

ACTIVE VIBRATION CONTROL OF TRANSVERSE VIBRATING
SEGMENTED MARINE RISER

NIK MOHD RIDZUAN BIN SHAHARUDDIN

A thesis submitted in fulfilment of the
requirements for the award of the degree of
Doctor of Philosophy (Mechanical Engineering)

Faculty of Mechanical Engineering
Universiti Teknologi Malaysia

MARCH 2015

In the name of Allah, The Most Gracious, The Most Merciful

To my beloved parents, Shaharuddin Bin Shaari and Nik Hasni Binti Othman, who always pray for me and who always provide me with support and encouragement that greatly contributed to the successfulness of my study.

To my siblings, Mohd Iqbal Al-Baqri, Nik Sara Syazrah, Nik Reina Nisrinah and Nik Nur Izzati who always be there for me in my life.

ACKNOWLEDGEMENT

Alhamdulillah, all praise is due to Allah S.W.T, the Most Beneficent and the Most Merciful, who has taught me what I knew not.

First and foremost, I would like to express my deepest gratitude, appreciation and recognition to my supervisor, Associate Professor Dr. Intan Zaurah Binti Mat Darus for all her advice, guidance, motivation and attention in helping me completing this research. Her extraordinary professionalism, experience and expertise in supervising me have enlightened and broaden the way of my thinking and understanding in handling research.

Special thanks to Sazli Mohd Saad who has helped me and to all my Active Vibration Control (AVC) lab mates who have assisted me directly and indirectly throughout the completion of my thesis. Last but not least, warmest affections to my beloved family for all their inspirations and encouragement in motivating me to carry out this project.

Thank You.

ABSTRACT

Vortex induced vibration (VIV) could be regarded as a fluid-structure interaction vibration type where the bluff structure vibrates due to fluid flowing around the body. The separation of boundary layer has created vortex layer that staggers the structure in cross-flow direction. VIV suppression work has attracted numerous researchers to build a passive device that could reduce the vibration. However, such device requires an intricate design which incurs high expense and indirectly contributes to higher chance of VIV occurrence due to the additional mass to the system. This research proposed a method to overcome those shortcomings by introducing an active flow control concept to the system. Since the vibration originates from unhindered flowing fluid, the approach is to avoid the development of the vortex by attaching a single control rod to the system as an actuator. The actuator injects momentum to the boundary layer thus preventing the VIV phenomenon. Both simulation and experimental works were implemented in this study. The input-output data of the system were measured directly from the experimental rig. For system identification, three methods were employed which were least square (LS), recursive least square (RLS) and differential evolutionary (DE) algorithms. It was found that the DE methods were stable, had considerably lower mean squared error (MSE) and the transfer function itself represented the natural frequency of the system. The study was continued by tuning the proportional-integral-derivative (PID) based controllers to the simulated system plant in offline mode. The PID based controllers were tuned using heuristic and Ziegler-Nichols (ZN) methods. The best performance was recorded. However, it was observed that once the disturbance of the system changed, the performance of the PID tuned using heuristic and ZN were deteriorated. To overcome this drawback, adaptive tuning algorithms were introduced, namely ZN-Fuzzy-PID and ZN-Fuzzy-Iterative Learning Algorithm-PID (ZN-Fuzzy-ILA-PID) based controllers. In simulation, it was found that the ZN-Fuzzy-ILA-PD controller outperformed other controllers with 57.82 dB of attenuation level. In experimental works, dynamic response comparison was made between the bare pipe, fixed single and double control rods. It was observed that the fixed single and double control rods could not effectively attenuate the system, but amplified the vibration instead. Further experimental work was conducted by varying the rotating speed of the actuator at various disturbances. The result shows that at 100 % actuator rotating speed with 33 Hz disturbance flow to the system, the vibration was successfully reduced with attenuation level of 20.71 dB. However, by changing the disturbance, the actuator performance was reduced. Therefore, the controller was adaptively tuned using the fuzzy and iterative learning (ILA) schemes. It was observed that the maximum vibration attenuation was achieved by ZN-Fuzzy-ILA-PD controller with 13.8 dB of attenuation level at changing disturbance. Overall results show that by adopting the single rotating control rod, the vibration of VIV could be successfully attenuated.

ABSTRAK

Pusaran induksi getaran (VIV) boleh dikenali sebagai interaksi struktur bendalir dimana struktur itu bergetar akibat daripada aliran bendalir di sekelilingnya. Pemisahan lapisan bendalir telah membentuk lapisan pusaran yang menghuyung struktur tersebut dalam arah aliran silang. Usaha mengurangkan VIV telah menarik ramai penyelidik untuk membina radas pasif yang boleh mengurangkan getaran. Walaubagaimanapun, radas tersebut memerlukan reka bentuk khusus yang memerlukan perbelanjaan tinggi dan secara tidak langsung menyumbang kepada berlakunya VIV disebabkan penambahan beban pada sistem. Kajian ini mencadangkan satu kaedah bagi mengatasi kelemahan tersebut dengan memperkenalkan konsep kawalan aliran secara aktif kepada sistem. Memandangkan getaran berasal dari aliran air tanpa halangan, pendekatannya ialah menghalang pembentukan pusaran dengan memasang satu rod kawalan pada sistem sebagai penggerak. Penggerak akan menyuntik momentum kepada lapisan sempadan lantas menghalang fenomena VIV. Kedua-dua kerja simulasi dan eksperimen telah dilaksanakan di dalam kajian ini. Data input-output sistem telah diambil secara langsung dari eksperimen. Untuk pengenalanpastian sistem, tiga cara telah digunakan iaitu kuasa dua terkecil (LS), rekursif kuasa dua terkecil (RLS) dan evolusi kebezaan (DE). Didapati bahawa kaedah DE adalah stabil, mempunyai nilai min ralat kuasa dua (MSE) terendah dan formula tersebut mewakili nilai frekuensi asli sistem tersebut. Kajian diteruskan dengan menala pengawal terbitan kamiran berkadaran (PID) pada sistem simulasi dalam mod luar talian. Kawalan berasaskan PID ditala menggunakan kaedah heuristik dan Ziegler-Nichols (ZN). Prestasi terbaik telah direkodkan. Walaubagaimanapun, apabila gangguan sistem diubah, prestasi talaan PID menggunakan heuristik dan ZN merosot. Untuk mengatasi kelemahan ini, beberapa algoritma talaan ubah suai diperkenalkan seperti ZN-Kabur-PID dan ZN-Kabur-Algoritma Pembelajaran Berlelaran-PID (ZN-Fuzzy-ILA-PID). Dalam simulasi, didapati bahawa kawalan ZN-Fuzzy-ILA-PID telah mengatasi kaedah kawalan yang lain sebanyak 57.82 dB tahap pengurangan. Dalam eksperimen, perbandingan sambutan dinamik telah dibuat di antara paip terdedah, rod kawalan tunggal dan berganda tetap. Diperhatikan bahawa rod kawalan tunggal dan berganda tidak berkesan melemahkan sistem, malah memperkuatkan getaran. Kerja eksperimen lanjutan telah dibuat dengan mengubah kelajuan pemutaran penggerak pada pelbagai gangguan. Hasil menunjukkan pada 100 % kelajuan pemutaran penggerak dan 33 Hz gangguan bendalir pada sistem, getaran telah berjaya dikurangkan dengan tahap pengurangan sebanyak 20.71 dB. Walaubagaimanapun, dengan mengubah gangguan, prestasi penggerak telah merosot. Justeru, pengawal ditala secara ubahsuai dengan menggunakan skim kabur dan pembelajaran berlelaran. Diperhatikan bahawa pengurangan getaran yang maksimum telah dicapai oleh kawalan ZN-Fuzzy-ILA-PD dengan 13.80 dB tahap pengurangan pada gangguan berlainan. Keputusan keseluruhan menunjukkan dengan mengguna pakai rod kawalan tunggal berputar, getaran VIV berjaya dikurangkan.

TABLE OF CONTENTS

CHAPTER	TITLE	PAGE
	DECLARATION	ii
	DEDICATION	iii
	ACKNOWLEDGEMENTS	iv
	ABSTRACT	v
	ABSTRAK	vi
	TABLE OF CONTENTS	vii
	LIST OF TABLES	xii
	LIST OF FIGURES	xv
	LIST OF ABBREVIATIONS	xxi
	LIST OF SYMBOLS	xxiii
	LIST OF APPENDICES	xxvi
1	INTRODUCTION	1
	1.1 Introduction	1
	1.2 Problem statement	3
	1.3 Research objectives	4
	1.4 Scope of the research	5
	1.5 Research contributions	6
	1.6 Research methodology	7
	1.7 Structure of thesis	12
2	LITERATURE REVIEW	15
	2.1 Introduction	15
	2.2 Flow theory: boundary layer separation	16

2.3	Vortex induced vibration	17
2.4	Dimensional parameters affecting VIV	22
2.5	VIV experimental method	28
2.6	Vortex induced vibration modelling	32
2.7	Vibration control method	33
2.7.1	Passive vibration control method	33
2.7.2	Active vibration and flow control method	35
2.8	Research gap	41
2.9	Concluding remarks	42
3	EXPERIMENTAL SETUP AND RESULTS	43
3.1	Introduction	43
3.2	Experimental setup	43
3.2.1	Riser model	47
3.2.2	Specification of flow generator	49
3.3	Instrumentation and data acquisition system	50
3.3.1	Accelerometer	52
3.3.2	Water flow sensor	54
3.3.3	Pump speed controller	55
3.4	VIV experimental results	57
3.4.1	Decay test	57
3.4.2	Water flow analysis	59
3.4.3	Dynamic response of flexibly mounted cylinder	60
3.5	Concluding remarks	76
4	SYSTEM IDENTIFICATION AND ACTIVE VIBRATION CONTROL	77
4.1	Introduction	77
4.2	System identification	78
4.2.1	ARX model structure	80
4.2.2	Least square identification	83
4.2.3	Recursive least square identification	88
4.2.4	Differential evolution identification	94
4.2.5	Discussion	103

