₂ conversion and forming 40% of CH_4 at 400 °C reaction temperature. XRD results revealed an amorphous phase with the occurrence of active species of $RuO₂$, $MnO₂$, and $Nd₂O₃$, and the mass ratio of Mn was the highest among other active species as confirmed by EDX. The ESR resulted in the paramagnetic of Nd^{3+} at the g value of 2.348. Meanwhile nitrogen adsorption (NA) analysis showed the Type IV isotherm which exhibited the mesoporous structure with H3 hysteresis of slit shape pores. 2018 King Saud University. Production and hosting by Elsevier B.V. This is an open access article under the CC BY-NC-ND license [\(http://creativecommons.org/licenses/by-nc-nd/4.0/](http://creativecommons.org/licenses/by-nc-nd/4.0/)).

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1. Introduction

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Today's natural gas is one of the fastest components of energy consumption in the world. The requirement energy was constantly for household activities, electricity and transportation [\[1,2\]](#page-8-0). For Malaysia, natural gas is the future energy and these

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are ensured by large reserves of Malaysia and higher strength with large gas reserves in the neighboring countries [\[3\]](#page-8-0). In 2001, the country exported 49.7% of natural gas liquefied natural gas (LNG) to Japan, South Korea and Taiwan under long-term contracts [\[4\]](#page-8-0). However, the presence acid gas of carbon dioxide in natural gas will not only corrode the pipeline, lower the quality of natural gas and reduce the value of natural gas in the market but also can be harmful to the environment. When burning, untreated natural gas will release $CO₂$ gas, which is considered as the main greenhouse gas in the environment [\[5\]](#page-8-0). The release of the greenhouse gases affects the climate changes and human health. Therefore, it is necessary to develop a technology that will enable us to use fossil fuels while reducing emissions of greenhouse gases. Among other techniques, membrane technology is selected as the most practical technology. However, these methods are not effective if it involves high content of $CO₂$ gas and low selectivity toward toxic gas separation. The high cost that needed at all stage of providing customers with natural gas will be a burden to our government [\[6\]](#page-8-0). Because of these issues, catalytic methanation reaction has been designed and proposed due to its effectiveness to simultaneously convert $CO₂$ to $CH₄$ gas, assisted with heterogeneous catalyst $[7-9]$. In the purge of natural gas, carbon dioxide conversion to methane is an important process whereby hydrogen gas is used together with carbon
dioxide gas through the methanation process as shown in
Eq. (1) below [10].
 $CO_2 + 4H_2 \xrightarrow{\text{catalyst}} CH_4 + 2H_2 O$ (1) dioxide gas through the methanation process as shown in Eq. (1) below $[10]$.

$$
CO_2 + 4H_2 \xrightarrow{\text{caauss}} CH_4 + 2H_2 O \tag{1}
$$

The important requirement for selecting the correct catalyst system lies in its ability to receive and activate $CO₂$. Moreover, the acidic properties of $CO₂$ require the use of catalyst system with the Lewis basic properties. These requirements are apparently suitable with some transition metal oxides and lanthanide oxides. Their acid and redox properties can be improved by adding other oxides [\[11,12\]](#page-8-0). The investigation was conducted by Wang et al. $[13]$ who found that the $CO₂$ adsorption strength was controlled by the Lewis base of the catalyst, the center of the metal surface d-band, and charge transfer from the metal surface to the chemisorbed $CO₂$ [\[14\].](#page-8-0) The conventional nickel based catalyst has been widely used before due to low cost however, this catalyst will give higher $CO₂$ conversion only at high reaction temperature and also sensitive toward chemical attack by forming cokes. Therefore, recently among catalysts used, lanthanide oxide has been widely employed as a based in methanation reaction such as cerium, lanthanum, samarium, and praseodymium. Recently, researchers have successfully studied the potential of cerium as an oxygen storage vacancy in which higher CO_2 conversion (97.73%) and 91.31% CH4 formation were achieved using Ru/Mn/Ce $(5:30:65)/A₂O₃$ catalyst in flue gases [\[15\]](#page-8-0) whereas Ru/Mn/Ce $(5:35:60)/A1_2O_3$ performed 100% CO₂ conversion and 80% $CH₄$ formation for $CO₂$ methanation in simulated natural gas [\[16\].](#page-8-0) Other than cerium, samarium also has been utilized as a based catalyst in $CO₂$ methanation reaction with 100% $CO₂$ conversion and 93.46% CH₄ formation under molar ratio of 4:1 (H_2 :CO₂) [\[17\]](#page-8-0). Similarly, the CO₂ conversion and CH₄ formation were also investigated using praseodymium and lanthanum oxides as a based in methanation reaction with 100% $CO₂$ conversion and 41% $CH₄$ formation [\[8,18\]](#page-8-0). The potential lanthanum as a promoter also has been further investigated by Wierzbicki et al. [\[19\]](#page-8-0) and they concluded that medium strength of basic site in rare earth metal has affected the $CO₂$ adsorption capacity by improving the reducibility of active species and weakening the interaction between metal. The optimum loading of La was considered as an important aspect that affect the reducibility and increase the basicity of the catalyst in methanation reaction [\[20\]](#page-8-0).

