

DEVELOPMENT OF AN ULTRA-LIGHTWEIGHT COCONUT
SHELL-BASED PROPPANT FOR HYDRAULIC FRACTURING OF
SUBTERRANEAN FORMATIONS

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Dedicated to my beloved family

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ABSTRACT

Hydraulic fracturing (HF) has seen a considerable increase in interest for the purpose of improved oil recovery. HF creates high conductive conduits between wellbores and reservoirs by a pressurized fluid mixed with proppants. The problem of most popular fracturing fluid (i.e., slickwater) is the high settling rate of common proppants, e.g. sand, which results in small effective propped fractures. Ultra-lightweight (ULW) proppants are easily transported by slickwater and can cover further fracture area. However, ULW proppants cannot provide enough strength at high closure pressure. This study developed a moderately high strength, chemically modified and reinforced composite proppant (CMRCP) which is composed of chemically modified coconut shell, composite material, and epoxy resin. Investigating the performance of new ULW proppant was conducted using laboratory and simulation works such as characterization, quality and mechanical evaluation, simulation mechanical response of particles under compression, fracture conductivity, and HF design. Characterization indicated that the coating layers of CMRCP provide thermal stability of 297.5 °F. Also, quality tests revealed that CMRCP is a neutral buoyant proppant with lower bulk density than frac sand, glass beads, ULW-1.75, and ceramic. Desirable strength (i.e., 8,000 psi) and conductivity (i.e., 791 mDft) from mechanical tests and fracture conductivity were observed, respectively. The results showed an improved performance than Brady sand and its counterpart (i.e., ULW-1.25). The results of strength tolerance and fracture conductivity of CMRCP were 25% and 77% higher than ULW-1.25. Furthermore, experimental and simulation of proppant's mechanical response with different geometries approved that round geometry provides further strength. Finally, HF design shows that the new product can realise high cumulative production, net present value, and return on investment. This study introduced a new ULW proppant that has moderately high strength, resistant to high temperature, easy to get, light, and cost effective, and it can be used as proppant for HF of subterranean formations.

ABSTRAK

Peretakan hidrolik (HF) telah menarik banyak perhatian bagi tujuan pengeluaran minyak tertingkat. HF mewujudkan saluran konduktif yang tinggi di antara lubang telaga dengan reservoir menerusi pengaplikasian cecair bertekanan tinggi yang dicampurkan dengan penyangga. Masalah yang dihadapi bendalir peretak yang paling popular (iaitu air licik) ialah kadar pemedapan tinggi yang dialami penyangga biasa, misalnya pasir, yang hanya menghasilkan retakan kecil yang kurang berkesan. Penyangga lampau ringan (ULW) mudah diangkut oleh air licik dan boleh menyanggah kawasan retakan secara menyeluruh. Walau bagaimanapun, penyangga ULW tidak mempunyai kekuatan yang cukup untuk menahan tekanan penutupan yang tinggi. Kajian ini telah menghasilkan penyangga komposit berkekuatan tinggi, terubah suai secara kimia dan diperkukuh (CMRCP). Penyangga itu diperbuat daripada tempurung kelapa yang diubah suai secara kimia, bahan komposit, dan resin epoksi. Kajian terhadap prestasi penyangga ULW baharu melibatkan kerja-kerja di makmal dan penyelidikan misalnya pencirian, penilaian kualiti dan mekanikal, penyelidikan respons mekanikal zarah bawah mampatan, kekonduksian retakan, dan reka bentuk HF. Pencirian menunjukkan bahawa lapisan-lapisan CMRCP menghasilkan kestabilan terma setinggi 297.5 °F. Ujian kualiti turut mendedahkan bahawa CMRCP ialah penyangga apung neutral yang mempunyai ketumpatan pukal lebih rendah daripada pasir peretak, manik kaca, ULW-1.75, dan seramik. Kekuatan (iaitu 8000 psi) dan ujian kekonduksian (iaitu 791 mDft) yang dikehendaki masing-masing diperoleh daripada ujian mekanikal dan kekonduksian retakan. Keputusan kajian telah menunjukkan prestasi yang lebih baik daripada pasir Brady dan bahan setaranya (iaitu ULW-1.25). Keputusan toleransi kekuatan dan kekonduksian retakan CMRCP ialah 25% dan 77% lebih tinggi daripada ULW-1.25. Selanjutnya, kajian di makmal dan kajian penyelidikan terhadap respons mekanikal penyangga dengan geometri yang berbeza membuktikan bahawa geometri bulat memberikan kekuatan tambahan. Akhir sekali, reka bentuk HF menunjukkan bahawa produk baharu itu mampu merealisasikan pengeluaran kumulatif, nilai bersih kini, dan pulangan ke atas pelaburan yang tinggi. Kajian ini memperkenalkan penyangga ULW baharu yang mempunyai kekuatan yang tinggi, kalis suhu tinggi, mudah diperoleh, ringan, dan kos efektif. Penyangga itu boleh diguna dalam operasi peretakan hidrolik formasi subpermukaan.