4.3	Offline controller implementation	105
4.3.1	P-Controller	106
4.3.1.1	P-Control scheme results	108
4.3.2	Ziegler-Nichols PID parameter tuning	113
4.3.3	ZN-Fuzzy-PID and ZN-Fuzzy-PD controllers	120
4.3.3.1	ZN-Fuzzy-PID and ZN-Fuzzy-PD control structures	122
4.3.3.2	Rule base	123
4.3.3.3	ZN-Fuzzy-PID and ZN-Fuzzy-PD results: sinusoidal disturbance	125
4.3.3.4	ZN-Fuzzy-PID and ZN-Fuzzy-PD results: real disturbance	127
4.3.3.5	ZN-Fuzzy-PID and ZN-Fuzzy-PD results: multiple real disturbances	129
4.3.4	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD controllers	133
4.3.4.1	ZN-Fuzzy-ILA-PID controller simulation design model	135
4.3.4.2	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD results: sinusoidal disturbance	135
4.3.4.3	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD results: real disturbance	139
4.3.4.4	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD results: multiple real disturbances	142
4.3.5	Discussion	145
4.4	Concluding remarks	148
5	EXPERIMENTAL: PASSIVE AND ACTIVE OPEN LOOP VIBRATION CONTROL	149
5.1	Introduction	149
5.2	Passive control experimental setup	150
5.2.1	Passive control results	153
5.3	Active open loop control experimental setup	158
5.3.1	DC motor and coupling	158

5.3.2	Actuator instrumentation system	160
5.3.3	Matlab SIMULINK and instrument configuration	162
5.4	Active open loop control of flexibly mounted system	165
5.4.1	Control rod direction analysis	165
5.4.2	Rotation speed analysis	167
5.4.3	Varying disturbance analysis	170
5.4.3.1	Frequency response	174
5.5	Discussion	178
5.6	Concluding remarks	180
6	EXPERIMENTAL: ACTIVE CLOSED LOOP VIBRATION CONTROL	182
6.1	Introduction	182
6.2	Active closed loop control strategy	183
6.3	Experimental closed loop control based on conventional and intelligent control schemes	186
6.3.1	Controller implementation on experimental rig	186
6.3.2	Experimental results	189
6.3.2.1	Conventional strategy – ZN-P, ZN-PD and ZN-PID	189
6.3.2.2	Intelligent strategy – ZN-Fuzzy-PD, ZN-Fuzzy-ILA-PD and ZN-ILA-P	194
6.3.2.3	Frequency response analysis	198
6.3.2.4	Robustness test – additional mass	201
6.4	Discussion	203
6.5	Concluding Remarks	206
7	SIMULATION AND EXPERIMENTAL COMPARATIVE ASSESSMENT ON ACTIVE CONTROL	208
7.1	Introduction	208
7.2	Active control on simulation and experimental – discussion and comparative study	209
7.3	Concluding remarks	214

8	CONCLUSION AND FUTURE WORKS	215
8.1	Conclusion	215
8.2	Future works	219
	REFERENCES	221
Appendix	A	234

LIST OF TABLES

TABLE NO.	TITLE	PAGE
2.1	Regimes of fluid flow across circular cylinders by Lienhard (1966)	20
2.2	Literature review on mass ratio and mass damping effect on upper branch reduced velocity range and dimensional peak respectively	25
2.3	Literature review on vortex induced vibration experiment	29
2.4	Literature study on previous VIV experiment at various particulars and results	31
3.1	Experimental particulars for VIV test	49
3.2	Large volume displacement pump specification	50
3.3	PCB piezotronics accelerometer specification (Piezotronics, 2013)	52
3.4	Specification of Vernier flow rate sensor (Vernier, 2012)	54
3.5	Specification of ABB-ACS550-01-012A-4 (ABB, 2013)	57
3.6	Percentage of error between theoretical and experiment method	58
3.7	Water flow speed measurement at 25 Hz to 49 Hz pump rotation frequency	62
4.1	Least square identification results	87
4.2	MSE analysis for RLS estimation at forgetting factor, $\lambda = 0.5$	92
4.3	MSE analysis for RLS estimation at varying forgetting factor	93
4.4	MSE analysis for differential evolution optimization at varying model order	103
4.5	Optimized system identification results at 2 nd order system structure	105

4.6	Trial and error tuning results of proportional gain controller	109
4.7	Heuristic P-control attenuation level under multiple sinusoidal disturbances	111
4.8	Ziegler-Nichols PID tuning equation	113
4.9	ZN-PID based simulated control result under sinusoidal disturbance	116
4.10	ZN-PD controller magnitude under different amplitude disturbance	118
4.11	Attenuation of ZN-PID based controller magnitude under real disturbance	120
4.12	Rule-base of ZN-Fuzzy-PID based controller	124
4.13	ZN-Fuzzy-PID and ZN-Fuzzy-PD attenuation level under sinusoidal disturbance	125
4.14	ZN-Fuzzy-PID and ZN-Fuzzy-PD attenuation level under real disturbance	128
4.15	Attenuation level under multiple real disturbances	132
4.16	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD learning parameter settings	136
4.17	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD attenuation level under sinusoidal disturbance	138
4.18	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD gain parameter values under sinusoidal disturbance	138
4.19	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD attenuation level under real disturbance	141
4.20	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD based controller gain parameter values under real disturbance	141
4.21	ZN-Fuzzy-ILA-PID based controller gain parameter values multiple real disturbances	144
4.22	Initial and final value of parameter gains under multiple real disturbances	144
4.23	Performance comparison of conventional PID based controller under single sinusoidal disturbance	146
4.24	Performance of ZN-Fuzzy-PID and ZN-Fuzzy-PD controllers	147
4.25	Performance of ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD controllers	148
5.1	Open loop control attenuation level at varying actuator speed and flow disturbance	177
6.1	Ziegler-Nichols PID tuning parameter	183
6.2	Intelligent control parameters setting	183

6.3	Controller performance comparison at changing disturbance to the system	204
6.4	Controller performance comparison at additional fixed rod to the system	205
7.1	Control schemes tested in both simulation and experimental environments	210
7.2	Simulation attenuation level attained at disturbance of 31 Hz	211
7.3	Experimental attenuation level attained at disturbance of 31 Hz	212
7.4	Comparison of attenuation level attained at disturbance of 31 Hz	213

LIST OF FIGURES

FIGURE NO.	TITLE	PAGE
1.1	Typical steel catenary riser (Sparks, 2007)	2
1.2	Research strategies flowchart	11
2.1	Definition sketch for boundary layer and displacement thickness (Currie, 1993)	16
2.2	Boundary layer separation occur due to adverse pressure gradient (Sears and Telionis, 1975)	17
2.3	Relationship between Strouhal number and Reynolds number for circular cylinders (Lienhard, 1966)	21
2.4	Lift coefficient, C_L for a stationary circular cylinder as a function of Reynolds number, Re (Norberg, 2001)	22
2.5	The lock-in region from reduced velocity, U_r against mass ratio, m^* (Govardhan & Williamson 2000)	23
2.6	The two types of amplitude response based on mass-damping parameter (Khalak and Williamson, 1999)	27
2.7	The Griffin plot (Khalak and Williamson, 1996)	27
3.1	An isometric view of newly designed circulating water tank	45
3.2	Actual view of experimental tank	45
3.3	The 2D view of tank utilized in the study and flow orientation inside the tank	46
3.4	Configuration of modelled pipe riser	47
3.5	The arrangement of modelled pipe inside the circulating water tank	48
3.6	Submersible large volume displacement pump L-63 (HCP Pump, 2011)	50
3.7	Data acquisition card PCI-6259 (Instruments, 2008)	51
3.8	Connector block SCC-68 (Instruments, 2008)	51

3.9	PCB piezotronics accelerometer (Piezotronics, 2002)	53
3.10	Schematic diagram of vibration measurement system	53
3.11	SensorDAQ and Vernier flow rate sensor (Vernier, 2012)	55
3.12	Connection diagram for water flow measurement	55
3.13	The power box with ABB inverter	56
3.14	The connection diagram of the control system	56
3.15	Air decay test results	59
3.16	Still water decay test results	59
3.17	Water flow measurement at 25 Hz to 49 Hz pump speed	63
3.18	Flow water speed at corresponding pump rotation frequency	65
3.19	Amplitude response of bare circular cylinder	65
3.20	Time history response at $U_r = 2.39$ until $U_r = 7.10$	66
3.21	Frequency history response at $U_r = 2.39$ until $U_r = 7.10$	68
3.22	Vortex mode image captured	71
3.23	The flow visualization of bare pipe for 35 seconds at pump disturbance speed 29 Hz	72
3.24	The flow visualization of bare pipe for 35 seconds at pump disturbance speed 35 Hz	73
3.25	The flow visualization of bare pipe for 35 seconds at pump disturbance speed 45 Hz	74
3.26	The vortex mode region (Xu <i>et al.</i> , 2009)	75
4.1	System identification methods in establishing estimated plant system	78
4.2	Basic procedure of system identification technique (Ljung, 1999)	79
4.3	Idealized case for ARX input-output system (Mat Darus and Tokhi, 2006)	82
4.4	Measured experimental data at 37 Hz pump speed	84
4.5	Least square identification results	86
4.6	Least square pole-zero map	86
4.7	Least square correlation test results	87
4.8	RLS algorithm diagrammatic representation (Mat Darus and Tokhi, 2006)	89
4.9	Recursive least square identification results	90
4.10	Recursive least squares pole-zero map	91

4.11	Recursive least squares correlation test results	91
4.12	RLS parameter estimation convergence profile of a 2 nd order ARX model parameter	92
4.13	Mutation process within DE algorithm	95
4.14	Crossover process within DE algorithm	96
4.15	Selection process within DE algorithm	97
4.16	Block diagram of ARX parameter estimation using DE algorithms	100
4.17	Differential evolution identification results	101
4.18	Differential evolution pole-zero map	101
4.19	Differential evolution algorithm correlation test results	102
4.20	DE parameter estimation convergence profile of a 2 nd order ARX model parameter	102
4.21	Proposed active vibration control strategy for flexibly mounted system	106
4.22	The basic P-controller scheme	107
4.23	Convergence of MSE value against increasing P gain value	109
4.24	Heuristic P-control system response under sinusoidal disturbance (Frequency, $f_D = 1.074$ Hz, Amplitude, $A_D = 0.27$ m/s)	110
4.25	Different flow speed amplitude tested to the system	111
4.26	Heuristic P controlled system response under multiple sinusoidal disturbances	112
4.27	Heuristic P controlled frequency response under multiple sinusoidal disturbances	112
4.28	Period of oscillation identified from $K_u=100$	114
4.29	ZN-PID based control scheme system response under sinusoidal disturbance	115
4.30	ZN-PID based control scheme frequency response under sinusoidal disturbance	115
4.31	ZN-PD controlled system response under multiple sinusoidal amplitude disturbances	117
4.32	ZN-PD frequency response under multiple sinusoidal amplitude disturbances	117
4.33	Actual flow speed disturbance exerted to the vibrating system	119
4.34	ZN-PD time history response under real disturbance	119