Previously, neodymium is one of lanthanide oxide which provides a good performance in electrical and optical properties [\[21,22\].](#page-8-0) Long and Wan [\[23\]](#page-8-0) have investigated the activity of neodymium oxide doped with strontium fluoride for oxidative coupling of methane. It was found that the addition of $Nd₂O₃$ into SrF₂ lattice has increased the basicity, conductivity and dispersion of surface active sites. However, the methane conversion was increased from 26.6% to 33.7% at 700 $^{\circ}$ C with GHSV = $20,000$ h⁻¹. In addition, neodymium also has been used as a dopant in methanation [\[24\]](#page-8-0) in which the addition of small amount of neodymium has stabilized the nickel oxide against degradation of its textural properties and gave a complete $CO₂$ conversion at 350 °C. Nevertheless, up to the present time, there was no literature reporting on the use of neodymium oxide as a based catalyst in methanation reaction. The $CO₂$ conversion using cobalt doped with ruthenium was also studied by Zhu et al. [\[25\].](#page-8-0) The performance of cobalt doped with ruthenium showed that the selectivity of $CH₄$ was higher ($>90\%$) at 200 °C as compared to monometallic cobalt catalyst which only gave 50% CH₄ selectivity at 300 °C. This study showed that the addition of Ru to cobalt oxide has enhanced the performance of the respective catalyst. Therefore, the present study focuses on the synthesis, physicochemical properties and catalytic activity of neodymium doped manganese with ruthenium as co-dopant and evaluation of its promoting effect toward $CO₂$ methanation reaction.

2. Experimental

2.1. Synthesis of $Ru/Mn/Nd/Al_2O_3$

The supported $Ru/Mn/Nd$ (5:20:75)/ Al_2O_3 catalysts with various calcination temperatures were synthesized by means of incipient wetness impregnation technique using manganese nitrate, $MnNO₃$ as the dopant and ruthenium (III) chloride hydrate, $RuCl_3 \tH_2O$ as co-dopant. In a typical synthesis, neodymium (III) nitrate hexahydrate (5.00 g) was dissolved in 4 mL distilled water and mixed with a 2.29 g of $MnNO₃$ and 0.23 g RuCl₃ with 10 mL of distilled water. Next, 3 mm of alumina beads with surface area, $253 \text{ m}^2/\text{g}$ was immersed in the mixed solution for 24 h. Then, the supported catalysts were dried in the oven at $80-90$ °C for 24 h and followed by calcination in the furnace under atmosphere at $400 \degree C$, $700 \degree C$, 800 °C, 900 °C, 1000 °C, and 1100 °C for 5 h at a flow rate of 10 $\mathrm{C/min}$. [Table 1](#page-2-0) shows the composition of each amount of based, dopant and co-dopant at various temperatures.

2.2. Catalytic testing

The catalytic testing of $CO₂$ methanation was performed in a house-built microreactor (tube length of 300 mm and tube size of 25 mm ID) equipped with Fourier Transform Infrared Nicolet Avatar 370 DTGS and operated at atmospheric pressure. The analysis was carried out using simulated natural

Table 1 Composition of synthesis neodymium oxide based catalyst at various ratios and temperatures.