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LIST OF SYMBOLS

D	-	Depth of Reservoir (ft)
E	-	Modulus of Elasticity (psia)
F	-	Contact Force (lbf)
k	-	Permeability (mD)
P	-	Reservoir Pressure (psia).
R	-	Radius of the Sphere (ft)
C _b	-	Bulk Compressibility (psia)
D _l	-	Test liquid density, (lb/ft ³)
D _p	-	Specific gravity of proppant (lb/ft ³)
E _{infiltration}	-	Infiltration Elasticity (psia)
h _f	-	Fracture height (ft)
k _f	-	Fracture Permeability
P _p	-	Pore Pressure (psia)
P _{bd}	-	Breakdown Pressure (psia)
q _i	-	Production Rate (ft ³ /s)
w _o	-	Width of the Fracture(ft)
W _{f,l}	-	Weight of flask filled with test liquid (lb)
W _f	-	weight of empty flask (lb)
W _p	-	Weight of proppant (lb)
W _{f,l,p}	-	Weight of flask, liquid and proppant (lb)
U _{avg}	-	Linear Velocity (ft/s)
P(r)	-	Hertzian distribution of pressure (psia)
x _f	-	Fracture half-length, (ft)
μ _e	-	Effective viscosity of fracturing fluid (cp)
ρ _b	-	Bulk Density (lb/ ft ³) or (gr/cm ³)
μ	-	Fracturing fluid viscosity, (cp)

v - Poisson's ratio, dimensionless

LIST OF ABBREVIATIONS

API	- American Petroleum Institute
ASTM	- American Standard
CBD	- Chemical Bath Deposition
CE	- Chain Extender
CMRCP	- Chemically Modified and Reinforced Composite Proppant
CP	- Conventional Proppant
CPs	- Conventional Proppant Systems
CS	- Cold Spray
EDX	- Energy Dispersive X-Ray Spectrometry
FESEM	- Field Emission Scanning Electron Microscope
FEM	- Finite Element Method
FC	- Fracture Conductivity
FML	- Full Monolayer
FTIR	- Fourier Transform Infrared Spectroscopy
FTU	- Formazin Turbidity Units
HF	- Hydraulic Fracturing
HVPC	- High Velocity Particle Consolidation
HSP	- High Strength Proppant
IOR	- Improved Oil Recovery
ISO	- International Standard Organization
ISP	- Intermediate Strength Proppant
KGD	- Khristianovich-Zhel'tov-Geertsmadeklerk
LW	- Lightweight
LRS	- Liquid Resin System
LPCS	- Low-Pressure Cold Spray
LPTA	- Lembaga Perlesenan Tenaga Atom