4.35	ZN-PD frequency response under real disturbance	119
4.36	ZN-Fuzzy-PID tuned strategy controller	121
4.37	The Matlab SIMULINK ZN-Fuzzy-PID controller diagram	121
4.38	Input membership function	122
4.39	Output membership function	123
4.40	Surface view of fuzzy parameter gains	124
4.41	ZN-Fuzzy-PID and ZN-Fuzzy-PD time history response under sinusoidal disturbance (Frequency, $f_D = 1.074$ Hz, Amplitude, $A_D = 0.27$ m/s)	126
4.42	ZN-Fuzzy-PID and ZN-Fuzzy-PD frequency response under sinusoidal disturbance	126
4.43	ZN-Fuzzy-PID and ZN-Fuzzy-PD parameter gains under sinusoidal disturbance	127
4.44	ZN-Fuzzy-PID and ZN-Fuzzy-PD time history response under real disturbance	128
4.45	ZN-Fuzzy-PID and ZN-Fuzzy-PD frequency response under real disturbance	129
4.46	ZN-Fuzzy-PID and ZN-Fuzzy-PD gain parameters under real disturbance	130
4.47	Multiple flow speed disturbance exerted to the vibrating system	131
4.48	ZN-Fuzzy-PID and ZN-Fuzzy-PD time history response under multiple real disturbances	131
4.49	ZN-Fuzzy-PID and ZN-Fuzzy-PD frequency response under multiple real disturbances	132
4.50	ZN-Fuzzy-PID and ZN-Fuzzy-PD gain parameters under multiple real disturbances	133
4.51	The PID-type iterative learning algorithm scheme	134
4.52	The ZN-Fuzzy-ILA-PID based strategy block diagram	134
4.53	SIMULINK diagram for ZN-Fuzzy-ILA-PID based control system	135
4.54	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD time history response under sinusoidal disturbance (Frequency, $f_D = 1.074$ Hz, Amplitude, $A_D = 0.27$ m/s)	137
4.55	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD frequency response under sinusoidal disturbance	138
4.56	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD gain parameters under sinusoidal disturbance	139
4.57	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD time history	

	response under real disturbance	140
4.58	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD frequency response under real disturbance	141
4.59	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD gain parameters under real disturbance	142
4.60	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD time history response under multiple real disturbances	143
4.61	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD frequency response under multiple real disturbances	144
4.62	ZN-Fuzzy-ILA-PID and ZN-Fuzzy-ILA-PD gain parameters under multiple real disturbances	145
5.1	Cross section view of control rod arrangement beside the main pipe	151
5.2	Actual view of control rod configuration beside the main pipe	152
5.3	Data collecting arrangement for passive control	153
5.4	Time history response of the flexibly mounted system	155
5.5	The amplitude ratio over reduce speed plot at various reduce speed for all cases	156
5.6	Frequency response of modelled pipe at various reduced speed, U_r	157
5.7	Schematic diagram of permanent magnet DC motor (Moreton, 2000)	159
5.8	Actuator system for active vibration control	159
5.9	Arrangement of actuator in controlling vibration	160
5.10	MD10C integration circuit diagram	161
5.11	MD10C motor driver hardware (Technologies, 2013)	161
5.12	Time sample configuration in Matlab SIMULINK	162
5.13	Channel configuration in Matlab SIMULINK	163
5.14	The basic SIMULINK block used for analog input and output	164
5.15	CCW rotating direction response results	166
5.16	CW rotating direction response results	167
5.17	Time history response under various actuator control speed at 33 Hz	169
5.18	Attenuation level under various actuator control speed at 33 Hz	169
5.19	Enlarge view of frequency response under various actuator control speed at 33 Hz	169

5.20	Time history response of vibrating system under open loop control	171
5.21	The comparison of V_{rms} values between uncontrolled and controlled system at various actuator speed over different disturbance	173
5.22	Frequency response at various disturbance speed	174
6.1	Vibration signal manipulation	184
6.2	Simulink model of modified vibration signal	185
6.3	Schematic diagram of instrumentation configuration	185
6.4	Controllers block diagram	187
6.5	The schematic diagram of conventional and intelligent control schemes in Matlab SIMULINK	188
6.6	Experimental time response of vibration suppression for ZN-P	191
6.7	Experimental time response of vibration suppression for ZN-PD	192
6.8	Experimental time response of vibration suppression for ZN-PID	193
6.9	Experimental time response of vibration suppression for ZN-Fuzzy-PD controller	195
6.10	Experimental time response of vibration suppression for ZN-Fuzzy-ILA-PD controller	196
6.11	Experimental time response of vibration suppression for ZN-ILA-P controller	197
6.12	Frequency response of vibrating system at 31 Hz of disturbance	199
6.13	Frequency response of vibrating system at 35 Hz of disturbance	200
6.14	Vibration signal for robustness test	201
6.15	Frequency response of vibrating system with additional fixed rod	202

LIST OF ABBREVIATIONS

A/D	-	Analog to digital converter
AC	-	Alternate current
ANFIS	-	Adaptive neuro-fuzzy inference system
ARX	-	Auto-regressive with exogenous input
AVC	-	Active vibration control
CCW	-	Counter clockwise
CFD	-	Computational fluid dynamic
CR	-	Crossover
CW	-	Clockwise
D/A	-	Digital to analog converter
DAC	-	Disturbance accommodating control
DAQ	-	Data acquisition system
DC	-	Direct current
DE	-	Differential evolutionary
F	-	Mutation intensity
FFT	-	Fast fourier transform
GA	-	Genetic algorithm
ILA	-	Iterative learning algorithm
LS	-	Least square
MGA	-	Modified genetic algorithm
MIMSC	-	Modified independent modal space control
MSBC	-	Moving surface boundary control
MSE	-	Mean squared error
NF	-	Natural frequency
NI	-	National Instrument

NL	-	Negative large
NN	-	Neural network
NP	-	Population size
NS	-	Negative small
P	-	Proportional
PC	-	Personal computer
PD	-	Proportional derivative
PI	-	Proportional integral
PID	-	Proportional integral derivative
PL	-	Positive large
PS	-	Positive small
RLS	-	Recursive Least Square
ROV	-	Remote operated vehicle
TF	-	Transfer function
TTW	-	Traveling wave wall
V	-	Voltage
VIV	-	Vortex induced vibration
ZE	-	Zero
ZN	-	Ziegler-Nichols

LIST OF SYMBOLS

$A(q)$	-	Polynomials parameters of autoregressive
A/D	-	Amplitude ratio
a_c	-	Characteristic area
a, b	-	Unknown system parameter to be identified
$B(q)$	-	Polynomials parameters of exogenous
C_A	-	Added mass coefficient
C_L	-	Lift coefficient
CR	-	Crossover constant
c	-	Damping coefficient
D	-	Main pipe diameter
D_c	-	Control cylinder diameter
D/D_c	-	Main pipe over control cylinder diameter ratio
dB	-	Decibel
de/dt	-	Change of error
d_{im}	-	Dimensionality
$\xi(k)$	-	System white noise
e	-	Error
$\varepsilon(k)$	-	Model prediction error
F	-	Mutation constant
F_N	-	Natural frequency
F_L	-	Lift force
F_v	-	Vibrating frequency
f_{shed}	-	Shedding frequency
$G(q, \theta)$	-	Deterministic part
$H(q, \theta)$	-	Stochastic part

J	-	Least square estimation
K_I	-	Integral gain
K_D	-	Derivative gain
K_P	-	Proportional gain
K_S	-	System stiffness
k	-	Spring coefficient
k_s	-	Roughness height
L	-	Main pipe length
L_s	-	Main pipe submerged length
L_c	-	Control cylinder length
L/D	-	Main pipe length over diameter ratio
L_c/D_c	-	Control cylinder length over diameter ratio
λ	-	Forgetting factor
M_T	-	Total Mass
m^*	-	Mass ratio
m	-	Cylinder mass
m_L	-	Oscillating mass
m_a	-	Added mass
m_d	-	Displaced mass
μ	-	Dynamic viscosity
NP	-	Population size
n_u, n_y	-	Model orders
Θ	-	Dimensional parameter sets in matrix form
Φ_P	-	Proportional learning parameter
Ψ_I	-	Integral learning parameter
Γ_D	-	Differential learning parameter
ρ	-	Density
q^{-1}, z^{-1}	-	Back-shift operator
Re	-	Reynolds number
S_t	-	Strouhal number
S_p	-	Schewe parameter
U	-	Velocity
U_r	-	Reduce speed

$u(t)$	-	System input
$u_{j,G+1}$	-	Trial vector
V	-	Voltage
$v_{j,G}$	-	Mutant vector
x	-	Displacement
$x_{ri,G}$	-	Target vector
Y	-	System output sets in matrix form
$y(t)$	-	System output
$y(k)$	-	Output measurement
y_d	-	Desired output
y_p	-	Output prediction

LIST OF APPENDICES

APPENDIX	TITLE	PAGE
A	List of publications	234

CHAPTER 1

INTRODUCTION

1.1 Introduction

Currently, the rapid growth of oil and gas industry activity has become more significant around the world as reservoir exploration has been expanded from shallow to deep water areas. Marine riser is an important structure that needs to be carefully designed and maintained as failure of these structures would lead to massive loss to humans and the environment. Figure 1.1 shows a typical steel catenary riser which acts as a channel flow for oil and gas to be conveyed from wellhead to the platform. There are many types of marine riser based on its function such as drilling riser, production riser, completion/work-over riser and export riser (Sparks, 2007). It is known that marine riser is one of the most common slender structures that are prone to vortex induced vibration phenomenon which in many cases causes fatigue damage to the vibrating structure (Xu *et al.*, 2009).