Catalysts	Ratio, $\%$	Calcination temperature, $^{\circ}C$		
Nd	100	400		
Mn/Nd	40/60	400		
Mn/Nd	30/70	400		
Mn/Nd	20/80	400		
Mn/Nd	10/90	400		
Ru/Mn/Nd	5/35/60	1000		
Ru/Mn/Nd	5/30/65	1000		
Ru/Mn/Nd	5/25/70	1000		
Ru/Mn/Nd	5/20/75	400, 700, 800, 900,		
		1000, 1100		
Ru/Mn/Nd	5/15/80	1000		
Ru/Mn/Nd	10/15/75	1000		
Ru/Mn/Nd	15/10/75	1000		

gas with a composition of 20% for $CO₂$ and 80% for $H₂$ with ratio (1:4) and flow rate of 50 mL/min in an isothermal tube furnace. Each trial was tested on a new catalyst sample for the purpose of preventing any ambiguous results due to loss of activity or any changes that might occur during reactions that cannot be retained by regeneration. Prior to the catalytic testing, catalysts are first subjected to air pruning at $100 \degree C$ for 30 min in order to activate the catalysts. After cooling process at room temperature, the reactant gas was introduced into the microreactor system without catalyst as a calibration. Thereafter, the reactant gas was passed through the catalyst and the temperature was elevated to the desired reaction temperatures. The product stream was collected in FTIR sample cells with KBr windows embedded and scanned using FTIR Nicolet Avatar 370 DTGS spectrophotometer. FTIR spectra were recorded in the range of $4000-450$ cm⁻¹ at 5 scan resolutions to ensure better signal to noise ratio. The GHSV was kept fixed at 636 mL g^{-1} h⁻¹ and methane formation is determined by Hewlett-Packard 6890 Series GC System (Ultra 1) with nominal column. Helium gas was used as a carrier gas with a flow rate of 20 mL/min at 75 kPa, and using Flame Ionization Detector (FID) with the injection port temperature at 150 °C, detection temperature at 310 °C and oven temperature at 40 °C. The catalyst was first preheated at 100 °C for 1 h to remove the moisture and hence activate the catalyst. The measurements were done at reaction temperatures of 100° C, 200 °C, 300 °C and 400 °C. The percentage of CO_2 conversion calculation is shown in Eq. (2) [\[26\]](#page-8-0).

$$
\% \text{ Yield of CH}_4 = \frac{[CH_4] \text{ from GC}}{\% \text{ Conversion of CO}_2} \times 100\% \tag{4}
$$

2.3. Characterization of catalysts

X-ray diffraction (XRD) was analyzed using Diffractometer D5000 Siemens Crystalloflex with Cu K_{α} radiation $(\lambda = 1.54060 \text{ Å})$ at a scanning range of 20 range $10^{\circ} - 80^{\circ}$. Field emission scanning electron microscopy (FESEM) images were obtained on a Zeiss Supra 35 VP with energy of 15.0 kV coupled with EDX analyzer. Samples were blasted using an electron gun with a tungsten filament under 25 kV resolution to obtain the required magnification image. The BET surface area was determined by nitrogen adsorption/desorption at -196 °C using Micromeritics ASAP 2010. The samples were degassed at 120 °C for 5 h and left under vacuum to cool down at ambient temperature before analysis. The electrons spin resonance (ESR) spectrometer was conducted by inserting sample powder into a $4 \text{ mm} \times 0.5 \text{ mm}$ quartz tube using Thermo-Flex3500 model. ESR measurements are carried out in the temperature range between 4.5 K and 300 K using a 100 kHz modulation frequency and a 2 G configuration amplitude. The microwave capacity can be reduced in the range between 200 mW and $0.2 \mu \text{W}$ and was adjusted in such a way so that it does not have any saturation effect. The reducibility and $CO₂$ desorption of the catalyst was performed by temperature programmed reduction (TPR) and $CO₂$ -temperature programmed desorption $(CO₂-TPD)$ using Micromeritics Autochem 2920. The TPR analysis was conducted by heating the catalyst up to 1000 °C under 10% H_2 in a quartz U-tube (internal diameter = 10 mm) and cleaned under Ar flow of 20 mL min at 150 °C for 2 h. The CO_2 -TPD was completed by placing an appropriate amount of catalyst sample in a quartz U-tube (internal diameter $= 10$ mm) and was cleaned under He flow for 20 mL/min at 150 °C for 1 h. The TGA-DTA curves were obtained by TGA-SDTA 851 Mettler Toledo simultaneous thermal analyzer.

