# APPLICATION OF POLYPROPYLENE NANOSILICA AS ADDITIVES IN WATER BASED MUD TO IMPROVE RHEOLOGICAL PROPERTIES AND SHALE STABILITY

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# **DEDICATION**

I would like to dedicate this work of mine to my family especially my parents for always being there for me, supporting me and caring for me from the moment I opened my eyes until now.I also would like to dedicate this work to lecturers and my friends who supported and helped me directly and indirectly.

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#### ABSTRACT

Drilling in swelling clay formation is rather challenging owing to the delicate formation of the wellbore. This is mostly because of the propensity of clay to swell when in contact with water. The high reactivity of swelling clays with water causes their constituents to swell and these can cause severe drilling problems, such as damage to the production zone. Potassium chloride (KCl) has been the most typical shale swelling control additive used to formulate WBM. However, at higher concentrations of KCl in WBM, the mud separates into two phases, which are liquid and sediments, and the swelling-control activity of the KCl is short-lived in WBM. A better efficient clay swelling-control additive, such as composite of polymer and nanoparticle, might be more effective. Therefore, in this study, the efficiency of synthesized polypropylene based nanosilica composite (PP-SiO2 NC) on clay swelling was carried out and its performance was compared to KCl mud and other types of water based mud. Samples of shale from Simpang Renggam shale formation were selected and tested for swelling behaviour over five different types of WBMs, which are (i) Basic mud (ii) KCl mud (iii) PP-SiO2 NC mud, (iv) Commercial SiO2 NP mud, and (v) Mixture of KCl and PP-SiO2 NC mud. At normal temperature 80°F and elevated temperature 250 °F, PP- SiO2 NC mud gave better results in the rheological properties such as gel strength, plastic viscosity, and yield point compared to other type of WBM. Improved shale swelling inhibition were achieved at a lower concentration (0.3 -1.0 g) of synthesized PP-SiO2 NC compared to 30g conventional KCl mud, which is required to attain its optimum inhibition level. 0.6g of PP-SiO2 NC based mud alone prove to be the best formulation as it only cause shale to swell up to 7.11% compared to KCl mud at 15.3%, mixture of KCl and PP-SiO2 NC mud at 9.2%, and commercial SiO2 NP mud at 10%. Indubitably, the synthesized PP-SiO2 NC mud provide better in rheological properties at normal and elevated temperature and more efficient in minimizing clay swelling behaviour compared to other type of WBM and it has a higher propensity to prevent loss of filtrates into the formation.

#### ABSTRAK

Penggerudian di syal agak sukar kerana perlu menghadapi isu formasi yang lembut dalam lubang telaga. Ianya disebabkan oleh ciri-ciri pembengkakan syal terutama apabila bersentuhan dengan air. Kereaktifan tinggi pada syal apabila bersentuhan dengan air menyebabkan komponen pada tanah liat membengkak dan ini menyebabkan berlaku banyak masalah seperti kerosakan pada zon pengeluaran. KCl telah menjadi aditif kawalan bengkak yang paling biasa digunakan untuk merumuskan WBM. Walau bagaimanapun, pada kepekatan KCl yang lebih tinggi di WBM, lumpur itu memisahkan dua fasa, iaitu cecair dan sedimen, dan aktiviti pengendalian bengkak KCl mempunyai jangka hayat yang pendek. Aditif pengawalan bengkak tanah liat yang lebih baik, seperti komposit polimer dan nanopartikel, mungkin lebih berkesan. Dalam kajian ini, kecekapan komposit polypropylene nanosilica (PP-SiO2 NC) pada kebengkakan tanah liat dijalankan dan prestasinya dibandingkan dengan lumpur KCl and lumpur WBM yang lain. Sampel syal dari Simpang Renggam telah dipilih dan diuji untuk tingkah laku bengkak ke atas lima jenis WBM yang berbeza, iaitu (i) Lumpur asas (ii) Lumpur KCl (iii) Lumpur PP-SiO2 NC (iv) Lumpur komersial SiO2 NP, dan (v) Lumpur campuran KCl dan PP-SiO2 NC. Pada suhu normal 80 °F dan suhu tinggi 250 °F, lumpur PP-SiO2 NC memberikan hasil yang lebih baik dalam sifat reologi seperti kekuatan gel, kelikatan plastik, dan titik hasil berbanding dengan jenis WBM yang lain. Perencatan bengkak syal yang lebih baik dicapai pada kepekatan yang lebih rendah (0.3 -1.0 g) lumpur PP-SiO2 NC yang disintesis berbanding dengan 30g lumpur KCl, yang diperlukan untuk mencapai tahap perencatan optimumnya. 0.6g lumpur PP-SiO2 NC menjadi formulasi terbaik kerana ia hanya menyebabkan syal membengkak sehingga 7.11% berbanding lumpur KCl pada 15.3%, campuran KCl dan PP-SiO2 NC lumpur pada 9.2%, dan lumpur komersial SiO2 NP pada 10%. Secara tidak langsung, lumpur PP-SiO2 NC yang disintesis memberikan prestasi lebih baik dalam sifat rheologi pada suhu normal dan suhu tinggi dan lebih berkesan dalam mengurangkan pembengkakan tanah liat berbanding dengan jenis WBM yang lain dan ia mempunyai kecenderungan yang lebih tinggi untuk mencegah kehilangan filtrat ke dalam formasi.

