

NUMERICAL MODELLING AND SIMULATION FOR ONE-DIMENSIONAL
FLUID STRUCTURE INTERACTION IN BLOOD FLOW

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To my beloved father, mother and family

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ABSTRACT

Fluid structure interaction (FSI) needs to be considered in modeling biofluids because the interaction between blood flow and vessel wall is of great clinical interest. However, the interaction between blood flow and vessel wall make FSI problems complex and challenging. Spurious oscillations were observed from numerical solutions and in the case of Bubnov-Galerkin finite element method, the oscillations occurred at relatively high pressure differences. In this thesis, Streamline-Upwind Petrov Galerkin (SUPG) stabilization scheme was formulated to solve one-dimensional FSI problems in blood flow to eliminate the spurious oscillations and to obtain stable numerical solutions for stenotic vessel. A pressure-area constitutive relation to complement the continuity equation and momentum equation was formulated by adopting the collapsible model. The geometry of stenotic vessel consists of single smooth and single irregular stenosis, multi-smooth and multi-irregular stenosis in this thesis. Numerical results show that there are no vessel collapse phenomena in single smooth stenosis and multi-smooth stenosis cases. Vessel collapse phenomena are observed for single-irregular stenosis with 85% cross sectional area amplitude at distal pressure of 47 mmHg while for multi-irregular stenosis with 60% and 85% cross sectional amplitudes at proximal stenosis and distal stenosis respectively, at distal pressure of 36 mmHg. In addition, paradoxical collapse motion along the time phase cycle is obtained in unsteady cases for single irregular stenosis and multi-irregular stenosis with the distal resistance of 2.73 mmHg/(ml/s) and 2.44 mmHg/(ml/s) respectively when sinusoidal pressure variation is applied at the inlet boundary. In conclusion, numerical results show that vessel collapse phenomena occurs when there is supercritical flow at the minimum cross sectional area of the stenotic vessel which is lower than the minimum cross sectional area at static condition and hence lead to the negative transmural pressure at that position.

ABSTRAK

Interaksi struktur bendalir (FSI) perlu diambil kira dalam pemodelan *biofluids* kerana interaksi antara aliran darah dengan dinding salur pembuluh mempunyai kepentingan klinikal yang besar. Walau bagaimanapun, interaksi antara aliran darah dengan dinding salur pembuluh menjadikan masalah FSI rumit dan mencabar. Ayunan palsu telah dapat diperhatikan dari penyelesaian berangka dan dalam kes kaedah unsur terhingga *Bubnov-Galerkin*, ayunan berlaku ketika terdapat perbezaan tekanan yang agak tinggi. Dalam tesis ini, skim penstabilan *Streamline-Upwind Petrov Galerkin* (SUPG) digubal untuk menyelesaikan masalah FSI satu dimensi dalam aliran darah untuk menghapuskan ayunan palsu dan mendapatkan penyelesaian berangka yang stabil bagi salur pembuluh stenosis. Hubungan konstitutif tekanan-kawasan untuk melengkapkan persamaan keselajaran dan persamaan momentum telah diformulasi dengan menggabungkan model boleh runtuh. Geometri salur pembuluh stenosis yang terdiri daripada stenosis tunggal yang seragam dan stenosis tunggal yang tidak seragam, stenosis pelbagai yang seragam dan stenosis pelbagai yang tidak seragam digunakan dalam tesis ini. Keputusan berangka menunjukkan bahawa tiada fenomena keruntuhan salur pembuluh dalam kes stenosis tunggal yang seragam dan stenosis pelbagai yang seragam. Fenomena keruntuhan salur pembuluh telah dikesan dalam kes stenosis tunggal yang tidak seragam dengan 85% amplitud kawasan keratan rentas stenosis pada tekanan distal 47 mmHg sementara dalam kes stenosis pelbagai yang tidak seragam masing-masing dengan 60% dan 85% amplitud keratan rentas pada stenosis proksimal dan stenosis distal, pada tekanan distal di 36 mmHg. Tambahan pula, keruntuhan salur pembuluh paradox di sepanjang masa kitaran fasa telah didapati untuk kes stenosis tunggal yang tidak seragam dan stenosis pelbagai yang tidak seragam dengan rintangan distal masing-masing 2.73 mmHg/(ml/s) dan 2.44 mmHg/(ml/s) apabila variasi tekanan sinusoidal digunakan pada sempadan masuk. Kesimpulannya, keputusan berangka telah membuktikan fenomena keruntuhan salur pembuluh terjadi apabila terdapat aliran superkritikal di kawasan keratan rentas minimum salur pembuluh stenosis adalah kurang daripada kawasan keratan rentas minimum pada keadaan statik dan seterusnya membawa kepada tekanan transmural negatif pada kedudukan tersebut.