Vortex induced vibration (VIV) could be regarded as vibration phenomenon which occurs to the structure, either in air or water. As the flow passes a bluff body at sufficiently large Reynolds number, vortices will be shed at the trailing edge of the body, creating fluctuating lift force due to pressure difference on the body surface that pulls the body from side to side across the wake. This lift force eventually will

create cross-flow vibrations. The source of the vibration is mainly from the vortex formed aft of the body. This phenomenon is known Vortex Induced Vibration. (Blevins, 1990; Daei-Sorkhabi and Zehsaz, 2009). This kind of fluid-structure interaction phenomenon has been widely investigated and reviewed previously in both numerical and experimental works. Details can be found in Bearman, (2011), Gabbai and Benaroya, (2005) and Sarpkaya, (2004).

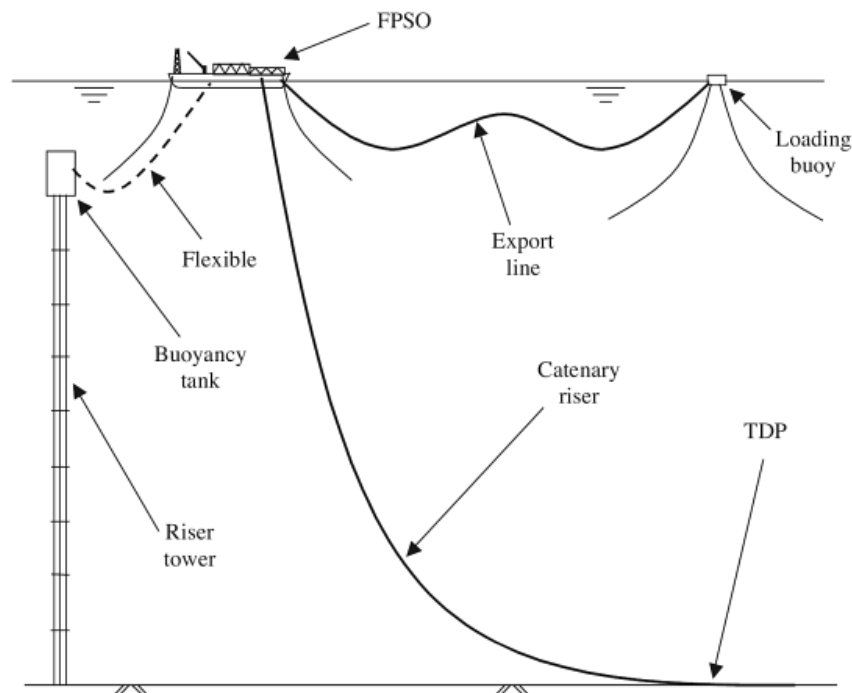


Figure 1.1: Typical steel catenary riser (Sparks, 2007)

The effect of vortex induced vibration in the water is more significant as the natural frequency is lowered due to the presence of the added mass (Yang *et al.*, 2010). Also, as in deeper water area, an increased length of riser pipe will lower its natural frequency correspondingly (Allen, 1998). Thus, the possibility of resonance is very high. If the vibration is not well controlled, it would lead to resonance problem and much more importantly, fatigue failure of the riser will occur over extended periods of time mainly due to resonance of cross-flow vibration in deeper water area. Fatigue study related to the VIV phenomenon can be found in Campbell, (1999), Cunffl *et al.*, (2002) Martins *et al.*, (1999) and Mukundan *et al.*, (2009).

Some typical example of disasters related to vortex induced vibration during resonance are the collapse of Tacoma Narrows Bridge and the destruction of piling of an oil terminal on the Humber estuary in 1960s (Griffin and Ramberg, 1976). These catastrophic incidents justify the need to suppress vibration in order to avoid the occurrence of resonance by way of any controlling method particularly for risers in deeper water area. Consequently, research on controlling vortex induced vibration has attracted the attention of researchers around the world.

Two distinct methods, which are passive and active control methods, are used to prevent the occurrence of VIV phenomena (Kumar *et al.*, 2008). In the perspective of VIV, passive control strategy is a method to attenuate the VIV phenomena by disturbing or eliminating the formation of vortices behind the pipe. This is achieved by introducing additional fixed or free to rotate shaped geometrical structures along the pipe. Conversely, in active vibration control strategy, an actuator is introduced at certain locations along the pipe where maximum vibration occurs. In this research, a secondary small rotating rod is introduced to the vibrating system which acts as an actuator that will rotate based on structure vibration. The rotating rod will inject momentum to the boundary layer thus eliminating the vortex formation behind the pipe (Modi, 1997).

1.2 Problem statement

Passive control strategy has always been the best choice for offshore industry to suppress the vortex induced vibration for marine riser. Researchers have developed and constructed various types of passive devices in the last few decades due to their high confidence level that these devices could deliver its task. Although proven successful in attenuating vibration, there are still some shortcomings of this method such as increasing drag force along the pipeline, barnacle problems, expensive, difficult to handle and modifies their geometrical structure (Kumar *et al.*,

2008). Also, it is found that the passive devices do not completely eradicate the vortex induced vibration at low mass and damping which often occurs in marine applications (Gabbai and Benaroya, 2005).

By introducing the active vortex control method to the marine riser, the disadvantages associated with passive control strategy and actuator installation difficulties could be reduced since the proposed method could control the vibrating structure without requiring enormous structural additions to the pipe as compared to passive method. In addition, there are no control region limitations and they are relatively easy to mantle and dismantle from the vibrating system. With the state-of-the-art technology available nowadays, the active control strategy could be implemented and accepted by industry as it could increase the reliability and lengthen the life service of marine riser.

1.3 Research objectives

The objectives of the current research are as follows:

- i) To model the offshore marine riser using system identification techniques.
- ii) To investigate adaptive active vibration control (AVC) algorithms using conventional and intelligent methodologies.
- iii) To assess and validate the thus developed algorithms for vibration control of flexible cylinder via simulation and experimental work.
- iv) To compare the performance of all thus developed algorithms in vibration reduction of the structure.

1.4 Scope of the research

The scope of the research includes:

- i) Modelling an offshore marine riser using parametric identification approach such as least square (LS), recursive least square (RLS) and differential evolutionary (DE) algorithms via system identification method.
- ii) Development and fabrication of a lab scale experimental rig for representation of the vibration of an offshore marine riser using flexibly mounted cylinder.
- iii) Development and integration of data acquisition (DAQ) and instrumentation systems for acquiring input-output vibrational data from the experimental rig.
- iv) Development of adaptive active vibration control (AVC) algorithms using conventional and intelligent methodologies, namely heuristically tuned P controller, PID based controller tuned using Z-N method, Fuzzy PID based controller and Fuzzy iterative PID based controllers.
- v) The developed algorithms are assessed and validated for vibration suppression of the flexibly mounted cylinder via simulation and experimental work.
- vi) Comparison of the performance of all thus developed algorithms in vibration reduction of the structure.

1.5 Research contributions

A brief outline of the main contributions of this research is given in the subsection as follows:

1. This research has conducted the design, fabrication and development of miniature water circulating tank that utilize a submersible large-volume displacement water pump in generating disturbance throughout the water tank. Various amplitudes of disturbance could be generated and controlled through an inverter from a single personal computer (PC). Since aluminium profile is used as its structure, a unique experimental rig based on respective research study could be installed and assembled easily onto the tank. With this characteristic, the developed miniature water tank could be used for other kinds of small underwater studies such as vibration control, harnessing energy device, remote operated vehicle (ROV), propulsion test and so forth. In current research, the active control of vortex induced vibration phenomenon is studied.
2. This research has contributed in developing the dynamic response of the vortex induced vibration phenomenon by using parametric system identification technique. This approach differs from other mathematical and physical models which use both input and output data from experiment in constructing the equation of the vibrating system based on the auto-regressive with exogenous input (ARX) structure model. Three parameter estimation techniques such as least square, recursive least square and differential evolutionary algorithms are tested for VIV-ARX model structure. The estimated model is verified by comparing its natural frequency with the true natural frequency obtained from the decay test. Among the identified models, mean squared error (MSE), stability and correlation test are performed in order to determine the best model that represents the vibrating system.

3. This research has contributed in investigating the real implementation of cancelling the vortex induced vibration phenomena by using a single rotating rod which is placed perpendicular (90° or -90°) to the water flow direction. The proportional, integral and derivative (PID) controller has been adapted to the system. Before implement to the experimental works, the modelled vibrating system is controlled within the simulation environment in order to pre-determine the appropriate gains for PID controller. Later, the performance of the simulated controllers is validated experimentally. Another novel contribution of this research is the online self-tuning fuzzy and iterative PID based controllers which can be implemented and validated experimentally.

4. This research has contributed by proposing a method in solving the closed loop control problem encountered during experimental validation. Problem arises as the actuator rotate in both clock wise and counter-clock wise directions, which are due to the sinusoidal vibration signal. In solving this, the sinusoidal vibration signal acquired from the sensor is manipulated to root mean square (RMS) value before being fed into the controller. By manipulating the sensor signal, a single direction of actuator rotation is attained and has enabled proper investigation of closed loop control strategy.

1.6 Research methodology

Methodology is an outline research steps. This outline or frame work is important as it will determine the successfulness of this study. Figure 1.2 shows all the steps involved from the beginning until the end of the research. An explanation of the framework is as follows:

Identifying Research Problem: In vibration study, particularly in marine riser application, the implementation of passive control devices such as helical strake, fairings and other flow disturbance devices onto marine riser pipe has some drawbacks as stated by previous researchers. Also, the probability of resonance occurrence is high due to additional mass and increased length of the marine structure in deep water areas. Thus, this research is conducted in order to improve some of these shortcomings by implementing the active vortex control device using a single rotating control rod on the modelled pipe.

Literature Study: The literature review is organized into three major parts which are. The vortex induced vibration phenomena, control method and finally the research gap. The vortex induced vibration part includes the theory behind the occurrence of VIV phenomena, previous experimental design, and data collection technique. As for controller part, it includes the passive and active control methods. Under active control method, all previous works in suppressing the vortex induced vibration phenomena using actuators is briefly described.