# TABLE OF CONTENTS

## TITLE

DE	ii			
DE	iii			
AC	iv			
AB	STRACT	v		
AB	STRAK	vi		
TA	BLE OF CONTENTS	vii		
LIS	T OF TABLES	xi		
LIS	T OF FIGURES	xii		
LIS	T OF ABBREVIATIONS	XV		
LIS	T OF APPENDICES	xvi		
CHAPTER 1	INTRODUCTION	1		
1.1	Background of Study	1		
1.2	Problem Statement	4		
1.3	Objectives	5		
1.4	.4 Scope of Study			
1.5	Significance of the Study	6		
CHAPTER 2	LITERATURE REVIEW	9		
2.1	Overview on Shale	9		
	2.1.1 Shale Types	9		
	2.1.2 Shale Mineralogy	13		
2.2	X-ray Diffraction Analysis	16		
2.3	Cation Exchange Capacity	17		
2.4	Shale Swelling	19		
2.5	Shale Dispersion	22		
2.6	Shale Hydration	23		
2.7	Borehole Instability	25		

	2.7.1	Stages of Shale Instability	26
2.8	Shale S	Stabilizing Additives	29
	2.8.1	Salts	30
	2.8.2	Polymer With Special Affinity	32
2.9	Deficit	s of Potassium Chloride	37
	2.9.1	Dehydration of Salts	37
	2.9.2	Weak Bonds with Shale Particles	38
	2.9.3	Insoluble Residue of KCl Salts	38
2.10	) Polypr	opylene	39
2.11	Nanosi	llica	40
2.12	Applic 2	ations of Polymer Nanocomposite in Drilling Fluids	42
	2.12.1	Application of Polymer Nanocomposites for Enhanced Rheological Properties	43
	2.12.2	Application of Polymer Nanocomposites for HPHT Environments	47
	2.12.3	Application of Polymer Nanocomposites for Shale Swelling	50
2.13	Key Su	ammary	52
CHAPTER 3	RESE	ARCH METHODOLOGY	55
3.1	Introdu	action	55
3.2	Framev	work	56
3.3	Synthe	sis of Polymer-Nano Composite Suspension	56
3.4	Charac	eterization of PP-SiO2 Nanocomposite	58
	3.4.1	Fourier Transform Infrared Spectroscopy (FTIR)	58
	3.4.2	Field Electron Scanning Microscopy (FESEM)	58
	3.4.3	Thermal Gravimetric Analysis (TGA)	58
3.5	Prepara	ation of Drilling Mud	59
	3.5.1	Preparation of Basic WBM	59
	~ ~ ~	Preparation of Polypropylene Based Silica	
	3.5.2	Nanocomposite Based Mud	61
3.6	3.5.2 Rheolo	Nanocomposite Based Mud	61 61
3.6	3.5.2 Rheolo 3.6.1	Nanocomposite Based Mud ogical Measurement Determination of Mud Weight	61 61 62