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LIST OF ABBREVIATIONS

CFD	-	Computational Fluid Dynamics
FSI	-	Fluid Structure Interaction
SUPG	-	Streamline-Upwind Petrov-Galerkin
DG	-	Discontinuous Galerkin
MUSCL	-	Monotonic Upwind Scheme for Conservation Law
<i>p-A</i>	-	Pressure-area

LIST OF SYMBOLS

t	-	Time
x	-	Axial coordinate
A	-	Cross sectional area
u	-	Velocity
c	-	Local wave speed
Q	-	Volumetric flow rate
P	-	Pressure
P_e	-	External Pressure
$P - P_e$	-	Transmural pressure
α	-	Momentum correction factor
ρ	-	Fluid density
κ	-	Viscosity friction coefficient
μ	-	Fluid dynamic viscosity
β	-	Vessel stiffness for p - A Model 1
A_o	-	Cross sectional area of the flow at reference pressure P_o
h_o	-	Vessel's wall thickness at reference pressure P_o
ν	-	Poisson ratio
E	-	Young's elastic modulus
L	-	Vessel length
A_{in}, A_{ou}	-	Flow cross sectional area at the inlet and outlet
K_p	-	Vessel stiffness for p - A Model 2
R	-	Mean flow radius
n_1, n_2	-	Tube law exponents
F_{frict}, F_f	-	Lumped loss in the flow

f_L	-	Major laminar loss
D_e	-	Hydraulic diameter
K_{sep}	-	Separation loss coefficient
A_{th}	-	Throat area of stenosis
L_s	-	Length of separation region
x_{sep}	-	Separation point
D_o	-	Nominal vessel diameter
$A_o(x)$	-	Vessel area variation
A_{oo}	-	Nominal vessel area
$\lambda_A(x)$	-	Stenosis shape function
λ_{Ao}	-	Cross sectional area reduction amplitude
x_s	-	Starting point of stenosis
x_E	-	Stopping point of the stenosis
$K_p(x)$	-	Vessel stiffness variation
K_{po}	-	Nominal vessel stiffness
$\lambda_K(x)$	-	Stiffness variation amplitude
f	-	Frequency
P_1	-	Perfusion / inlet pressure
P_2	-	Distal / outlet pressure
$\lambda_{Ao1}, \lambda_{Ao2}$	-	Cross sectional area reduction amplitude for multi-stenosis
$\lambda_{Ko1}, \lambda_{Ko2}$	-	Stiffness reduction amplitude for multi-stenosis
x_{sep1}, x_{sep2}	-	Separation point for multi-stenosis
A_{th1}, A_{th2}	-	Throat area for multi-stenosis
x_{s1}, x_{s2}	-	Starting point for multi-stenosis
x_{E1}, x_{E2}	-	Stopping point for multi-stenosis
L_{BS}	-	Length between stenosis
U	-	Matrix of dependent variables
F	-	Flux matrix
B	-	Force matrix (conservation form)
H	-	Jacobian of flux vectors
w	-	Weighting function
N_i	-	Linear shape function

$\mathbf{P}(\mathbf{w})$	-	Operator applied to the test function
$\mathbf{R}(\mathbf{U})$	-	Residual of one-dimensional FSI equations
$\boldsymbol{\tau}$	-	Stabilization parameters
$\mathbf{S}(\mathbf{U})$	-	Force matrix (quasi-linear form)
$\boldsymbol{\lambda}, \boldsymbol{\Lambda}$	-	Eigenvalues of \mathbf{H}
$\mathbf{L}, \mathbf{L}_{1,2}$	-	Left-eigenvectors of \mathbf{H}
C_{TI}	-	Time-independent compatibility conditions
C_{TD}	-	Time-dependent compatibility conditions
S	-	Speed index
R_{dis}	-	Distal resistance
A_{min}	-	Minimum cross sectional area
P_{min}	-	Minimum pressure
S_{max}	-	Maximum speed index
\bar{Q}	-	Average Flow Rate
$S1, S2$	-	Vessel position for multi-stenosis
A_{S1}, A_{S2}	-	Cross sectional area at vessel position $S1, S2$
P_{S1}, P_{S2}	-	Pressure at vessel position $S1, S2$
S_{S1}, S_{S2}	-	Speed index at vessel position $S1, S2$

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CHAPTER 1

INTRODUCTION

1.1 Research Background

Fluid structure interaction (FSI) is encountered and applicable in many different branches of engineering and science. For example, FSI is a crucial consideration in the design of many engineering systems such as aircraft and bridges. In general, FSI is defined as the interaction between the deformable structures with an internal or surrounding fluid flow. Such deformation can be either stable or oscillatory. The deformation of the structure contributes to the changes in boundary conditions of the fluid flow. Fluid flows encountered in our daily life include amongst others meteorological phenomena, environmental hazards, processes in human body such as blood flow and breathing.