Rig Design, Development and Fabrication: Literature study on vortex induced vibration experiment has been performed in order to obtain an idea on how previous experiments were conducted. Information regarding the dimension of pipe, spring system, rig design and instrumentation used in obtaining both input and output data are reviewed. After reviewing all previous designs based on miniature, simplicity and limitation characteristics, a final experimental design is produced. To measure vibration, an integrated comprehensive instrumentation and data acquisition system is crucial. Accelerometer is used in capturing the vibration data. However, for the sake of data analysis, displacement signal is retrieved in order to describe how the system behaves. Also, the VIV response towards various water flow speed is studied. The overall amplitude ratio over reduced velocity for the vibration system is plotted in a single graph. The actual natural frequency of the vibration system is determined from the decay test.

VIV System Identification: For this research, system identification technique will be utilized in representing the dynamic response of the vortex induced vibration. The data taken solely from experimental works will be used to describe how the cylinder behaves against the disturbance generated inside the circulating water tunnel. The water flow speed in the test section area is considered as an input to the vibrating system since the pipe vibrates according to the flow speed, while the vibration of the pipe is considered as an output of the system. The data obtained from the experimental works are employed in order to develop the ARX model structure. Three parameter estimation techniques namely LS, RLS and DE are used to optimize the ARX model structure. The natural frequency obtained from the system identification is compared with the actual natural frequency obtained from decay test. Comparative studies in terms of MSE, stability and correlation test are conducted in order to find the best model that represents the VIV phenomena. The best model that characterizes the vibrating system will be used in designing the PID controller in the simulation environment and later will be implemented experimentally.

Simulation on Active Vortex Control Strategy: At this stage, the system identification of VIV phenomena has been conducted. Prior to actual implementation of controller onto experimental rig, it is crucial to design the controller for active control of the vibrating system in simulation environment. Matlab SIMULINK software is utilized for such purpose. Initially, the P-controller is utilized as the control scheme. The proportional gain is tuned heuristically until the maximum attenuation is achieved. The effects of integral and derivative gains are studied by implement the Ziegler-Nichols tuning rules. The robustness of the system is tested by changing the disturbance to the system. The conventional tuning rules could not maintain the controlled signal thus an adaptive controller is crucial to be introduced to the system. ZN-Fuzzy-PID and ZN-Fuzzy-ILA-PID controllers are developed and its robustness is tested. Results obtained from all developed controller schemes are compared in terms of its attenuation level at first mode of vibration and robustness toward dynamic disturbance to the system.

Experimental works on Active Vortex Control: Initially, the cylindrical rod which used as an actuator in controlling the VIV is fixed besides the main pipe. The purpose is to study the performance of the fixed actuator rod to the vibrating system as a passive control strategy. Next, the investigation is conducted by rotating the actuator rod in both clockwise (CW) and counter clock wise (CCW) directions at various actuator rotation speeds. The same actuator rod speed variation study is also conducted at variation of water flow disturbance speed. The study is known as open loop control where the control action is implemented directly without considering the system output. The performance of passive and active open loop control are recorded. Later, the closed loop control strategy is conducted experimentally by feeding the system output to the controller. Conventional and intelligent controllers are tested in the closed loop control scheme and the performance of all developed controllers is studied. The robustness of the control schemes are tested experimentally by changing the water flow speed as the disturbance to the system.

Comparative and Performance Analysis: A comparative study between the simulation and experimental results were carried out and described in Chapter 7. The purpose of comparative study and performance analysis is to observe the performance of the developed controller. The overall performance of the control scheme is concluded.

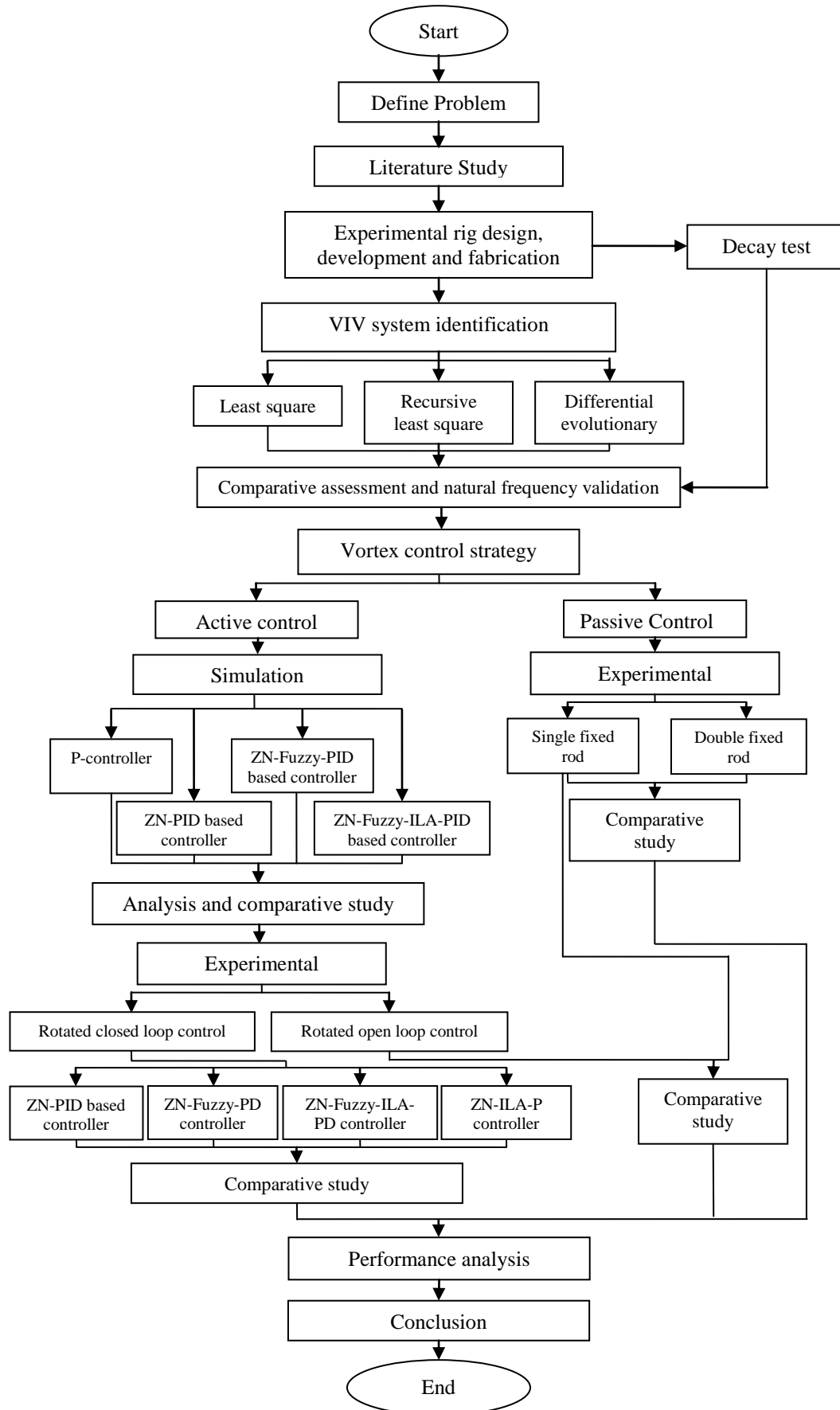


Figure 1.2: Research strategies flowchart

1.7 Structure of thesis

This thesis is organized into eight chapters. A brief outline of contents of the thesis is as follows:

Chapter 1 presents an introduction to the research problem. It includes the research background, problem statements as well as the research objective and scope. The structure of the thesis is also outlined in this chapter.

Chapter 2 is devoted to a literature study on vortex induced vibration exerted on bluff body. Then, literature studies on vibration controlling method are discussed. There are two well-known methods used in attenuating the VIV which are passive and active vibration control. All related VIV control studies using active control are presented. Finally, the research gap found in the active control of VIV study is identified in this chapter.

Chapter 3 describes the experimental setup and the VIV results obtained in this study. Both mechanical and instrumentation parameters are briefly explained in this chapter. This chapter also presents a description of the circulating tank, pipe rig structure and the water flow generator used in this research. As for the instrumentation section, the data acquisition, sensors, flow generator controller and actuator description are explained in detail. The decay test result, water flow analysis and the dynamic response of pipe are presented at the end of this chapter. Results obtained are verified with experimental results on VIV phenomenon by previous researchers.

Chapter 4 presents the system identification technique employed in VIV problem. In this chapter there are two distinct parts which are system identification and control simulation. In system identification, the ARX model is used to represent the system.

The LS, RLS and DE algorithms are used as the optimization tools in obtaining the parameters of the ARX model. Comparison among the stated tools in terms of natural frequency, mean squared error, stability and correlation tests are done. The transfer function that best represents the vibrating system is used as the system plant to be controlled in the simulation part. Several control schemes which are heuristically tuned P-controller, ZN-PID, ZN-Fuzzy-PID and ZN-Fuzzy-ILA-PID based controllers are discussed. Robustness of the developed controllers is tested.

Chapter 5 presents the result of passive and active open loop control studies. In passive control study, the effects of inserting a single and double fixed rod upon the bare pipe system are investigated. Initially, a single rod is assembled at 90° with respect to direction flow. The dynamic response of the passive single rod control system is recorded at various water flow speeds. Then, another rod is added to the system, which is fixed at the opposite location of previous one or -90° with respect to direction flow. The dynamic response of passive double rod control is examined. The results obtained from both single and double rod controls are compared with the bare pipe results, which have already been achieved in chapter 3. Discussions and comparisons are made among the bare pipe, single and double passive rod control.

The study continues by rotating the single rod at CW and CCW direction. The dynamic responses of the vibrating system are recorded for both rotating directions. The effect of rotating direction upon the vibrating system is studied. As the effective direction is achieved, the study continues by rotating the single rod at various rotation speeds under constant disturbance to the system. The speed is defined as the value of voltage supplied to the single rod. A miniature 12 V direct current (DC) motor is used for such purpose. The single rod rotation study is tested at changing disturbance. The effective rotation speed at respective disturbance is achieved from this study. Discussions and comparisons are made between the fixed single control rod and rotating single rod control.