3. Results and discussion

3.1. Catalytic activity measurement using FTIR analysis

The activities of a series of alumina supported neodymium oxide based catalysts for the $CO₂$ conversion are displayed in [Fig. 1.](#page-3-0) From the screening, the bimetallic oxide of Mn/Nd

Meanwhile, the methane formation and selectivity to methane are calculated using Eqs. (3) and (4) below:

% Selectivity to
$$
CH_4 = \frac{[CH_4] \text{ from GC}}{[Converted CO_2] \text{ from FTIR}} \times 100\%
$$
 (3)

 $(30:70)/A1₂O₃$ catalyst exhibited the highest $CO₂$ conversion with 38% as compared to monometallic oxide catalysts. The higher loading of 70 wt% of Nd immersed in the catalyst would enhance the activity of hydrogenation to produce methane as the increasing amount of active surface site in the supported catalyst [\[27\].](#page-8-0) However, excessive loading of

Fig. 1 $CO₂$ conversion over various ratios of Mn/Nd catalyst supported with Al_2O_3 calcined at 400 °C for 5 h.

Nd deteriorates the catalytic activity, decreasing in $CO₂$ conversion which might due to blockage of the active site.

Therefore, the inferior performance of supported bimetallic oxide catalysts has encouraged the study of trimetallic oxide. The addition of Ru as co-dopant improved the catalytic activity on $CO₂$ conversion as the presence of Ru favors the reduction process and dispersion on the surface of the catalyst. Overall, the CO_2 conversion obtained for $Ru/Mn/Nd$
(5:40:55)/ Al_2O_3 , $Ru/Mn/Nd$ (5:35:60)/ Al_2O_3 , $Ru/Mn/Nd$ $(5:40:55)/Al_2O_3$, Ru/Mn/Nd $(5:35:60)/Al_2O_3$ $(5:30:65)/A_2O_3$, Ru/Mn/Nd $(5:25:70)/A_2O_3$, Ru/Mn/Nd $(5:20:75)/A_2O_3$ and Ru/Mn/Nd $(5:15:80)/A_2O_3$ calcined at 400 °C were 20%, 28%, 36%, 39%, 45% and 32% at 400 °C reaction temperatures, respectively. From the earlier screening, it was observed that $Ru/Mn/Nd$ (5:20:75)/ Al_2O_3 showed a promising catalytic activity among other catalysts. Therefore, this potential catalyst has been further investigated with various calcination temperatures.

Fig. 2 shows the effect of calcination temperature of Ru/ Mn/Nd $(5:20:75)/\mathrm{Al}_2\mathrm{O}_3$ catalyst on CO_2 conversion. It can be seen that the $CO₂$ conversion reached 100% at 400 °C reaction temperature using a catalyst that was calcined at $1000 \,^{\circ}\text{C}$. Higher calcination temperature was more promising due to good dispersion of $Nd₂O₃$ on the catalyst surface. This is in good agreement with Duhan and Aghamkar who have concluded that calcination above 900 \degree C would activate the active species present on the catalyst surface [\[28\]](#page-8-0). Therefore, increasing calcination temperature would increase the catalytic activity in methanation reaction.

 $Ru/Mn/Nd$ (5:20:75)/ Al_2O_3 catalyst containing different Nd based ratios were investigated to obtain the optimum based loading to enhance the catalytic activity. The $CO₂$ conversions at 400 $^{\circ}$ C reaction temperature are shown in Fig. 3, from which it can be seen that the catalytic performance was

Fig. 2 Catalytic screening of Ru/Mn/Nd $(5:20:75)/Al_2O_3$ catalyst calcined at various calcination temperatures for 5 h.

Fig. 3 Catalytic screening of $Ru/Mn/Nd/Al_2O_3$ catalyst calcined at 1000 C with various metal oxides ratios at 400 C reaction temperature.

obviously improved by the appropriate ratio of Nd based catalyst (75 wt%). The $CO₂$ conversion increased from 82% to 100% with the increase of Nd ratio from 60 wt% to 75 wt%. however, it declined to 84% as the Nd ratio increased to 85 wt%. The excessive amount of Nd might have blocked the active site as reported by He et al. [\[29\]](#page-8-0) who found that the agglomeration of particle was occurred when increasing the amount of based catalyst resulting in the inhibition of the growth of the crystal which then blocked the surface active site. Perkas et al. [\[30\]](#page-8-0) also stated that the lowest catalytic activity of catalyst was obtained when highest amount of based loadings was present and preventing the activation of the reagents.