MPL	- Multiple layer
NIOSH	- National Institute for Occupational Safety and Health
NTU	- Nephelometric Turbidity Units
NPV	- Net Present Value
OSHA	- Occupational Safety and Health Administration
PGMA	- Poly Glycidyl Methacrylate Polymer
PKN	- Perkins-Kern Width Equation
PU	- Polyurethanes
PML	- Partial Monolayer
RCP	- Resin Coated Proppant
RCPs	- Resin Coated Proppant Systems
RSE	- Resource Engineering Systems
ROI	- Return on Investment
SG	- Specific Gravity
SEM	- Scanning Electron Microscope
SSP	- Self-Suspended Proppant
SPD	- Supersonic Particle/Powder Deposition
SMA	- Surface Modifying Agent
TGA	- Thermo Gravimetric Analysis
ULW	- Ultra-Lightweight
U.S	- Unites States
VES	- Viscoelastic Surfactant-Based

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CHAPTER 1

INTRODUCTION

1.1 Overview

Due to the decrease in oil discoveries in recent years, Improved Oil Recovery (IOR) methods will be capable of playing an essential role in replying to demand in the years to come. IOR processes consist of all techniques that are employed to enhance hydrocarbon production (Surguchev *et al.*, 2005). Well Stimulation as one of these techniques is composed of various operations to maintain or improve productivity of wells. It creates new channels or eliminates the obstacles in the pay zone to facilitate the flow of oil and gas from the formation to the wellbore (Pershikova, 2007). Hydraulic fracturing (HF) is known as the main method to stimulate oil and gas wells, and it begins with pumping a fracturing fluid into a well to enhance pressure above fracturing pressure of the subterranean formation that contains entrapped oil or gas (Soane *et al.*, 2010). This process results in cracks and breaks that disrupt the underlying layer to allow the transfer of hydrocarbon products to the wellbore at a significantly higher rate. Once the fracture is created, a slurry composed of fracturing fluid and proppant is injected to open and maintain a path flow from the fracture to the wellbore (Soane *et al.*, 2010). Fracturing fluids used to transport proppant inside the fracture include water based fluids, linear gels, cross-linked gels, oil based fluids, and foam/ poly emulsions fluids (Montgomery, 2013). Further information about history of the fracturing fluid, composition, economical issue, methods of utilization, and cost of the fracturing fluid can be found in the technical literature (Montgomery, 2013).

Another part of the slurry is proppant, and it is defined as any non-liquid material that is used to provide structural support for created fracture and to keep it open (Windebank *et al.*, 2013). Proppant demand for HF treatment of the unconventional reservoirs has been increased from 5 billion pounds in 2004s to 60–70 billion pounds in 2012s (Palisch *et al.*, 2012). In accordance to a report, the oil and gas industry supplied over 135 billion pounds of various proppants in 2015s, close to 50 percent growth over 2012s (McEwen, 2015).

The proppant can be frac sand, nut hulls, ceramics, bauxites, glass beads, RCP, and combinations thereof (Lesko *et al.*, 2008). These types of proppants are known as conventional proppant (CP). In the recent years, a new generation of proppants with low specific gravity, high strength, and low settling velocity that are known as Lightweight (LW) and Ultra-Lightweight (ULW) proppant have been introduced to the market. One aim of proppant industry has been to reduce proppant density without sacrificing strength. Thus, the ULW proppant with specific gravity of 1.25-1.75 made from a substrate material such as a walnut hull or porous ceramic and two layers of polymers as coating was introduced to the market to satisfy this aim (Wood *et al.*, 2003).

Therefore, a chemically modified and reinforced composite proppant (hereafter it is called CMRCP) that is comprised of the coconut shells as substrate and two layers of polymer (reinforced and coating layers) is introduced in this study. The new proppant is produced at three stages. First, substrate surface is modified with a solution of sodium hydroxide to improve its capability for reinforcement. Then, the modified substrate is reinforced with a composite material to improve its strength. Thereafter, coating of the reinforced coconut shell is performed with a thin layer of polymer. The epoxy resin is chosen as polymer because the reinforced layer contained the poly glycidyl methacrylate (PGMA) polymer, and the epoxy group of the PGMA polymer is capable of providing a strong bond with epoxy resin. In this study, experimental and computational analysis methods are used to characterize and investigate the capability of the new ULW proppant. Narrowing down of the study is shown in Figure 1.1.