Chapter 6 presents the closed loop implementation on the experimental rig. As much as 6 controllers are tested on the experimental rig, which consist both conventional and intelligent controllers. The controllers are ZN-P, ZN-PD, ZN-PID, ZN-Fuzzy-PD, ZN-Fuzzy-ILA-PD and ZN-ILA-P. It is noted that the values of the gain parameter used in all controllers are based on the simulated values as described in chapter 4 of this thesis. As for actuator, the study proposes a control strategy where the vibration signal measured by accelerometer is converted into RMS value. The control scheme will operate based on the converted value. In order to demonstrate the robustness of the developed controllers, the disturbance exerted on the vibrating system is increased and additional fixed rod is attached to the vibrating system. The attenuation level for all controllers upon the vibrating system is recorded. Comparisons are made between the conventional and intelligent controller performance.

Chapter 7 compares the performance of the implemented controllers in both simulated and experiment environments. The steps involved in obtaining the simulation results are recalled. The purpose is to ensure that the same condition such as the disturbance exerted on the system and the same control schemes are implemented in both simulation and experiment environments. As much as 5 controllers are compared which are ZN-P, ZN-PD, ZN-PID, ZN-Fuzzy-PD and ZN-Fuzzy-ILA-PD. The attenuation level achieved by the tested controller in simulation and experiment is tabulated separately. Then the percentage of attenuation level from both environments is compared.

Chapter 8 summarizes the work presented and draws some relevant conclusions. The future works on active control of VIV phenomena are discussed.

REFERENCES

- ABB (2013). ABB–ACS550–01–012A–4, Johor Bahru, Malaysia.
- Ahn, H. - S., Chen, Y. Q., and Moore, K. L. (2007). Iterative learning control: Brief survey and categorization. *IEEE Transactions on Systems, Man and Cybernetics Part C: Applications and Reviews*. 37(6), 1099-1121.
- Anh, H. P, H and Ahn, K. K. (2009). Identification of Pneumatic Artificial Muscle Manipulators by a MGA-Based Nonlinear NARX Fuzzy Model. *Mechatronics*. 19(1), 106 – 133.
- Allen, D. W. (1998). Vortex-Induced Vibration of Deepwater Risers. *Proceedings of the Offshore Technology Conference-OTC 8703*. 4 May. Houston, Texas, 209-215.
- Allen, D.W. and Henning, D. L. (2001). *U.S Patent No. 6,223,672 B1*. Washington, DC: U.S.
- Allen, D. W. and Henning, D. L. (2003). Vortex-Induced Vibration Current Tank Tests of Two Equal-Diameter Cylinders in Tandem. *Journal of Fluids and Structures*. 17(6), 767-781.
- Asim, T., Sendanayake, I., Mishra, R., Zala, K. and Ubbi, K. (2013). Effects of a Moving Surface Boundary Layer Control Device (MSBC) on the Drag Reduction in Heavy Commercial Vehicles. *Proceedings of the 40th National Conference on Fluid Mechanics & Fluid Power*. 12-14 December. NIT Hamirpur, Himachal Pradesh, India.
- Assi, G. R. S., Meneghini, J. R., Aranha, J. A. P., Bearman, P. W. and Casaprima, E. (2006). Experimental Investigation of Flow-Induced Vibration Interference between Two Circular Cylinders. *Journal of Fluids and Structures*. 22(6-7), 819-827.

- Assi, G. R. S., Bearman, P. W. and Kitney, N. (2009). Low Drag Solutions for Suppressing Vortex-Induced Vibration of Circular Cylinders. *Journal of Fluids and Structures*. 25(4), 666-675.
- Balas, G., Doyle, J., Glover, K., Packard, A. and Smith, R. (1998). *μ -Analysis and Synthesis Toolbox: for Use with Matlab, User's Guide Version 3*. Natick, Massachusetts, U.S.A.: MUSYN Inc.
- Baz, A. and Poh S. (1988). Performance of an Active Vibration Control System with Piezo-Electric Actuators. *Journal of Sound and Vibration*. 126(2), 327-343.
- Baz, A. and Ro, J. (1991). Active Control of Flow-Induced Vibrations of a Flexible Cylinder using Direct Velocity Feedback. *Journal of Sound and Vibration*. 146(1), 33-45.
- Baz, A. and Kim M. (1993). Active Modal Control of Vortex-Induced Vibrations of a Flexible Cylinder. *Journal of Sound and Vibration*. 165(1), 69-84.
- Baz, A., and Kim, M. (1994). Authors' Reply. *Journal of Sound and Vibration*, 175(1), 137.
- Bearman, P. W. and Brankovic, M. (2006). Measurements of Transverse Forces on Circular Cylinders Undergoing Vortex-Induced Vibration. *Journal of Fluids and Structures*. 22, 829-836.
- Bearman, P. and Branković, M. (2004). Experimental Studies of Passive Control of Vortex-Induced Vibration. *European Journal of Mechanics - B/Fluids*. 23(1), 9-15.
- Bearman, P. W. (2011). Circular Cylinder Wakes and Vortex-Induced Vibrations. *Journal of Fluids and Structures*. 27(5-6), 648-658.
- Blackburn, H. M., Govardhan, R. N. and Williamson, C. H. K. (2001). A Complementary Numerical and Physical Investigation of Vortex-Induced Vibration. *Journal of Fluids and Structures*. 15(3-4), 481-488.
- Blevins, R. D. (1984). Review of Sound Induced by Vortex Shedding from Cylinders. *Journal of Sound and Vibration*. 92(4), 455-470.
- Blevins, R. D. (1990). *Flow Induced Vibration*. New York: Van Nostrand Reinhold Company.
- Blevins, T. (2012). PID Advances in Industrial Control. *Proceedings of IFAC Conference on Advances in PID Control*. 28-30 March. Brescia, Italy.

- Blevins, R. D. and Coughran, C. S. (2009). Experimental Investigation of Vortex-Induced Vibration in One and Two Dimensions with Variable Mass, Damping, and Reynolds Number. *Journal of Fluids Engineering*. 131(10), 101-202.
- Bloor, M. S. (1964). The Transition to Turbulence in the Wake of a Circular Cylinder. *Journal of Fluid Mechanics*. 19(2), 290-304.
- Bosch, P. P. J., and Klauw, A. C. (1994). *Modeling, Identification, and Simulation of Dynamical Systems*. Boca Raton: CRC Press.
- Braaten, H., Lie, H. and Skaugset, K. (2008). Higher Order Modal Response of Riser Fairings. *Proceedings of ASME 2008 27th International Conference on Offshore Mechanics and Arctic Engineering*. 15-20 June. Estoril, Portugal. 969-978.
- Branković, M. and Bearman, P. W. (2006). Measurements of Transverse Forces on Circular Cylinders undergoing Vortex-Induced Vibration. *Journal of Fluids and Structures*. 22(6-7), 829-836.
- Buresti, G., Iungo, G. V. and Lombardi, G. (2007). *Methods for the Drag Reduction of Bluff Bodies and their Application to Heavy Road-Vehicles*. 1st Interim Report Contract between CRF and DIA.
- Campbell, M. (1999). The Complexities of Fatigue Analysis for Deepwater Risers. *Proceedings of the Deepwater Pipeline Technology Conference*. March. New Orleans, 1-13.
- Carbonell, P., Wang, X. and Jiang, Z.-P. (2003). On the Suppression of Flow-Induced Vibration with a Simple Control Algorithm. *Communications in Nonlinear Science and Numerical Simulation*. 8(1), 49-64.
- Chen, S. S. (1987). *Flow-Induced Vibrations of Circular Cylindrical Structures*. New York: Hemisphere Publishing Corporation.
- Chen, W.-L., Xin, D. B., Xu, F., Li, H., Ou, J. P. and Hu, H. (2013). Suppression of Vortex-Induced Vibration of a Circular Cylinder using Suction-Based Flow Control. *Journal of Fluids and Structures*. 42, 25–39.
- Chen, W., Liu, Y., Xu, F., Li, H. and Hu, H. (2014). Suppression of Vortex Shedding from a Circular Cylinder by using a Traveling Wave Wall. *Proceedings of the 52nd Aerospace Sciences Meeting American Institute of Aeronautics and Astronautics*. 13-17 January 2014, National Harbor, Maryland, 1-11.

- Cheng, L., Zhou, Y. and Zhang, M. M. (2003). Perturbed Interaction between Vortex Shedding and Induced Vibration. *Journal of Fluids and Structures*. 17(7), 887-901.
- Cheng, L., Zhou, Y. and Zhang, M. M. (2006). Controlled Vortex-Induced Vibration on a Fix-Supported Flexible Cylinder in Cross-Flow. *Journal of Sound and Vibration*. 292(1-2), 279-299.
- Choi, H., Jeon, W. P. and Kim, J. (2008). Control of Flow over a Bluff Body. *Annual Review of Fluid Mechanics*. 40, 113-139.
- Cunfl, L. C., Biolley, F., Fontainel, E., Etienne, S. and Facchinetti, M. L. (2002). Vortex-Induced Vibrations of Risers: Theoretical, Numerical and Experimental Investigation. *Journal of Oil and Gas Science and Technology – Rev. IFP*. 57 (1), 59-69.
- Currie, I. G. (1993). *Fundamental Mechanics of Fluids*. New York: McGraw-Hill.
- Daei-Sorkhabi, A. H. and Zehsaz, M. (2009). Studies of Vortex Induced Vibration on the NACA0015. *International Journal of Mechanics*. 3(3), 39-43.
- Dahl, J. M., Hover, F. S. and Triantafyllou, M. S. (2006). Two-Degree-of-Freedom Vortex-Induced Vibrations using a Force Assisted Apparatus. *Journal of Fluids and Structures*. 22(6-7), 807-818.
- Dalton, C. and Xu, Y. (2001). The Suppression of Lift on a Circular Cylinder due to Vortex Shedding at Moderate Reynolds Numbers. *Journal of Fluids and Structures*. 15, 617–628.
- Farrell, T. E. (2003). *Development of a New Boundary Layer Control Technique for Automotive Wind Tunnel Testing*. Master Thesis, Wichita State University, US.
- Ffowcs Williams, J. E. and Zhao, B. C. (1989). The Active Control of Vortex Shedding. *Journal of Fluids and Structures*. 3(2), 115-122.
- Filippini, G., Nigro, N., Storti, M. and Paz, R. (2006). Vortex-Induced Vibration (VIV) Around a Cylinder at Low Reynolds Numbers: The Lock-In Phenomenon. *Mecánica Computacional*. 25, 851–885.
- Fortaleza, E., Creff, Y., and Le´vine, J., 2008, Active Control of Vertical Risers Undergoing Vortex-induced Vibrations. *Proceedings of the ASME 27th International Conference on Offshore Mechanics and Arctic Engineering*, 15-20 June. Estoril, Portugal, 593-601.
- Franzini, G. R., Fujarra, A. L. C., Meneghini, J. R., Korkischko, I., and Franciss, R. (2009). Experimental Investigation of Vortex-Induced Vibration on Rigid,