	3.6.3	Determination of Plastic Viscosity, Yield Point and Gel Strength	63
	3.6.4	Determination of Mud Filtration and Filter Cake Thickness	65
	3.6.5	High Temperature Roller Oven	66
3.7	XRD '	Test of Shale	67
3.8	Swelli	ing Test Using Linear Swell Meter (LSM)	68
	3.8.1	Linear Swell Meter Operation	69
	3.8.2	Shale Pellet Preparation	69
	3.8.3	Installation of Specimen Plugs on Fann Linear Swell Meter Measuring Head	74
	3.8.4	Numerical Measurement	76
	3.8.5	Limitations of the Linear Swelling Meter	76
CHAPTER 4	RESI	ILTS AND DISCUSSIONS	79
4.1	Introd	uction	79
4.2	Chara	cterization analysis of PP-SiO2 nanocomposite	79
	4.2.1	Fourier Transform Infrared Spectroscopy (FTIR) Analysis	79
	4.2.2	Field Emission Scanning Electron Microscopy (FESEM) Analysis	81
	4.2.3	Thermal Gravimetric Analysis (TGA)	83
4.3	Chara	cterization Analysis of Shale Core	85
	4.3.1	X-ray Diffraction (XRD) Analysis	85
4.4	Rheol	ogical Properties Analysis	86
	4.4.1	Effect of Synthesized PP-SiO2 composite over Plastic Viscosity of Water- Based Drilling Fluids	88
	4.4.2	Effect of Synthesized PP-SiO2 composite over Yield Point of Water- Based Drilling Fluids	89
	4.4.3	Effect of Synthesized PP-SiO2 Composite Over 10-s and 10-min Gel Strength of Water- Based Drilling Fluids	91
	4.4.4	Effect of Synthesized PP-SiO2 Composite Over Filtrate Loss Volume of Water-Based Drilling Fluids	93
4.5	Shale	Swelling Analysis	95
		0	20

	4.5.1	Effect Convent	of tiona	Synthesized ll KCl over Sha	PP-SiO2 ale Swelling	NC	and	95
	4.5.2	Effect of Concent Shale Sy	of Co ratio welli	ommercial SiC on of Synthesi ng	2 and Thre zed PP-SiC	e Diff 2 NC	erent over	96
CHAPTER 5	CON	CLUSIO	N A	ND RECOMN	/IENDATI(	ONS		99
5.1	Conclu	usion						99
5.2	Recon	imendatio	ons					100
REFERENCE	S							101
Appendices								105-106

# LIST OF TABLES

#### TABLE NO. TITLE PAGE Table 2.1 Compositions of shale from Mexico, Norway and Malaysia, determined by XRD 13 Table 2.2 Major clay minerals properties 15 Table 2.3 Cation exchange capacity (CEC) values of clay minerals. 17 Table 2.4 Classification of shale problem 23 Table 2.5 Typical shale problems in drilling operation 28 Table 2.6 Physical and Chemical Properties of Polypropylene 39 Table 2.7 Physical and chemical properties of nanosilica 40 Table 2.8 PNCs rheological performance in drilling operations 44 Table 2.9 PNCs performance under HPHT in drilling operations 49 Table 3.1 Formulation of Drilling Mud System 60 60 Table 3.2 Composition of Drilling Mud system Table 3.3 **Rheological Properties Test** 61 Table 4.1 Rheological properties of all mud sample at room temperature (80 °F) 87 Table 4.2 Rheological properties of all mud sample at high temperature (250 °F) 87

# LIST OF FIGURES

FIGURE NO	. TITLE	PAGE
Figure 2.1	Main compositions of shale	10
Figure 2.2	(a) Kaolinite structure, (b) SEM image of kaolinite	11
Figure 2.3	(a) Illite structure, (b) SEM Image of illite	11
Figure 2.4	(a) Montmorillonite structure and (b) SEM image of montmorillonite	12
Figure 2.5	Division of silicates. Bold letters are minerals found in bentonite	14
Figure 2.6	(a) Single silicon tetrahedron, (b) Silicon tetrahedron sheet arranged in hexagon (c) Single alumina octahedron and (d) Sheet structure of alumina or magnesium octahedron	15
Figure 2.7	Interlayer spacing from XRD against normalized maximum load from indentation tests	17
Figure 2.8	Effect of potassium chloride and ammonium chloride in concentration of Sabah shale	20
Figure 2.9	Effect of KCl with different polymer in Terengganu shale	20
Figure 2.10	The effect of adding polymer in Sabah and Terengganu fields' shale	21
Figure 2.11	Crystalline swelling	21
Figure 2.12	The phenomenon of shale dispersion	23
Figure 2.13	Hydration swelling: Positively charged ions (cations) being attracted to the negatively charged basal planes of shales	25
Figure 2.14	Shale condition before drilling	27
Figure 2.15	Shale condition after drilling	28
Figure 2.16	Shale condition after caving occur	29
Figure 2.17	Potassium chloride performance compare to the others systems performed by LSM	31
Figure 2.18	Monomeric amine shale inhibitor	33
Figure 2.19	Oligomeric amine shale inhibitor	33
Figure 2.20	Different types of viscosifiers with different concentrations in KCl-based mud system	34
Figure 2.21	Depiction of simple salts and inhibition	38