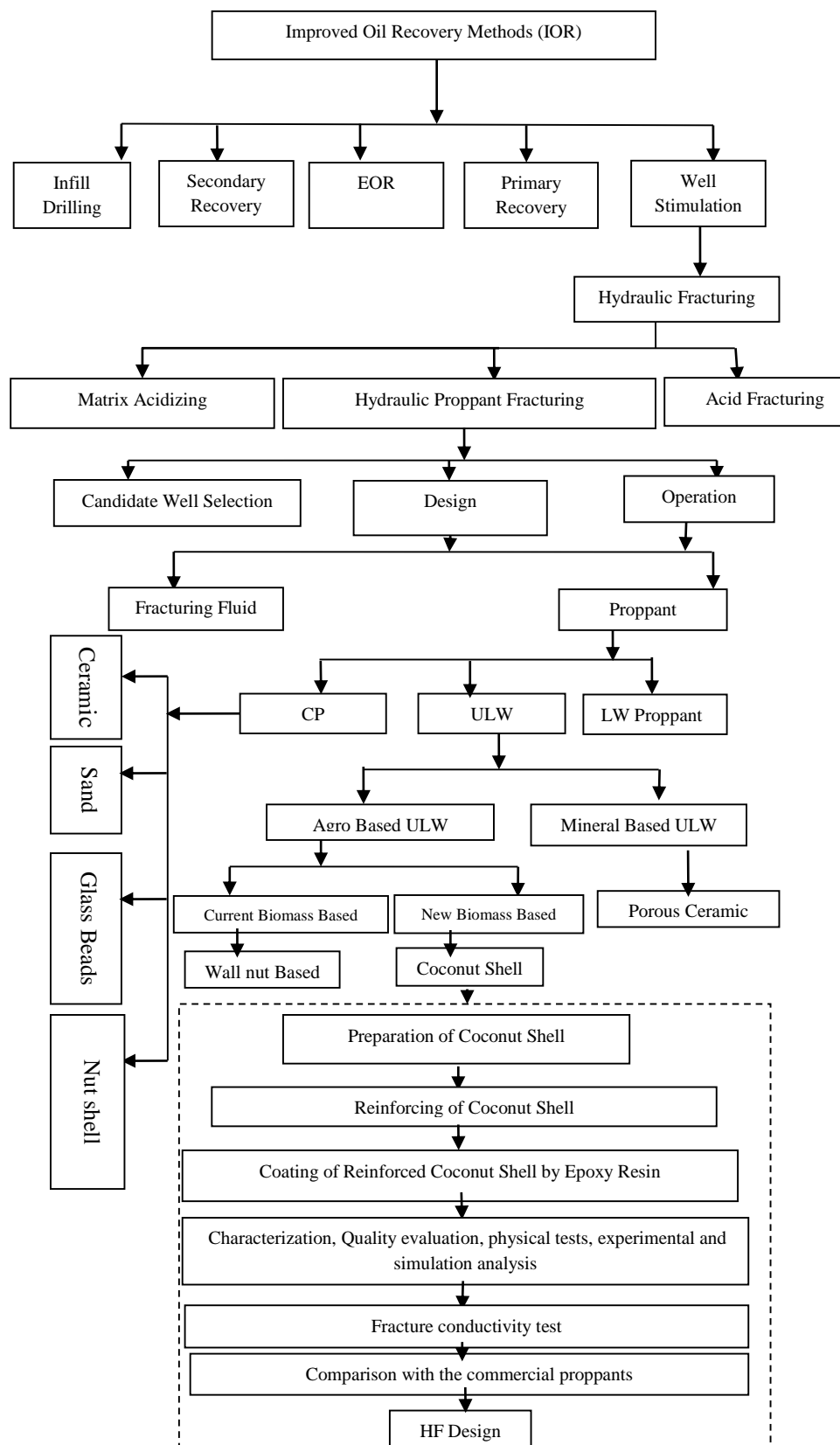


Figure 1.1 Narrowing down of the study

1.2 Background of the Problem

Researchers are trying to improve the quality of proppant to remove the drawbacks of CP for HF treatment. For example, the widespread use of frac sand as propping agent with an average specific gravity of 2.5-2.70 (Luo *et al.*, 2011) is common because of the low cost and ready accessibility (O'Brien and Haller, 2014). However, frac sand is not capable of providing sufficient strength to resist crushing (Li *et al.*, 2014). The high embedment pressure of the formation causes proppant embedment, and exceeding the load bearing capacity of the frac sand leads to crushing of the frac sand. As a result, fines produced from the crushed frac sand plug the fracture leading to proppant flowback. Proppant flowback is the transfer of proppants back into the wellbore with the production of formation fluids from formation (Nguyen, 2004), and it causes reduction of the fracture conductivity, restriction of production, and erosion of tubular and wellhead equipment as well as surface facilities. In addition, proppant flowback fills treating vessels that cause failure in the treating process (Ellis and Surles, 1998).

Another main problem of using frac sand proppant for the HF treatment is related to enhancement of frac sand mining across the bank river. Frac sand mining has created a considerable public health threat in the region possibly due to the negative effects of mining, processing and transporting of frac sand.

By surface coating the frac sand proppant with a thin layer of resin, the brittle frac sand proppant becomes resistant to acid and crushing (Droppert *et al.*, 2002). Also, the coated sand is capable of consolidating, and it has great potential to minimize proppant flowback. This is because coating layers retain the small particles that are generated from the frac sand due to the increase of the closure pressure (Barmatov *et al.*, 2010). Although coating layers have eliminated some of the drawbacks of frac sand but utilization of sand coated proppant is restricted to wells with certain closure stress (less than 8,000 psia) (Ellis and Surles, 1997). Also, phenolic acid and formaldehyde that are known as dangerous chemical materials are used for sand coating that cause health problems for those who are exposed to this type of proppant (Malone, 2012).