- Smooth and Inclined Cylinders. *Journal of Fluids and Structures*. 25(4), 742-750.
- Fujisawa, N., Kawaji, Y. and Ikemoto, K. (2001). Feedback Control of Vortex Shedding from a Circular Cylinder by Rotational Oscillations. *Journal of Fluids and Structures*. 15(1), 23-37.
- Gabbai, R. D. and Benaroya, H. (2005). An Overview of Modelling and Experiments of Vortex-Induced Vibration of Circular Cylinders. *Journal of Sound and Vibration*. 282(3-5), 575-616.
- Gattulli, V. and Ghanem, R. (1999). Adaptive Control of Flow-Induced Oscillations including Vortex Effects. *International Journal of Non-Linear Mechanics*. 34(5), 853-868.
- Goldfarb, M. and Sirithanapipat, T. (1999). The Effect of Actuator Saturation on the Performance of PD-Controlled Servo Systems. *Mechatronics*. 9(5), 497-511.
- Govardhan, R. and Williamson, C. H. K. (2000). Modes of Vortex Formation and Frequency Response of a Freely Vibrating Cylinder. *Journal of Fluid Mechanics*. 420, 85-130.
- Griffin, O. M. and Ramberg, S. E. (1976). Vortex Shedding from a Cylinder Vibrating in line with an Incident Uniform. *Journal of Fluids Mechanics*. 75, 257-271.
- Griffin, O. M., Skop, R. A. and Koopmann, G.H. (1973). The Vortex-Excited Resonant Vibrations of Circular Cylinders. *Journal of Sound and Vibration*. 31(2), 235-249.
- Griffin, O. and Ramberg, S (1982). Some Recent Studies of Vortex Shedding with Applications to Marine Tubulars and Risers. *Journal of Sound and Vibration*. 104(1), 2-13.
- Hassan, M. F., Mailah, M., Junid, R. and Alang, N. A. (2010). Vibration Suppression of a Handheld Tool Using Intelligent Active Force Control. *Proceedings of the World Congress on Engineering*, 30 June-2 July. London, UK.
- Huera-Huarte, F. J. and Bearman, P. W. (2009). Wake Structures and Vortex-Induced Vibrations of a Long Flexible Cylinder—Part 1: Dynamic Response. *Journal of Fluids and Structures*. 25(6), 969-990.
- Hong, S., Choi, Y. R., Park, J. B., Park, Y. K. and Kim, Y. H. (2002). Experimental Study on the Vortex-Induced Vibration of Towed Pipes. *Journal of Sound and Vibration*, 249(4), 649-661.

- Hover, F.S. Tvedt, H. and Triantafyllou, M.S. (2001). Vortex-Induced Vibrations of a Cylinder with Tripping Wires. *Journal of Fluid Mechanics*. 448, 175-195.
- How, B. V. E., Ge, S. S. and Choo, Y. S. (2009). Active Control of Flexible Marine Risers. *Journal of Sound and Vibration*. 320(4-5), 758-776.
- Instruments, N. (2008). High-Speed M-Series Multifunction Data Acquisition, NI PCIe-6259 Austin, Texas, USA.
- Ismail, R., Mat Darus, I. Z. and Ismail, A. Y. (2006). Identification Algorithms of Flexible Structure using Neural Networks. In *Proceedings of 2006 4th Student Conference on Research and Development*, 27-28 June. Selangor, Malaysia, 162-168.
- Jalil, N. A. and Mat Darus, I. Z. (2013). System Identification of Flexible Beam Structure using Artificial Neural Network. *Proceedings of the fifth 2013 IEEE International Conference on Computational Intelligence, Modelling and Simulation*. 24 – 25 September. Seoul, Korea, 3 – 7.
- Jauvtis, N. and Williamson, C. H. K. (2003). Vortex-Induced Vibration of a Cylinder with Two Degrees of Freedom. *Journal of Fluids and Structures*. 17(7), 1035-1042.
- Jeon, D. and Gharib, M. (2001). On Circular Cylinders undergoing Two-Degree-of-Freedom Forced Motions. *Journal of Fluids and Structures*. 15(3-4), 533-541.
- Khalak, A. and Williamson, C. (1996). Dynamics of a Hydroelastic Cylinder with Very Low Mass and Damping. *Journal of Fluids and Structures*. 10(5), 455-472.
- Khalak, A. and Williamson, C.H.K. (1997). Investigation of Relative Effects of Mass and Damping in Vortex-Induced Vibration of a Circular Cylinder. *Journal of Wind Engineering and Industrial Aerodynamics*. 69-71, 341-350.
- Khalak, A. and Williamson, C. H. (1999). Motions, Forces and Mode Transitions in Vortex-Induced Vibrations at Low Mass-Damping. *Journal of Fluids and Structures*. 13(7-8), 813-851.
- Kiu, K. Y., Stappenbelt, B. and Thiagarajan, K. P. (2011). Effects of Uniform Surface Roughness on Vortex-Induced Vibration of Towed Vertical Cylinders. *Journal of Sound and Vibration*. 330(20), 4753-4763.
- Koma, A. Y., Zimcik, D. and Mander, A. (2004). Experimental and Theoretical System Identification of Flexible Structures with Piezoelectric Actuators.

- Proceedings of the 2004 International Congress of the Aeronautical Sciences.*
29 August – 3 September. Yokohama, Japan, 1-8.
- Korkischko, I. and Meneghini, J. R. (2012). Suppression of Vortex-Induced Vibration using Moving Surface Boundary-Layer Control. *Journal of Fluids and Structures.* 34, 259–270.
- Koulocheris, D., Dertimanis, V. and Vrazopoulos, H. (2004). Evolutionary Parametric Identification of Dynamic Systems. *Forschung im Ingenieurwesen.* 68, 173-181.
- Kumar, R. A., Sohn, C. H. and Gowda, B. H. L. (2008). Passive Control of Vortex-Induced Vibrations: An Overview. *Recent Patents on Mechanical Engineering.* 1(1), 1-11.
- Kuo, C. H., Chiou, L. C. and Chen, C. C. (2007). Wake Flow Pattern Modified by Small Control Cylinders at Low Reynolds Number. *Journal of Fluids and Structures.* 23(6), 938-956.
- Kuo, C. H. and Chen, C. C. (2009). Passive Control of Wake Flow by Two Small Control Cylinders at Reynolds Number 80. *Journal of Fluids and Structures.* 25(6), 1021-1028.
- Landl, R. (1975). A Mathematical Model for Vortex-Excited Vibrations of Bluff Bodies. *Journal of Sound and Vibration.* 42(2), 219-234.
- Lee, S.J., Lee, S.I. and Park, C.W. (2004). Reducing the Drag on a Circular Cylinder by Upstream Installation of a Small Control Rod. *Fluid Dynamics Research.* 34, 233-250.
- Lienhard, J.H., (1966). Synopsis of Lift, Drag, and Vortex Frequency Data for Rigid Circular Cylinders. Bulletin 300, Washington State University.
- Lin, Y. H. and Chu, C. L. (1994). Comments on Active Modal Control of Vortex Induced Vibrations of a Flexible Cylinder. *Journal of Sound and Vibration.* 175(1), 135-137.
- Ljung, L. (1987). *System Identification: Theory for the User*, Upper Saddle River, N.J.: Prentice Hall PTR.
- Ljung, L. (2010). Perspectives on System Identification. *Annual Reviews in Control.* 34, 1 – 12.
- Mann, G. K. I., Hu, B. G. and Gosine, R. G. (1999) Analysis of Direct Action Fuzzy PID Controller Structures. *Proceedings of Systems, Man, and Cybernetics, Part B: Cybernetics.* June. 29(3), 371-388.

- Mat Darus, I. Z. and Al-Khafaji, A. A. M. (2012). Nonparametric Modelling of a Rectangular Flexible Plate Structure, *International Journal of Engineering Application of Artificial Intelligence*, 25, 94-106.
- Mat Darus, I. Z. and Tokhi, M. O. (2004). Finite Difference Simulation of a Flexible Plate Structure. *Journal of Low Frequency Noise, Vibration and Active Control*. 23(1), 27-46.
- Mat Darus, I. Z. and Tokhi, M.O. (2004). Parametric Modeling of a Flexible 2D Structure. *Journal of Low Frequency Noise, Vibration and Active Control*. 23(2), 115 – 131.
- Mat Darus, I. Z. and Tokhi, M. O. (2006). Parametric and Non-Parametric Identification of a Two Dimensional Flexible Structure. *Journal of Low Frequency Noise, Vibration and Active Control*. 25, 119-143.
- Marcollo, H. (2002). *Multimodal Vortex-Induced Vibration*. PhD Thesis, Monash University, Australia.
- Martins, C. A., Costa, A. B., Harada, C. A. N. and Silva, R. M. C. (1999). Parametric Analysis of Steel Catenary Riser: Fatigue Behavior near the Touchdown Point. *Proceedings of the 9th International Offshore and Polar Engineering Conference*. 30 May – 4 June. Brest, France, 314-319.
- Matsumoto, M. (2002). Vortex Shedding of Bluff Bodies: A Review. *Journal of Fluids and Structures*. 13(7-8), 791-811.
- Mittal, S. (2001). Control of Flow Past Bluff Bodies using Rotating Control Cylinders. *Journal of Fluids and Structures*. 15(2), 291-326.
- Mittal, S. (2003). Flow Control Using Rotating Cylinders: Effect of Gap. *Journal of Applied Mechanics*. 70(5), 762–770.
- Mittal, S. and Kumar, B. (2003). Flow Past a Rotating Cylinder. *Journal of Fluid Mechanics*. 476, 303–334.
- Modi, V. J., Mokhtarian, F., Fernando, M. S. U. K. and Yokomizo T. (1991a). Moving Surface Boundary-Layer Control as Applied to Two-Dimensional Airfoils. *Journal of Aircraft*. 28(2), 104-112.
- Modi, V. J., Fernando, M. S. U. K. and Yokomizo, T. (1991b). Moving Surface Boundary-Layer Control - Studies with Bluff Bodies and Application. *Journal of American Institute of Aeronautics and Astronautics*. 29(9), 1400-1406.
- Modi, V. J., Shih, E., Ying, B. and Yokomizo, T. (1992). Drag Reduction of Bluff Bodies through Momentum Injection. *Journal of Aircraft*. 29(3), 429-436.