The catalytic activity of $Ru/Mn/Nd/Al_2O_3$ catalyst was further explored by varying ruthenium loadings $(5 \text{ wt\%}, 10 \text{ wt\%})$, and 15 wt%). The $CO₂$ conversion of each catalyst started to drastically increase at $250 \degree C$ reaction temperature. In summary, the optimum ruthenium loadings to achieve higher $CO₂$ conversion was 5 wt% as the addition of small amount of noble metals could promote catalyst to achieve superior activity for methane formation [\[31\].](#page-8-0) This phenomenon was also in line with Zamani et al. [\[32\]](#page-8-0) which reported that the addition of 5 wt% of ruthenium to based catalyst could enhance the catalytic activity by achieving almost 100% of $CO₂$ conversion. As shown in Fig. 4, it was observed that the incorporation of ruthenium into the manganese oxide catalyst showed a positive effect on the methanation reaction. This is similar to the finding by Panagiotopoulou et al. [\[33\]](#page-8-0) where $CO₂$ methanation was strongly favored with the increasing of Ru content. Therefore, $Ru/Mn/Nd$ (5:20:75)/Al₂O₃ catalyst was the best catalyst calcined at 1000 °C.

Fig. 4 CO_2 conversion of Ru/Mn/Nd $(x:y:75)/A1_2O_3$ catalyst calcined at $1000\,^{\circ}\text{C}$ for 5 h with various ruthenium loadings $(x = 5\%, 10\%, 15\%)$.

Fig. 5 CO_2 conversion of Ru/Mn/Nd (5:20:75) catalyst at various catalyst loadings calcined at $1000 \degree C$ for 5 h.

Optimization parameter with various loading of catalyst during reaction was also investigated as illustrated in Fig. 5. At reaction temperature of 200 \degree C, the CO₂ conversion started to increase drastically for each catalyst dosage. The highest $CO₂$ conversion was achieved with 7 g of catalyst dosage. This observation might be due to the increase in active site which was affected by the increase of catalyst loading. This finding was in a good agreement with Lu et al. [\[34\]](#page-8-0) who found that the smaller amount of loading based exhibited a lower degradation rate due to inadequate catalytic active sites during the reaction.

3.2. Characterization

3.2.1. X-ray diffractogram (XRD) analysis

Diffractogram of $Ru/Mn/Nd$ (5:20:75)/ Al_2O_3 catalyst is shown in Fig. 6 by different calcination temperatures; 900 °C, 1000 °C and $1100 \, \text{°C}$, respectively. The X-ray diffractograms pattern for all prepared catalysts exhibited polycrystalline peak. At calcination temperature of $900\,^{\circ}\text{C}$, four peaks were observed and assigned to cubic Al_2O_3 which was emerged at 2 θ of 39.42° , 45.79° , 60.54° and 66.85° . In addition, the peaks of $RuO₂$ with tetragonal phase were observed at 2 θ of 28.10 and 36.53°, while Nd_2O_3 with cubic phase at 2 θ of 28.61° and 33.21°. This result was in good agreement with Yadav et al. $[35]$ who stated that $Nd₂O₃$ with cubic phase can only be seen when the catalyst was calcined at temperature more

than 200 °C. Another three small peaks observed at 34.83° . 42.90 $^{\circ}$, and 54.70 $^{\circ}$ were corresponded to the cubic phase of Mn_2O_3 . Similar species with the respected 2 θ was observed for the diffractogram of $1000 \,^{\circ}\text{C}$ calcination temperature. However, higher intensity for the Nd₂O₃ ($2\theta = 33.21^{\circ}$) and Mn_2O_3 (2 θ = 34.83°, 42.90°) can be remarkably seen. The intensity of these peaks further decreased when increasing the calcination temperature up to $1100 \degree C$. Therefore, it can be concluded that Mn_2O_3 and Nd_2O_3 species are the major active species that contribute to higher catalytic activity at 1000 °C calcination temperature.

3.2.2. Electron spin resonance (ESR)

ESR analysis was used to examine catalyst with unpaired spins which it interacts to each other, coherent electromagnetic radiation and the magnetic moments of neighboring nuclei [\[36\]](#page-8-0). The broad spectrum obtained was due to polycrystalline property of the catalyst resulted in wide distribution of the electron spin orientation [\[37\]](#page-8-0) as the catalyst was in the polycrystalline structure as observed in XRD (Fig. 6). The g-value of 4.36 was attributed to the Al_2O_3 from the catalyst support while g-value of 2.35 exhibited ''wing" on both sides was attributed to Nd^{3+} from Nd_2O_3 compound [\[38,39\],](#page-8-0) as shown in Fig. 7. This result was reinforced with XRD analysis which showed the presence of $Nd₂O₃$ species. Comparing with XRD analysis, it can be observed that the peak of $Nd₂O₃$ was higher at $1000 \, \text{°C}$, hence causing the increase in the amount of paramagnetic species which lead to the increment in its intensity as well as catalytic activity as compared to 900 $^{\circ}$ C and 1100 $^{\circ}$ C.