Since application of frac sand and coated sand are restricted to a certain closure pressure (less than 8,000 psia), ceramic proppant with a specific gravity of 3.3-3.6 (Jones and Cutler, 1985) was introduced to stimulate formation with higher closure pressure (Smith *et al.*, 2011). Although conventional ceramic proppant has shown exceptional crush strength, it has exhibited extreme density that requires viscous fluids to carry within the fracture (Smith *et al.*, 2011). When it transfers with a low-density fluid (e.g., slickwater), it settles before reaching the end of the fracture. Consequently, using viscous fluids creates problems such as damage to the formation and surface equipment and increase in the cost of the HF treatment during propped fracturing treatment.

Also, environmental problems that are related to ceramic factories cause a lot of damage to human beings. These factories cause emissions that are released into air, water and land, and they make noise and undesirable smells during production of the ceramic products (IPPC, 2007). All involved parts of the ceramic industry are consuming higher amounts of energy, and they consume natural gas, liquefied petroleum gas and fuel oil for firing. Utilization of these materials as feed leads to the production of high amounts of carbon dioxides and other harmful gases (IPPC, 2007).

Other proppants which have been used in proppant industry are agro-based materials such as nutshells which were introduced in the proppant industry in the 1960s. In contrast to frac sand, nutshells cause less damage when exposed to the surface equipment because these hard fibrous products are deformable. In addition, nutshells are free from the silica that causes inhalation health concerns (Kramer, 2015). It was found that when agro-based materials are used in proper concentration and size, they yield high fracture capacities relative to frac sand (Fast *et al.*, 1961). However, utilization of agro-based proppant such as nutshells has reduced fracture conductivity, and nutshells that are made naturally have limited application as closure pressure increases (Liang *et al.*, 2015). It is due to the high tendency of nutshells to deform even in lower closure stress.