Figure 2.22	Transmission electron microscopy images of spherical silicon nanoparticles from 5 nanometers to 50 nanometers	42		
Figure 2.23	Thermal gravimetric analysis of acrylamide polymer and ZnO nanoparticles-acrylamide polymer composite			
Figure 2.24	(a) Weight loss of synthesized composite observed at 60 % (b) shale swelling and recovery percent			
Figure 2.25	(a) Shale mineralogy (b) recovery rate increase of shale (87-97 wt. %) with increase in fluids concentration (0.3-1.0 wt. %)	52		
Figure 2.26	Formation Process of PP-SiO <sub>2</sub> NCs	53		
Figure 3.1	Framework Methodology	56		
Figure 3.2	Mud balance	63		
Figure 3.3	Rheometer	64		
Figure 3.4	API Filter Press	66		
Figure 3.5	Roller oven	67		
Figure 3.6	XRD instrument	68		
Figure 3.7	FANN Model 2100 Linear Swell Meter.	68		
Figure 3.8	Experimental mechanism for shale swelling			
Figure 3.9	(a) Compactor cell (b) alignment of chamber cap "I" with specimen chamber "Arrow"	71		
Figure 3.10	Core and core chamber layout	71		
Figure 3.11	Core chamber assembly onto compactor cylinder	72		
Figure 3.12	Panel valve and pressure gauge on compactor cell	72		
Figure 3.13	Core extraction tool	73		
Figure 3.14	Sample plug prepared from shale powder using compactor	73		
Figure 3.15	Shale plug were kept in desiccators	74		
Figure 3.16	(a) Components of core stack (b) Core stack (c) installation of core holder (d) core holder assembly locked with core holder.	75		
Figure 3.17	Core holder assembly hanged over measuring head	75		
Figure 3.18	Core holder assembly submerged in the drilling mud	76		
Figure 4.1	FTIR analysis of synthesized polypropylene-based nanosilica composite	81		
Figure 4.2	(a) FESEM images of polypropylene; (b) FESEM images of polyethylene-block-poly (ethylene glycol); (c) EDX spectra of polyethylene-block-poly (ethylene glycol); (d) FESEM image of polypropylene-based silica nanocomposite; (e) FESEM image of polypropylene-based silica nanocomposite; (f) EDX spectra of polypropylene-based silica nanocomposite	82		

Figure 4.3	Thermal behavior of polypropylene and polypropylene-	
	based silica nanocomposite	84
Figure 4.4	Shale Composition (%)	86
Figure 4.5	Comparison of Plastic Viscosities Before and After Aging	89
Figure 4.6	Comparison of Yield Point before and After Aging	90
Figure 4.7	Effect of synthesized PP-SiO2 composite over 10-sec GS WBDF	91
Figure 4.8	Effect of synthesized PP-SiO2 composite over 10-min GS WBDF	92
Figure 4.9	Effect of synthesized PP-SiO2 composite compare to conventional drilling fluids over API filtrate loss volume	94
Figure 4.10	Linear Swell Meter results of basic, KCl, PP-SiO2 NC, and a mixture between KCl and PP-SiO2 NC muds.	96
Figure 4.11	Linear Swell Meter results of Commercial SiO2 and Three Different Concentration of PP-SiO2 NC muds.	98

# LIST OF ABBREVIATIONS

KC1	-	Potassium Chloride
PP-SiO2	-	Polypropylene Nanosilica
PNC	-	Polymer Nanocomposites
PAM	-	Polyacrylamide
LPLT	-	Low Pressure Low Temperature
HPHT	-	High Pressure High Temperature
PPgMA	-	Polypropylene Grafted Maleic Anhydrite
XRD	-	X-ray Diffraction
TEM	-	Transmission Electron Microscopy
XRF	-	X-ray Florescence
FESEM	-	Field Electron Scanning Microscopy
FTIR	-	Fourier Transform Infrared Spectroscopy
LSM	-	Linear Swell Meter
PP	-	Polypropylene
NP	-	Nanoparticles
MA	-	Maleic Anhydride
SiO2	-	Nanosilica
CEC	-	Cation Exchange Capacity
WBDF	-	Water Based Drilling Fluid
OBM	-	Oil Based Mud
CMC	-	Carboxy Methyl Cellulose
PAC	-	Polynomic Cellulose
PHPA	-	Partially Hydrolized Polyacrylamide
XG	-	Xanthan gum
PV	-	Plastic Viscosity
YP	-	Yield Point
GS	-	Gel Strength
MWCNT	-	Multiwall Carbon Nanotubes
TGA	-	Thermal Gravimetric Analysis
EDA-G	-	Ethylenediamine Modified Graphene
API	-	American Petroleum Institute

# LIST OF APPENDICES

APPENDIX

# TITLE

PAGE

Appendix A XRD Results

105

### **CHAPTER 1**

### INTRODUCTION

#### **1.1 Background of Study**

Shales are clastic sedimentary rock type of fine-grained constituents, which is a mixture of clay flakes and silt-sized particles (tiny fragments) of other minerals, such as calcite and quartz. Shale has the tendency to absorb water and swell owing to the presence of clay in the shale. This is due to the high sensitivity of clay minerals in water because of their high water absorption capacity. Montmorillonite is a common typical water sensitive clay. Other water sensitive clays are smectite/inter layered montmorillonite and illite. Kaolinite, Chlorite, apalite, feldspar, quartz, gypsum and carbonate are also clay rock minerals with lower swelling affinities (Ismail, 1996).