FSI is more often considered in modelling biofluids because the interaction between the blood flow and vessel wall is of great clinical interest, for example, in studying cardiovascular diseases which are a major cause of death in developed countries (Mortazavinia *et al.*, 2012). The consideration of the interaction between blood flow and vessel wall had seldom being consideration in the previous studies

due to the difficulty in solving the coupled fluid and solid equations (Zhang *et al.*, 2003). Although the assumptions of the rigid wall surfaces yield results that are reasonable accurate, there are still have some considerations to be taken into such that the elastic nature of the arterial wall, stresses on the arterial wall that play crucial role in arterial disease as well as the material property alterations with the development of the atherosclerotic lesion. (Kanyanta *et al.*, 2009; Friedman *et al.*, 2010; Siogkas *et al.*, 2011).

Recent studies about the effect of rigid wall and FSI on flow distributions in arterial modelling had been carried out. The axial velocities of rigid wall are higher compared to the ones in compliant model. Such situation is explained through mass conservation theory where the internal fluid pressure exerted on the vessel wall pushes the vessel wall outward consistently and slows fluid flow due to the flow area expansion. These findings showed that incorporating FSI has significant effects on blood flow characteristics, yet FSI models are computationally expensive when the arterial geometry is highly complicated. (Lee and Xu, 2002; Siogkas *et al.*, 2011; Mortazavinia *et al.*, 2012; He *et al.*, 2016).

1.2 Problem Statement

FSI describes the wave propagation in arteries driven by the pulsatile blood flow. From theoretical point of view, such problems are complex and challenging due to high nonlinearity of the problem. Two-dimensional and three-dimensional mathematical models are solved with the aid of the commercial software or black-box solvers, yet there are some considerations such as added mass effect, coupling conditions between fluid and structure and suitable boundary conditions to avoid the wave reflection influence the numerical stability.

Despite of the numerical stability obtained from the physical problems, there is wiggling phenomena observed in computational fluid dynamics (CFD) problems especially flow with high Peclet number or high Reynolds number. Same phenomenon is expected for one-dimensional FSI blood flow problems for relatively high pressure differences. Besides, numerical formulation and simulation become complicated to include the geometrical variation of the vessel such as the spatial variation of area and corresponding stiffness resulting from the attempt to model the stenosis. Moreover, flow in stenotic vessel is further complicated when there is choked flow or flow transition where vessel collapse is observed.

Thus, sets of governing equations together with suitable boundary conditions are important to study the flow behavior in straight and stenotic vessel. Numerical technique and formulation with oscillations free is significant in ensuring the attainment of reliable information and numerical results.

1.3 Objectives of Research

The objectives of this research are specified as follows:

1. To develop numerical method based on finite element method with Streamline-Upwind Petrov-Galerkin (SUPG) stabilization scheme to solve one-dimensional blood flow in a stenosed artery.
2. To determine the effect of geometry to the flow behavior by including the irregular shape and multi-stenosis geometry.
3. To determine the effect of area reduction amplitude to the flow behavior in smooth and irregular stenosis.
4. To determine the effect of distal pressure to the flow behavior in smooth and irregular stenosis.
5. To identify the physiological conditions for vessel collapse phenomena in stenotic vessel.

1.4 Scope of Research

The scope of this study is on the numerical modelling and simulation in one-dimensional FSI blood flow cases. One-dimensional, incompressible, Newtonian flow is considered in this study. Continuity equation, momentum equation and pressure-area constitutive relation are coupled and solved numerically with the employment of compatibility conditions at the boundary nodes. Besides, finite element method with SUPG stabilization formulation is employed as space discretization and first-order forward difference is employed as time discretization. For straight vessel, two types of pressure-area constitutive relations are coupled together with continuity equation and momentum equation, that are, nonlinear elastic model and collapsible model, which are termed as $p - A$ Model 1 and $p - A$ Model 2 respectively. Pressure differences for $p - A$ Model 1 range from 400 Pa to 2500 Pa while pressure differences for $p - A$ Model 2 range from 10 mmHg to 45 mmHg.