Accordingly, reinforcing and coating of nutshells with polymers can improve their strength to high closure stress, protecting particles from crushing, help resist embedment, and prevent the liberation of fines (Rickards *et al.*, 2003, Schein *et al.*, 2004, Abbott *et al.*, 2008, Brannon *et al.*, 2010). Since specific gravity of these coated materials is lower than CP, they are called ULW proppant. ULW proppant is defined as a proppant with the specific gravity less than or equal to 2.45 while its particle size is ranged in a mesh size of 12/20 to about 40/70 (Brannon *et al.*, 2010).

ULW Proppants are ideally suited to slickwater fracturing treatments because they have light weight, and they do not settle before reaching the end of the fracture (Brannon *et al.*, 2009). Slickwater is a cost saving fracturing fluid with low viscosity. Most of the slickwater fracturing fluid is water while other additives such as friction reducer, acid, surfactant, potassium chloride, scale inhibitor, pH adjusting agent, iron control agents, corrosion inhibitors, and biocides are added to the fluid (Barati and Liang, 2014).

Transferring ULW proppants with slickwater have indicated more benefits such as reducing proppant settling and creating more effective fracture length (Rickards *et al.*, 2003; Schein *et al.*, 2004). The performance of ULW proppants was great in reservoirs with closure pressures up to 5,000 psia and bottom hole temperatures up to 225 °F (Posey, 2007).

Placement of ULW proppant within the fracture is usually performed with various arrangements including partial monolayer (PML), full monolayer (FML), and multiple layers (MPL) of proppants. As previously mentioned by Economides *et al.*, (2000), the PML is the best arrangement because of providing further fracture conductivity related to other arrangements. In a properly engineered fracture treatment, ULW proppant could form PML arrangement (Brannon *et al.*, 2009). Also, the ULW proppants provide further fracture conductivity compared to conventional frac sand proppant. As reported by Brannon *et al.* (2009), adding small amounts of ULW proppant to pad leads to great improvement in the fracture conductivity. In addition, the settling rate of ULW proppants is less than CP (Brannon *et al.*, 2004). It means that they are transported easily within the fracture

with lower proppant settling that leads to the provision of further effective propped fracture length. As the result of more propped fracture length for low permeability reservoirs, the production is improved (Wood *et al.*, 2003). However, the ULW proppant cannot provide high strength under closure stress. It seems that using higher strength substrate and reinforcing of substrate with composite material before coating can improve strength of ULW proppant.

Since nutshells are always subjected as a good substrate for ULW proppant, and coconut shell is classified as a part of nutshells, it is obvious that it has potential to convert to a good substrate of ULW proppant. Advantages of coconut shell including light weight with specific gravity of 1.25-1.33 (Reddy *et al.*, 2014), high strength to withstand closure stress with Young modulus of 9.2 GPa, renewable, ready accessible with low price, and good capability for coating with a less expensive method have qualified it as a good substrate of ULW proppant in tropical countries such as Malaysia. Some advantages of coconut shell have qualified it to apply in various industries. For example, inherent mechanical properties of coconut shell such as high strength and high modulus (Sapuan *et al.*, 2003) enable it to be applied as fillers in the composition of new composites. In addition, the excellent shock-absorbing capability of coconut shells accounts for its robustness (Martone *et al.*, 2010). Also, coconut shell provides low specific gravity which has been used as a coarse aggregate for light weight concrete (Reddy *et al.*, 2014)

Since the ULW proppants must provide appropriate strength to withstand high closure pressure (Brannon *et al.*, 2004), are light to buoyant on the fracturing fluid (Wood *et al.*, 2003), deform to prevent breaking (Brannon and Starks, 2009), inexpensive, and safe to reduce damage to the workers who are exposed to propping agent, it is obvious that coconut shell that is reinforced with a composite material before coating has all of these requirements, and it can be used as ULW proppant.

1.3 Problem Statement

Using renewable resources, saving cost of HF treatment, improving hydrocarbon recovery and pollution preservation are essential needs in today's oil and gas industry. Expense of the propping agent alone could be 67 % of the total stimulation costs, and it has converted proppants as an important parameter for technological research (Economides *et al.*, 2000).