More than 75% of the drilled formations worldwide are composed of shale (Berry, 2008). The swelling characteristics of different rock types to mud combinations is crucial in predicting different problems of drilling. It will also help to determine the appropriate mud system to make stable the unforgiving shale environment. This rock characteristic is very complex and is dependent on the type of rock and the nature of the mud compositions, and greatly contributes to caving, heaving, sloughing and progressive wellbore expansion problems in the shale section of the wellbore (Chenevert, 1989). As shale encounters water, there is an exchange of which induces the rock to absorb water. Thus, swelling of shale swells and weakened rock formation (Eurock, 1996). Furthermore, shale swelling leads to easy parting of shale particles from both the drilled debris and wall of the borehole seeping into the mud system as another solid material. This leads to substantial changes in the muds rheological properties, causing other wellbore problems, such as induced fracturing and pipe sticking (Chenevert, 1989).

It is generally understood that high contents of montmorillonite (smectite clay) in the shale is the major cause for undue shale swelling characteristics. In drilling, it is always very difficult to comprehend the unusual shale swelling characteristics found in some shale rocks with little or no swelling clays. Nevertheless, some rich shale formations, in which montmorillonite is the highest constituent contain less swelling behavior in comparison with shales of low stretchy clay content. This help other factors to control the shale-swelling tendency (Amanullah, 1993). A significant consideration in these drilled formations is on how to safeguard the water-sensitive clays from having contact with water and to lessen problems caused by the adsorption of water by the clay. Numerous investigations have been carried out to analyze the performances of different mud additive for shale swelling reduction. Potassium Chloride (KCl) is still considered as the most efficient additive for shale stabilization via cationic exchange (Boyd, 2012). It is believed to be the most functional shale stabilizer in conventional based mud. However, wells drilled with KCl drilling mud needs high amount of K<sup>+</sup> ions to constrain shale. Brien and Chenevert (1973), Clark et al. (1976), and Chang and Leong (2014) reported that high KCl concentration in WBM can separate KCl into two phases, such as sediment and liquid. High filtration loss volumes have been achieved by using KCl based drilling mud.

Polymeric materials in drilling mud were developed to improve rheological properties (Guo *et al.*, 2006) and inhibit shale swelling behaviour (Fritz and Jarrett, 2012; Deville et al., 2011). Polymers contained remarkable hydrophilicity and a well-proportioned hydrodynamic volume successive to hydration, which can make the drilling mud rheological properties to be stable, and subsequently control the filtrates loss properties. As well depth rises, the thermal gradient increases, which leads to harsh downhole environment. Polymer behavior in drilling fluids at high temperature is indicative of the effectiveness of such polymer (Mao et al., 2015). Results from fields indicates that polymeric based drilling fluid are unstable at high temperature, and are always prone to degradation (Amanullah *et al.*, 2011). Thus, drilling personnel's are seeking for novel materials that are physically small, environmental friendly, multi-functional, chemically and thermally stable to be added in drilling fluid for enhanced drilling operation (Amanullah and Al-Tahini, 2009; Hoelscher *et al.*, 2013; Zakaria *et al.*, 2012).

Applications of nanotechnology have been envisaged to usher in new opportunities for exploration phase especially in drilling industry. Drilling fluid r heology and thermal stability can be improved with nanoparticles (NPs) (Abdo and Haneef, 2013). Different applications of NPs in drilling muds have been reported, and they range from viscosity stabilization, prevention of loss circulation at high temperature, enhancing the carrying ability of the mud of drilled cuttings, abating water seepage into the formation, dehydrating clay and minimizing pipe-sticking incidents. Variety of NPs have been examined for viscosity enhancement and shale inhibition characteristics of drilling muds. The most investigated NPs for drilling are nanosilica, multi-walled carbon nanotubes, graphene oxide, copper oxide and zinc oxide and (William *et al.*, 2014).