3.2.3. Temperature programmed reduction (TPR)

The H_2 -TPR profile for Ru/Mn/Nd (5:20:75)/Al₂O₃ are shown in Fig. 8. At calcination temperature of $1000 \degree C$, four

Fig. 7 ESR spectra of $Ru/Mn/Nd$ (5:20:75)/Al₂O₃ catalyst calcined at (a) $900 \degree C$, (b) $1000 \degree C$, and (c) $1100 \degree C$ for 5 h.

Fig. 6 XRD diffractogram of Ru/Mn/Nd $(5:20:75)/A1_2O_3$ catalyst calcined at various temperatures; $900\,^{\circ}\text{C}$, $1000\,^{\circ}\text{C}$ and 1100 \degree C for 5 h.

Fig. 8 H₂-TPR profile of Ru/Mn/Nd $(5:20:75)/Al_2O_3$ calcined at 1000 °C and 1100 °C for 5 h.

reduction peaks were observed at $189.9 \degree C$, $461.4 \degree C$, $724.5 \degree C$ and 879.2 °C. The first reduction peak at 189.9 °C was attributed to the reduction temperature for ruthenium species with total hydrogen consumption of 0.155 mmol/g STP. According to Li et al., a broad shoulder peak at $180-300$ °C was attributed to the $RuO₂$ reduction to metal Ru [\[40\]](#page-9-0) and this observation was also detected in XRD analysis. The second reduction peak at 461.4 °C with H_2 consumption of 0.09 mmol/g at STP was assigned to the reduction of Mn^{4+} to Mn^{2+} species which was in agreement with Peluso et al. [\[41\]](#page-9-0). Meanwhile, the third reduction peak (724.5 °C) was ascribed to the surface reduction of mixed metal oxides with total H₂ consumption was 0.018 mmol/g STP $[42]$. Meanwhile, 879.2 °C was assigned as the reduction of bulk oxygen of $Nd₂O₃$ with $H₂$ consumption was 0.018 mmol/g STP. Introduction of Nd^{3+} cation into the catalyst improves the mobility of oxygen into the lattice [\[42\],](#page-9-0) therefore it contributed to higher catalytic activity at this calcination temperature. For calcination temperature of 1100° C, all the reduction peaks observed showed a similar trend as those at 1000 °C. Peak shift occurs at higher temperatures up to $1100\degree C$ due to strong interactions between metal oxides and carriers, therefore higher temperatures needed by active species to be reduced [\[43\]](#page-9-0). From the TPR profile, no reduction peak of γ -Al₂O₃ was observed, proving that γ -Al₂O₃ is an inert support.

3.2.4. CO_2 -temperature programmed desorption (CO_2 -TPD)

The CO_2 -TPD profile of Ru/Mn/Nd (5:20:75)/Al₂O₃ revealed one desorption peaks at 148.2 °C with 1.56 mmol/g STP as shown in Fig. 9. It indicated that the peak was assigned to $CO₂$ adsorbed on the manganese species. The lowest desorption temperature was due to desorption of the weakest bonding mode of $CO₂$ onto a weak basic site on catalyst surface [\[42,44\].](#page-9-0) Consequently, it increased the catalytic activity of the catalyst at 1000 °C calcination temperature. Peak area at a lower temperature of $148.2 \degree C$ indicated that the chance for methane formation was higher.

3.2.5. Nitrogen adsorption (NA) analysis

The adsorption–desorption curve of Ru/Mn/Nd (5:20:75)/ Al_2O_3 catalyst is depicted in Fig. 10. From the graph, the hysteresis formed around above 0.5P/Po suggested the type IV isotherm and H_3 hysteresis loop which is characteristic of solids consisting of non-rigid aggregates of plate-like particles forming a non-uniform slit-shaped pores [\[45,46\].](#page-9-0) The formations of the non-uniform channel within the pores would

Fig. 9 CO_2 -TPD curve of Ru/Mn/Nd (5:20:75)/Al₂O₃ calcined at 1000 °C for 5 h.