Although CPs have wide application in the HF treatment, some of the drawbacks that they have shown during the HF operation impose extra cost to HF treatment. As indicated by Li *et al.* (2013), frac sand proppant does not provide sufficient strength to resist crushing of the high closure stresses. When frac sand proppant is exposed to high closure stress (further than 5,000 psia), it produces fines that will plug the formation and fracture path flow (Economides *et al.*, 2000). It also causes damage to the surface equipment and adds extra cost to HF treatment (Ellis and Surles, 1998).

In contrast to frac sand, high strength tolerance is the main characteristic of ceramic proppants and resin coated proppant (RCP) but their extreme density have restricted their utilization in a wide range (Smith *et al.*, 2011). It means that they require viscous fracturing fluids and high pumping rates to suspend into fracturing fluid. Also, they cause greater than normal wear on fluid carrying and pumping equipment (Li *et al.*, 2013).

Slickwater fracturing treatment has indicated great success for stimulating of numerous formations because it does not require viscous fracturing fluid. However, higher settling rate of frac sand, RCP, and ceramic proppant have restricted its utilization (Liang *et al.*, 2015). In contrast to CPs, ULW proppants were ideally suited to slickwater fracturing treatments because they have light weight, and they do not settle before reaching the end of the fracture (Brannon *et al.*, 2009). However, ULW proppants had indicated low strength, proppant embedment, high price and difficult placement within the fracture (Wood *et al.*, 2003). Utilization of common ULW proppants are restricted to closure pressure of 5,000-6,000 psia (Wood *et al.*,

2003; Brannon *et al.*, 2004). The major advantage of ULW proppants is their low specific gravity, not strength. They will deform easily under high closure pressure and reduce the fracture conductivity.

Development of science and technology is beneficial to use new materials (e.g., high strength substrate, composite material,...) and techniques (e.g., surface modifying, reinforcing, new coating methods,...) for development of a new generation of ULW proppants which can tolerate higher closure pressure. Therefore, using a substrate that has better properties than walnut hull can improve the strength of agro-based ULW proppants. Also, application of surface modification technique and composite material show promising results for strength improvement. If the surface of coconut shell is modified by sodium hydroxide and reinforced with a composite material then coated properly with epoxy resin, it is capable of providing higher strength under closure pressure. The new ULW proppant (i.e., CMRCP) that is light, strength, safe, inexpensive, easy to get, and reliably delivered can be used and developed as an economic proppant to improve the quality of HF treatment

1.4 Research Objectives

The main objectives of this study are as follows:

1. To develop ultra-lightweight and a high strength proppant through reinforcing and coating of the coconut shell with a composite material and polymer.
2. To characterize the mechanical response of CMRCP particles under compression.
3. To evaluate the performance of CMRCP for providing fracture conductivity, and to simulate its performance in the field using HF design.

1.5 Scope of Research

In this study, CMRCP that is comprised of coconut shells as substrate and two coating layers of composite and polymer is produced at three-step process. First step includes modifying the surface of the coconut shell for the reinforcement. Second step is reinforcing of closely sized coconut shell particles (20/40 US mesh) with a composite material composed of the flax fiber and poly glycidyl methacrylate polymer (PGMA). The aim of reinforcing coconut shell with the composite material is to improve its strength to resist closure pressure. Similar to the procedure that is used for most RCP, the third step includes coating of reinforced particles with a thin layer of epoxy resin. Scope of the study includes the following procedures:

- 1- Preparation of the coconut shell particles to use as a substrate in the composition of ULW proppant. The process of preparing coconut shell particles includes drying, crushing, grinding, and sieving.
- 2- Reinforcement of coconut shell particles with a composite material that is comprised of the flax fiber & PGMA polymer by using chemical bath deposition method.
- 3- Coating of the reinforced coconut shells with epoxy resin by using chemical bath deposition method.
- 4- Evaluating the quality of the uncoated coconut shell and CMRCP based on the standard procedure (API RP 60).
- 5- Investigation of physical properties of the uncoated coconut shell and CMRCP using crush resistance test.
- 6- Evaluation of mechanical behavior of the uncoated coconut shell, reinforced coconut shell and CMRCP using single compression test (Dag series 4000). In addition, simulation and experimental results of mechanical behavior of single particles of the uncoated coconut shell,

reinforced coconut shell and CMRCP under compression are developed and compared.