Micro-nanoparticle composite can be the needed solution for the shale swelling inhibition. Composite materials of organic polymer/inorganic nanoparticle have been widely examined for a long time as reported in literatures. When NP phase in the polymer matrix become nanosized (1-100 nm), they are referred to as polymer nanocomposites (PNCs) (Kickelbick, 2003; Prasad and Geckeler, 2011). PNCs indicates the production and manipulation of polymer or copolymer materials with NPs dispersed in the polymer matrix with at least one of its dimension in the nanometer range of 1-100 nm (Kickelbick, 2003). The tiny size, high area of surface to volume ratio, and high surface energy of NPs empowers it to adsorb over the surface of the clay and seals its pore throats. Commonly used shale inhibitive polymer, such as partially hydrolyzed polyacrylamide (PHPA) have been proven to have the characteristics of coating the shale surface (Hale and Mody, 1993). Thus, shale plugging and coating can be attained with the combination of polymeric material and nanoparticle to form a nanocomposite with enhanced properties more than the properties of the individual constituent. PNC can be produced by directly inserting the nanofiller into the polymer, or by grafting NP into the polymer. It can also be produced through entrapment of the polymer in the NP, such as entrapment of hydrophobic chemically inert polypropylene (PP) at the surface of nanosilica (Zu et al., 2013). This will enhance the properties of the polymer matrix, such as viscoelastic, stronger flame resistant, self-assembly, barrier properties, thermal and chemical stability, and improve the alterations in surface wettability.

Literatures on PNC has showed that the advances made on PNC as an additive of drilling mud is still recent, and its full application in oil and gas industry, more importantly the drilling industry is still in the early stage. Hence, this study was conducted to examine the performance of water-based mud (WBM) formulated with different concentrations of synthesized polypropylene nanosilica (PP-nanosilica) composite as it influences the WBM rheological properties, and its effect on shale swelling inhibition.

# **1.2 Problem Statement**

Recently, one of the most serious issues confronting drillers in the oil and gas industry is on how to develop a smart, cost effective and environmentally friendly WBM which can ensure stability of the mud's rheological properties at high pressure high temperature (HPHT) conditions and enhance shale inhibition properties of the mud (Chu et al., 2013; Mao et al., 2015). Instability in muds rheology and shale may cause different serious wellbore problems that will hinder effective hydrocarbons productions. These problems can occur in the form of high loss of filtrates into the producing formation, spud losses, reduce drilled cutting and other solids particles transportation efficiency, reduce drilling rate, shale collapse and sloughing, and increase differential stuck pipe (DeNinno et al., 2016; Mohiuddin et al., 2007). These problems can be resolved if the mud rheological properties, such as plastic viscosity (PV), yield point (YP) filtrates loss control volumes, lubricity are improved and shale swelling behavior are inhibited by the drilling mud. While KCl have been mostly employed to dehydrate clay and inhibit shale swelling behaviour, its limitation of forming two phases in drilling mud have been a serious concern to drilling personnels. High KCl concentration in WBM can cause KCl to develop into two phases, such as liquid and sediments. These sediments in drilling mud can lower the drilling rate, thus prompting higher pump power requirements. Besides, it is not eco-friendly when high concentrations are required to minimize shale high swelling rate. Therefore, low concentrations of KCl are preferred in the drilling mud, but the usage of low concentrations of KCl alone is somewhat ineffective in reducing shale instability (Deville, Halliburton, 2011). It is thought that PHPA-KCl polymer mud system can

achieve the desired shale swelling inhibition, but this combination also has proven to be inactive in unforgiving formations, such as shale, HPHT, deep-water and ultra – deep water (Berry, 2005). Therefore, to address these problems, the combination of hydrophobic chemically inert PP with the ability to repel water molecules in the mud owing to its hydrophobicity and nanosilica proven to be effective in plugging the shale nano-void space were used to inhibit shale-swelling characteristics and drill-in effectively in the unforgiving formations. The synthesized PP-nanosilica composite based drilling mud were used in this study on account of their attractive properties and functionalities, such as enhanced shale plugging characteristics, rheological properties, thermal and chemical stability.

### 1.3 Objectives

The main aim of this study was to enhance the rheological properties and shale inhibition characteristics of conventional WBM using synthesized PP-SiO2 composite. This study was conducted to achieve the outlined objectives:

- i. To synthesize and characterize PP-SiO2 NC material.
- ii. To investigate the rheological properties of synthesized PP-SiO2 NC in WBM at different concentrations and compared with typical rheological properties of drilling fluids employed for drilling in shale formation at low pressure-low temperature (LPLT) and high pressure-high temperature (HPHT) conditions.
- iii. To identify the types of minerals of different shale samples in order to determine the most suitable shale to be used for easier facilitation of shale swelling data interpretation.
- iv. To analyze the clay hydration and shale swelling behavior of synthesized PP-SiO2 NC in WBM on the selected shale sample.