Fig. 10 Isotherm plots of $Ru/Mn/Nd$ (5:20:75)/Al₂O₃ catalyst calcined at (a) 900 °C (\bullet), (b) 1000 °C (\bullet), and (c) 1100 °C (\bullet) for 5 h.

change the adsorption and desorption of the catalysts as well as increase the adsorption of active reactant [\[47\]](#page-9-0). The plot corresponds to the existence of mesopores and extension to the porous bottleneck form since monolayer was completed and the multilayer adsorption started to occur at high P/Po [\[18,48\].](#page-8-0) The obtained BET surface area at $900 \degree C$, $1000 \degree C$, and 1100 °C were 56.32 m²/g, 83.67 m²/g and 73.91 m²/g with average pore diameter of 71.31 \AA , 95.97 \AA , and 72.13 \AA respectively. These results suggested that $1000 \degree C$ is the most potential catalyst due to the higher surface area and average pore diameter which determine the higher catalytic activity as it gave space for the $CO₂/H₂$ to react on the surface of the catalyst.

3.2.6. Field emission scanning electron microscopy (FESEM)- Electron dispersion X -ray (EDX) analysis

The micrographs for $Ru/Mn/Nd$ (5:20:75)/Al₂O₃ catalysts with calcination temperatures of $900 \degree C$, $1000 \degree C$, and $1100 \degree C$ are shown in [Fig. 11.](#page-6-0) The micrographs showed an agglomeration of particles which are not homogenously affected by calcination temperature [\[49\].](#page-9-0) Some particles formed a flat slab which might attribute to the existence of $Nd₂O₃$ [\[44,50\]](#page-9-0) and supported by XRD which showed the presence of this species on the catalyst surface. At $1000\,^{\circ}\text{C}$ calcination temperature, the particles seemed to be shattered and coalesce forming a larger particle and this event is consistent with previously reported literature [\[51\]](#page-9-0), whereby addition of neodymium has led to shattered particle. This was possibly due to the porosity of alumina and oxygen vacancy of neodymium which caused the charging effects. The particle size of Ru/Mn/Nd $(5:20:75)/\text{Al}_2\text{O}_3$ catalysts calcined at 900 °C, 1000 °C, and 1100 °C is 108 nm, 123 nm, and 117 nm respectively. This particle size is larger due to lower surface area obtained from BET analysis as it form agglomeration particle.

EDX analysis gives information on the percentage of the elements existing on the sample surface, and the composition of the catalyst that was successfully coated on the support. From the [Table 2](#page-6-0), Mn was found to be higher percentage atomic ratio which might due to the higher affinity of Mn to be adsorbed on the surface. At $1000\,^{\circ}\text{C}$ calcination temperature, the atomic ratio for Nd, Ru and Mn was quite higher with 3.92%, 1.84% and 4.72%, respectively on the catalyst surface which contributed to higher activity at this temperature. This finding was supported with XRD analysis which showed a higher intensity of peak at $1000\,^{\circ}\text{C}$ compared to

Fig. 11 FESEM micrographs of Ru/Mn/Nd (5:20:75)/Al₂O₃ catalyst calcined at (a) 900 °C, (b) 1000 °C, and (c) 1100 °C for 5 h in 50,000 \times magnification.

Table 2 EDX analysis for $Ru/Mn/Nd$ (5:20:75)/ Al_2O_3 catalysts calcined at 900 °C, 1000 °C, and 1100 °C for 5 h.

Calcination	Atomic ratio $(\%)$					
temperature, $^{\circ}C$	A1		Nd	Mn	Ru	
900	32.32	46.10	2.44	4.48	0.46	
1000	36.53	48.35	3.92	4.72	1.84	
1100	31.50	51.54	3.15	4.64	0.70	

other calcination temperature. All the active species were observed in XRD analysis.

3.2.7. Thermogravimetric analysis (TGA-DTA)

The evolution of weight loss with drying or decomposition of the dried catalyst is important to determine the maximum temperature after the catalyst is completely decomposed. This analysis also serves to establish the lowest temperature at which the catalyst is thermally stable and the lowest temperature for the calcination process. Fig. 12 shows a TGA-DTA thermogram obtained for $Ru/Mn/Nd$ (5:20:75)/Al₂O₃ catalyst and the summarized results of TGA-DTA is tabulated in Table 3.

The first region of weight loss in the thermogram from 60 °C to 240 °C was attributed to the removal of bulk and physisorbed water. The first intense endothermic peak at DTA curve corresponded to the thermal desorption of water [\[52\]](#page-9-0). A broad endothermic peak appeared at $240-440$ °C from

Fig. 12 TGA-DTA thermograms of as-synthesize of Ru/Mn/Nd $(5:20:75)/Al₂O₃$ catalyst.