- 7- Control quality evaluation of the uncoated coconut shell and CMRCP by using commercial proppants.
- 8- Characterization of the uncoated coconut shell, reinforced coconut shell and CMRCP to find microstructure, compounds and functional groups, elements, and thermal stability of particles. Field emission scanning electron microscope (FESEM), scanning electron microscope (SEM), energy dispersive X-ray spectrometry (EDX) test, Fourier transform infrared spectroscopy (FTIR), and thermo gravimetric analysis (TGA) tests are used to characterize the uncoated coconut shell, reinforced coconut shell and CMRCP.
- 9- Simulation of mechanical behavior of the uncoated coconut shell and CMRCP under compression using ABAQUS software.
- 10- Evaluation of flow capacity of the uncoated coconut shell and CMRCP using fracture conductivity test according to the standard procedure (ISO13503-5). Sandstone core from Kuala Terengganu were used in the fracture conductivity tester.
- 11- Performing HF design with using FracproPT (version 10.824-2015) simulator to investigate the performance of CMRCP in San Juan basin formation. This field is chosen because Brady sand and ULW-1.25 have been widely used as proppant to stimulate wells in San Juan basin formation.

1.6 Significant of the Study

- 1- Provision of the coconut shell is cost saving, and it is available in tropical countries like Malaysia. Thus, more economic benefits can be obtained

during utilization of coconut shells as substrate of ULW proppant, and it has great capability to convert as an economical product especially for tropical countries like Malaysia.

- 2- Coconut shells appear to be the best natural role model as proppant agent if reinforced and coated in order to increase impact-resistance. As presented in this study, CMRCP has high strength compared to the current commercial ULW proppants (ULW-1.25) that are introduced into the market.
- 3- Production process of CMRCP is safe because most of the elements that are used in the composition of CMRCP are organic materials which do not emit harmful gases, and they are degradable into nature.

1.7 Thesis Outline

The present thesis comprised of five chapters that are organized as follows:

Chapter 1: First chapter includes an overview of the study, background of the problem, problem statement, objectives, scopes and significance of the study.

Chapter2: A comprehensive review on the improved oil recovery methods, well stimulation, hydraulic fracturing and acid fracturing, HF models, HF design, proppant, history of proppant, various types of proppant such as CP and ULW proppant, physical properties of proppant, and evaluation of the quality of proppant are presented in the second chapter. In addition, this chapter is focused on the ULW proppant, historical background of ULW proppant, applications of ULW proppant, classification of ULW proppant, various arrangements of ULW proppant within the fracture, characterization of ULW proppant, simulation mechanical

response of ULW proppant under compression, quality evaluation of ULW proppant, and advantages and disadvantages of ULW proppant, coated proppant and various methods of proppant coating, diverse types of polymers that are used for coating of proppant, and fracturing fluids.

Chapter 3: Third chapter describes the procedure of performing the study that is divided into main parts such as preparation of substrate material and evaluation of its quality as well as simulating mechanical response of the uncoated coconut shells under compression, the procedure of the reinforcing and coating of desirable particle size of coconut shells in addition to simulating mechanical response of CMRCP under compression, evaluating quality of CMRCP for possible use as proppant, the trend of setting up the fracture conductivity tester, and the procedure of performing HF design.

Chapter 4: Implementation, analysis, and discussion of the various parts of the study and a comparison with other available proppants are presented in this chapter.

Chapter 5: This chapter covered conclusions and future works.

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