### 1.4 Scope of Study

The scopes of this study are as follows:

- i. Synthesizing, and characterizing PP-SiO2 NC material.
- ii. Formulating five muds system: basic mud, KCl mud, PP-SiO2 NC mud, SiO2 NP mud, and a mixture between KCl and PP-SiO2 NC mud systems.
- iii. Different weight amounts of synthesized PP-SiO<sub>2</sub> NC of 0.3g, 0.6g, and 1.0g was added to the prepared WBM.
- iv. Mineral components and clay compositions were identified using x-ray diffraction for different types of shale samples.
- v. The rheological properties of synthesized PP-SiO2 NC based drilling mud, such as plastic viscosity, yield point, gel strength, API filtrate loss volumes compared with those of based mud and KCl mud employed for drilling shale under LPLT and elevated temperature.
- vi. Shale swelling behavior of synthesized PP-SiO2 NC drilling fluids are examined at 3 different concentrations from 0.3 g, 0.6 g, and 1.0 g and compared with other type of water based mud using Linear Swell Meter equipment.

### 1.5 Significance of the Study

It is expected that this study will offer the following contributions;

- The findings of this study could lead to a new approach and prospects in improving drilling operations especially clay dehydration, shale swelling inhibition and environmental consideration under elevated temperature.
- The outcomes of this study could also provide optimum rheological properties needed to effectively drill shale formation under both LPLT and elevated temperature conditions.

- 3. Application in the real field could benefit the oil and gas industry in terms of making the drilling of sensitive reactive water formation more efficient and economic.
- 4. The polymer and nanoparticle product can be used in other areas of oil and gas industry, such as EOR, workover, and completion jobs.

#### REFERENCES

- American Petroleum Institute (1997), Recommended Practice Standard Procedure for Field Testing Drilling Fluids 13B
- Bakly, O. and Samir, A. (2007). Custom Designed Water-Based Mud System Helped Minimize Hole Washouts in High-Temperature Wells: Case History From Western Egypt. SPE/IADC 108292. SPE/IADC Middle East Drilling Technology Conference & Exhibition. Cairo, Egypt. 22-24 October 2007.
- Ballard, T.J., S.P. Beare, and T.A. Lawless. 1992. Fundamentals of shale stabilization:Water transport through shales. In European Petroleum Conference held in Cannes, France, 16-18 November 1992. SPE #24974
- Aston, M., and Elliott, G. (1994). *Water-based glycol drilling muds: shale inhibition mechanisms*. Paper presented at the European Petroleum Conference.
- Berry, S., Boles, J., Brannon, H., and Beall, B. (2008). Performance Evaluation of Ionic Liquids as a Clay Stabilizer and Shale Inhibitor. SPE 112540. SPE International Symposium and Exhibition on Formation Damage Control, 13-15 February 2008.
- Beihoffer, T., Dorrough, D., and Schmidt, D. (1990). *The development of an inhibitive cationic drilling fluid for slim-hole coring applications*. Paper presented at the SPE/IADC Drilling Conference.
- Boggs, S., Jr 2003. *Petrology of Sedimentary Rocks, Cladwell, New Jersey*: The Blackburn Press.
- Carminati, S., Del Gaudio, L., Del Piero, G., and Brignoli, M. (2001). Water-Based Muds and Shale Interactions. Paper presented at the SPE International Symposium on Oilfield Chemistry.
- Chenevert, M. E., O'Brien, Dennis E. (1973). Stabilizing Sensitive Shales With Inhibited, Potassium-Based Drilling Fluids. (SPE 4232). SPE-AIME Sixth Conference on Drilling and Rock Mechanics. Austin, Tex., 22-23 Jan 1973.
- Denis, J., Keall, M., Hall, P., and Meeten, G. (1991). Influence of potassium concentration on the swelling and compaction of mixed (Na, K) ion-exchanged montmorillonite. Clay Minerals, 26(2), 255-268.