DTA curve, indicating the decomposition of nitrate ion that was entrapped in the pores of the support [\[53\]](#page-9-0). The peak at 320–440 \degree C was attributed to the abstraction of chemically bound water from aluminium hydroxide or the removal of structural water from the alumina [\[52\].](#page-9-0) The mass loss from 440 °C to 650 °C was attributed to the loss of surface hydroxyl molecule. The DTA curve showed an endothermic peak at around 520 °C which indicates the decomposition of water from the catalyst [\[54\]](#page-9-0). The presence of water molecule was due to the amorphous surface of the catalyst that was still covered with water and the hydrophilic nature of alumina. At 650–900 °C, an endothermic peak was observed at 860 °C in the DTA curve, indicating that the catalyst had undergone morphological and structural modifications which can be attributed to the formation of phase-pure doped oxide as reported by Ketzial et al. [\[55\].](#page-9-0) It could be concluded that pure metal oxide may have been formed after $900 \degree C$, thus suggesting that calcination temperature of above $900\,^{\circ}\text{C}$ is adequate and capable of stabilizing the respective catalyst.

3.3. Methane formation using GC analysis

The potential $Ru/Mn/Nd$ (5:20:75)/Al₂O₃ catalyst has been further investigated for methane formation using GC analysis. At room temperature, no $CH₄$ formation was observed as shown in [Fig. 13](#page-7-0) and tabulated in [Table 4.](#page-7-0) Nonetheless, the

Fig. 13 Representative of the FTIR spectra showing CO_2 and CH₄ peaks which appeared during the CO_2/H_2 methanation reaction of Ru/Mn/Nd $(5:20:75)$ /Al₂O₃ catalyst calcined at 1000 °C for 5 h.

Table 4 Testing results of in-situ reactions of methane formation over $Ru/Mn/Nd$ (5:20:75)-Al₂O₃ catalyst at 1000 °C calcination temperature.

	$\%$ Formation of CH ₄	Formation of H_2O	
RT			100.00
100	1.29	5.29	93.42
200	4.91	18.87	76.22
300	10.00	58.66	31.34
350	22.06	57.90	20.04
400	40.32	59.68	$\overline{}$

Calculation based on $CO₂$ detected via FTIR and CH₄ detected via GC.

percentage of CH4 formation increased when increasing the reaction temperature up to 400 °C [\[56,57\]](#page-9-0). During reaction temperature at 100 °C, the catalytic $CO₂$ conversion could be due to the partial oxidation reaction since that the amount of unreacted $CO₂$ was higher than the formation of $CH₄$. Yaccato et al. [\[58\]](#page-9-0) has investigated the formation of carbon monoxide as the main product at low temperature. However, in this study no CO formed at low reaction temperature due to no peak of CO observed on the FTIR spectrum (Fig. 13). It showed that $CO₂$ peak was more profound at the lower activation temperature of 300 $^{\circ}$ C. When the reaction temperature increased, the $CO₂$ peak was gradually diminished until almost $CO₂$ peaks disappeared at the catalytic reaction temperature of 400 °C. The percentage of CH₄ formation at 400 °C reaction temperature was 40.32% and the by-product formed was only water molecule [\[17,18\].](#page-8-0)

4. Conclusion

The $Ru/Mn/Nd/Al_2O_3$ catalyst was highly active in methanation reaction. Almost 100% $CO₂$ conversion and over 40% CH₄ formation were achieved on Ru/Mn/Nd $(5:20:75)/A1_2O_3$ catalyst (calcination temperature was $1000 \degree C$) at $400 \degree C$ reaction temperature under the condition of GHSV = 636 h⁻¹. XRD results indicated that the polycrystalline peaks in the spectrum with $Nd₂O₃$ and $MnO₂$ as an active species. These species were reduced over 400 °C which represented high basicity to the catalyst as observed in TPR and TPD analyses. This potential catalyst illustrated some agglomeration and undefined shape in FESEM analysis. ESR analysis showed paramagnetic properties of $Nd₂O₃$ species at 1000 °C which enhance higher catalytic activity. $Ru/Mn/Nd$ (5:20:75)/ Al_2O_3 catalyst calcined at 1000 °C could be regenerated under oxidation reaction and can be stabilized for 5 h with above 90% CO₂ conversion before deteriorated after 6 h.

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Declaration of interest

The authors report no declarations of interest.

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