For stenotic vessel, one-dimensional, incompressible Newtonian flow with frictional losses is considered. Collapsible model is applied as pressure-area constitutive relation to describe the flow in stenotic vessel and capture the vessel collapse phenomena. Four different geometry of stenosis are discussed, which are single smooth stenosis, single irregular stenosis, multi-smooth stenosis and multi-irregular stenosis. For single stenosis and multi-stenosis cases, cross sectional area reduction amplitude vary from 60% to 85% and stiffness reduction amplitude is set 10. Perfusion pressure is set at 100 mmHg. Distal pressure is varying from 47 mmHg to 70 mmHg for single stenosis cases and 36 mmHg to 60 mmHg for multi-stenosis cases.

1.5 Significance of Research

First of all, SUPG stabilization scheme is formulated to solve one-dimensional FSI in straight and stenotic vessel. This study is significant as this would be the first application of SUPG in the study of one-dimensional FSI blood flow problems. Besides, one-dimensional FSI governing equations are solved numerically with the employment of compatibility conditions to minimize the wave reflection at the boundary. Compatibility conditions and SUPG stabilization term are derived from the characteristic system, which emphasizing the physical nature of the problem. With the approach that proposed in this study, the understanding on the characteristic flow behavior, physiological conditions to induce vessel collapse, relationship between cross sectional area, volumetric flow rate and pressure of the flow are observed.

1.6 Outline of Thesis

This thesis consists of seven chapters, including this introduction chapter. Chapter 1 introduces the general information about the thesis, including the research background, problem statement, objectives, scopes and significance of this study. Chapter 2 presents the literature review about FSI in blood flow. The chapter begins with the difficulty and challenges of considering FSI in two-dimensional and three-dimensional mathematical models which then contributes to the research on one-dimensional FSI model. Then, the governing equations and numerical works on one-dimensional FSI in blood flow are detailed. Chapter 3 discusses about the mathematical models which are used throughout the study, including the governing equations, initial conditions and boundary conditions.

Chapter 4 deliberates about the numerical technique and formulation in the study. The chapter begins with finite element method, followed by the SUPG formulation. The formulation of SUPG involves the stabilization term, which is correspond in adding the diffusion along the characteristic direction with the appropriate stabilization parameter. Nonreflecting boundary conditions which known as compatibility conditions are derived from the characteristic system of governing equations to minimize the outgoing characteristic waves at the boundary. Eigenvalues and left-eigenvectors of the Jacobian flux vectors are solved from the method of characteristics system in order to get the time-independent and time-dependent compatibility conditions. The coupled governing equations are discretized into matrix form and solved with Newton-Raphson nonlinear iterative solver. The stability criterion is discussed and an algorithm code is presented at the end of the chapter.

Chapter 5 discusses about the steady flow in the straight vessel, followed by stenotic vessel. Bubnov-Galerkin finite element is formulated for p - A Model 1, as in the work reported in Sochi (2015). However, when Bubnov-Galerkin finite element is applied to the higher pressure difference, that is, in the range higher than reported in Sochi (2015), spurious oscillations occur. In confirming the occurrence of the oscillations, p - A Model 2 is studied. Similar phenomenon is observed for both p - A models. Hence, SUPG stabilization scheme is formulated and the numerical results are validated with the analytical solutions for both p - A models. The analytical solution for p - A Model 1 is taken from Sochi (2015) while the analytical solution for p - A Model 2 is derived. Then SUPG formulation is extended to stenotic vessel and the numerical results are compared with the numerical works in Downing and Ku (1997). SUPG numerical results are shown to eliminate spurious oscillations obtained from Bubnov-Galerkin finite element formulation and provide reliable information of the flow. Afterward, SUPG formulation is extended to parametric variations study with the irregular geometry of stenosis. Four cases are studied and vessel collapse conditions are identified for single irregular stenosis and multi-irregular stenosis. The relationship between vessel collapse, pressure and speed index is discussed.

Chapter 6 discusses about the unsteady flow in stenotic vessel. Sinusoidal time variations are applied at the inlet boundary to mimic the pressure variation of 120/80 mmHg. Initially, SUPG unsteady numerical results are compared with Downing and Ku (1997). Parametric variations study is concerned as in previous chapter. Steady flow numerical results in previous chapter are applied as the initial values of unsteady flow cases in this chapter. Effect of distal resistance for all the cases are plotted and discussed. Furthermore, vessel conditions for each phase cycle are demonstrated by the plotting of the pressure distributions along the stenotic vessel throughout the phase cycle. Finally, the thesis ends with Chapter 7. Summary of research and some suggestions for future works are stated.

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