- Dept, A. P. I. P. (1990). *Recommended Practice Standard Procedure for Field Testing Water-based Drilling Fluids* (Vol. 13): American Petroleum Institute.
- Di Miao, C. 1996. Exposure of Bentonite to Salt Solution: Osmotic and Mechanical Effects. Geotechnique. Vol. 46. No. 4 695-707.
- Ewy, R. and Morton, K. (2009). Shale Swelling Tests using Optimized Water Content and Compaction Load. SPE 121334. SPE Western Regional Meeting, San Jose, California, USA. 24-26 March 2009.
- He, W., Gomez, S. L., Leonard, R. S., and Li, D. T. (2014). Shale-Fluid Interactions and Drilling Fluid Designs. Paper presented at the IPTC 2014: International Petroleum Technology Conference.
- Ismail, A. R., and Lim, F. C. H. (1995). Water-based mud formulations in drilling Terengganu shale formation. Paper presented at the Proceedings of The Eleventh Symposium of Malaysia Chemical Engineers, C16-11.
- Ismail, A.R. and Tan C.K. (1996). The Effect of Chemicals and Concentrations on Local Shale Formations. 12th Symposium of Malaysian Chemical Engineers, Bangi, Malaysia, 9-10 July 1996.
- Keall, M. J., Hall, P. L., and Meeten, G. H. (1991) The Influence of Potassium Concentration on The Swelling and Compaction of Mixed (Na, K) Ion-Exchanged Montmorillonite. Schlumberger Cambridge Research, UK, Clay Minerals (1991) 26, 255-268.
- Lanson, B., and Besson, G. (1992). Characterization of the end of smectite-to-illite transformation: Decomposition of X-ray patterns. Clays and Clay Minerals, 40(1), 40-52.
- Linear Swell Meter Model 2100 Instruction Manual 102114531, Revision B, Instrument No. 102123383 (2013) Fann Instrument Company, Houston, Texas, USA.
- Mohd Zaki Bin Dzulkifli (2011). Surfactant Types For Water Based Mud System In Shale Instability. Degree Thesis. Universiti Teknologi Malaysia. Skudai.
- O'Brien, D. E., (1973). *Stabilizing sensitive shales with inhibited, potassium-based drilling fluids*. SPE-AIME, Esso Production Research Co.
- O'Brien, D. E., and Chenevert, M. E. (1973). *Stabilizing sensitive shales with inhibited, potassium-based drilling fluids*. Journal of Petroleum Technology, 25(09), 1,089-081,100.

- Patel, A. D. (2009). Design and development of quaternary amine compounds: shale inhibition with improved environmental profile. Paper presented at the SPE International Symposium on Oilfield Chemistry.
- Patel, A., Stamatakis, S., Young, S., and Friedheim, J. (2007). Advances in Inhibitive Water-Based Drilling Fluids—Can They Replace Oil-Based Muds? Paper presented at the International Symposium on Oilfield Chemistry.
- Roehl, E. A., and Hackett, J. L. (1982). *A laboratory technique for screening shale swelling inhibitors*. Paper presented at the SPE Annual Technical Conference and Exhibition.
- Samir, A., Bakly, E., and Wafik, O. A. (2007). Custom Designed Water-based Mud Systems Help Minimize Hole Washouts in High Temperature Wells-Case History from Western Desert, Egypt. Paper presented at the SPE/IADC Middle East Drilling and Technology Conference.
- Santarelli, F., Chenevert, M., and Osisanya, S. (1992). *On the Stability of Shales and its consequences in terms of swelling and wellbore stability*. Paper presented at the SPE/IADC Drilling Conference.
- Santos, H., and Perez, R. (2001). *What have we been doing wrong in wellbore stability?* Paper presented at the SPE Latin American and Caribbean Petroleum Engineering Conference.
- Salles, F., Bildstein, O., Douillard, J.-M., Julien, M., and Van Damme, H. 2007. Determination of the Driving Force for the Hydration of the Swelling Clays from Computation of the Hydration Energy of the Interlayer Cations and the Clay Layer. The Journal of Physical Chemistry C111 (35): 13170-13176.
- Steiger, R.P and Leung, P.K. (1990). Lecture: Predictions of Wellbore Stability in Shale Formations at Great Depth. Exxon Production Research, Houston, Tex., USA. Rock at Great Depth, Fourmaintraux, Balkema, Rotterdam. ISBN 9061919754.
- Stephens, M., Gomez-Nava, S. and Churan, M. (2009). Laboratory Methods To Assess Shale Reactivity With Drilling Fluids. AADE National Technical Conference & Exhibition (NTCE), New Orileans, Louisiana, 2009.
- Wilson M.J. (1980) Interlayer and intercalation complexes of clay minerals. Pp. 197-248 in: Crystal Structures of Clay Minerals and their X-ray Identification (G.W. Brindley & G. Brown, editors). Mineralogical Society, London.

Zhang, J. (2004). A New Gravimetric – Swelling Test for Evaluating Water and Ion Uptake in Shales. SPE 89931. SPE Annual Technical Conference and Exhibition. Houston, Texas, USA. 26-29 September 2004.