- Modi, V. J. (1997). Moving Surface Boundary-Layer Control: A Review. *Journal of Fluids and Structures*. 11(6), 627-663.
- Modi, V. J., Munshi, S. R., Bandyopadhyay, G. and Yokomizo T. (1998). High-Performance Airfoil with Moving Surface Boundary-Layer Control. *Journal of Aircraft*. 35(4), 544-553.
- Mohd. Hashim, S. Z., Tokhi, M. O. and Mat Darus, I. Z. (2004). Nonlinear Dynamic Modelling of Flexible Beam Structures using Neural Networks. *Proceedings of the 2004 IEEE International Conference on Mechatronic*. 3 – 5 June. Istanbul, Turkey, 171 – 175.
- Mohd Yatim, H., Mat Darus, I. Z. and Mohamad, M. (2012). Parametric Identification and Dynamic Characterisation of Flexible Manipulator System. *Proceedings of the 2012 IEEE International Conference on Control, Systems and Industrial Informatics*. 23 – 26 September. Bandung, Indonesia, 16 – 21.
- Moore, K. L. (1993). *Iterative Learning Control for Deterministic Systems in Advances Industrial Control*, New York: Springer-Verlag.
- Moreton, P. (2000). *Industrial Brushless Servomotors*. Oxford: Boston.
- Muddada, S. and Patnaik, B. S. V. (2010). An Active Flow Control Strategy for the Suppression of Vortex Structures behind a Circular Cylinder. *European Journal of Mechanics - B/Fluids*. 29(2), 93-104.
- Mukundan, H., Modarres-Sadeghi, Y., Dahl, J. M., Hover, F. S. and Triantafyllou, M. S. (2009). Monitoring VIV Fatigue Damage on Marine Risers. *Journal of Fluids and Structures*. 25(4), 617-628.
- Munson, B. R., Young, D. F. and Okiishi, T. H. (2006). *Fundamentals of Fluid Mechanics*. (5th ed.) John Wiley and Son (Asia).
- Norberg, C. (2001). Flow Around a Circular Cylinder: Aspects of Fluctuating Lift. *Journal of Fluids and Structures*. 15(3-4), 459–469.
- Piezotronics, PCB. (2013). Model 333B30, New York, USA.
- Pivnoka, P. (2002). Comparative Analysis of Fuzzy PI/PD/PID Controller based on Classical Control Approach. *Proceedings of the 2002 IEEE International Conference on Computational Intelligence*. 12-17 May. Honolulu, HI, 541-546.
- Pop, I. and Watanabe, T. (1992). The Effects of Suction or Injection in Boundary Layer Flow and Heat Transfer on a Continuous Moving Surface. *Techn. Mechanik*. 13, 49-54.

- Pump, HCP. (2011). Series L-63, Taipei, Taiwan.
- Saad, S.M., Jamaluddin, H., and Mat Darus, I. M. (2013). Active Vibration Control of a Flexible Beam Using System Identification and Controller Tuning by Evolutionary Algorithm. *Journal of Vibration and Control*. 0(0), 1-16.
- Saad, S. M. (2014). *Evolutionary Optimisation and Real-Time Self-Tuning Active Vibration Control of a Flexible Beam System*. Doctor Philosophy, Universiti Teknologi Malaysia, Malaysia.
- Sakamoto, H. and Haniu, H. (1994). Optimum Suppression of Fluid Forces acting on a Circular Cylinder. *Journal of Fluids Engineering*. 116, 221-227.
- Sanchis, A., Sælevik, G. and Grue, J. (2008). Two-Degree-of-Freedom Vortex-Induced Vibrations of a Spring-Mounted Rigid Cylinder with Low Mass Ratio. *Journal of Fluids and Structures*. 24(6), 907-919.
- Sarpkaya, T. (1978). Fluid Forces on Oscillating Cylinders. *ASCE Journal of Waterway, Port, Coastal and Ocean Division*. 104, 275-290.
- Sarpkaya, T. (1979). Vortex-Induced Oscillations. *Journal of Applied Mechanics*. 46, 241-258.
- Sarpkaya, T. (1995). Hydrodynamic Damping, Flow-Induced Oscillations, and Biharmonic Response. *Journal of Offshore Mechanics and Arctic Engineering*. 117(4), 232-238.
- Sarpkaya, T. (2004). A Critical Review of the Intrinsic Nature of Vortex Induced Vibrations. *Journal of Fluids and Structures*. 19(4), 389-447.
- Sears, W. R., and Telionis, D. P. (1975). Boundary-Layer Separation in Unsteady Flow. *SIAM Journal on Applied Mathematics*. 28(1), 215-235.
- Shaharuddin, N. M. R. and Mat Darus, I. Z. (2013). System Identification of Flexibly Mounted Cylindrical Pipe due to Vortex Induced Vibration. *Proceedings of the 2013 IEEE International Conference on Computer and Informatics*. 7 – 9 April. Langkawi, Malaysia, 30 – 34.
- Singh, S. N., Rai, L., Puri, P. and Bhatnagar, A. (2005). Effect of Moving Surface on the Aerodynamic Drag of Road Vehicles. *Proceedings of the Institution of Mechanical Engineers, Part D: Journal of Automobile Engineering*. 219, 127-134.
- Sirca Jr, G. F. and Adeli, H. (2012). System Identification in Structural Engineering. *Scientia Iranica Transactions A: Civil Engineering*. 19(6), 1355 – 1364.

- Sparks, C. P. (2007). *Fundamentals of Marine Riser Mechanics: Basic Principles and Simplified Analysis*, Oklahoma: PennWell Corporation.
- Spearritt, D. J. and Ashokanathan, S. F. (1996). Torsional Vibration Control of a Flexible using Laminated PVDF Actuators. *Journal of Sound and Vibration*. 193(5), 941-956.
- Stappenbelt, B., Lalji, F. and Tan, G. (2007). Low Mass Ratio Vortex-Induced Motion. *Proceedings of the 16th Australasian Fluid Mechanics Conference*. 3-7 December. Gold Coast, Queensland, Australia, 1491-1497.
- Stokey, W. (2002). Vibration of Systems Having Distributed Mass and Elasticity. *Shock and Vibration Handbook*. New York: McGraw-Hill. 1-50.
- Storn, R. and Price, K. (1995). *Differential Evolution – A Simple and Efficient Adaptive Scheme for Global Optimization over Continuous Spaces*. Technical Report TR-95-012. International Computer Science Institute.
- Storn, R. (1996). On the Usage of Differential Evolution for Function Optimization. *Proceedings of the Fuzzy Information Processing Society*. 19-22 June. Berkeley, CA, 519-523.
- Strykowski, P. J. and Sreenivasan, K. R. (1990). On the Formation and Suppression of Vortex Shedding at low Reynolds Numbers. *Journal of Fluid Mechanics*. 218, 71-107.
- Sumer, B. M. and Fredsoe, J. (1997). *Hydrodynamics around Cylindrical Structures*. London: World Scientific Publishing Co. Pte. Ltd.
- Tani, J., Qiu, J. and Liu, Y. (1999). Robust Control of Vortex-Induced Vibration of a Rigid Cylinder Supported by an Elastic Beam using μ -Synthesis. *Journal of Fluids and Structures*. 13(7-8), 865-875.
- Tavakolpour, A. R., Mat Darus, I. Z., Tokhi, O. and Mailah, M. (2010). Genetic Algorithm-Based Identification of Transfer Function Parameters for a Rectangular Flexible Plate System. *Engineering Applications of Artificial Intelligence*. 23(8), 1388 – 1397.
- Technologies, C. (2013). MD10C Enhanced 10AMP DC Motor Driver, Johor Bahru, Malaysia.
- Trim, A. D., Braaten, H., Lie, H. and Tognarelli, M. A. (2005). Experimental Investigation of Vortex-Induced Vibration of Long Marine Risers. *Journal of Fluids and Structures*. 21(3), 335-361.

- Unbehauen, H. and Rao, G. P. (1998). A Review of Identification in Continuous-Time Systems. *Annual Reviews in Control*. 22, 145 – 171.
- Vandiver, J.K. (1993). Dimensionless Parameters Important to the Prediction of Vortex-Induced Vibration of Long, Flexible Cylinders in Ocean Currents. *Journal of Fluids and Structures*. 7(5), 423–455.
- Venkatraman, K. and Narayanan, S. (1993). Active Control of Flow-Induced Vibration. *Journal of Sound and Vibration*. 162(1), 43-55.
- Vernier (2012). Flow Rate Sensor. Beaverton, USA.
- Wang, X. K., Su, B. Y. and Tan, S. K. (2012). Experimental Study of Vortex-Induced Vibrations of a Tethered Cylinder. *Journal of Fluids and Structures*. 34, 51-67.
- Wellstead, P. E. and Zarrop, M. B. (1991). *Self-Tuning Systems: Control and Signal Processing*. New York, NY, USA: John Wiley & Sons, Inc.
- Williamson, C. H. K. (1989). Oblique and Parallel Modes of Vortex Shedding in the Wake of a Circular Cylinder at Low Reynolds Number. *Journal of Fluid Mechanics*. 206, 579-627.
- Williamson, C. H. K. and Govardhan, R. (2004). Vortex-Induced Vibrations. *Annual Review of Fluid Mechanics*. 36, 413-455.
- Wu, H., Sun, D. P., Lu, L., Teng, B., Tang, G. Q. and Song, J. N. (2012). Experimental Investigation on the Suppression of Vortex-Induced Vibration of Long Flexible Riser by Multiple Control Rods. *Journal of Fluids and Structures*. 30, 115–132.
- Xu, J., He, M., and Bose, N. (2009). Vortex Modes and Vortex-Induced Vibration of a long Flexible Riser. *Journal of Ocean Engineering*. 36(6-7), 456-467.
- Yang, J., Lei, F. and Huang, Y. (2010). Dynamic Characteristics Analysis of Underwater Flexible Structures. *Proceedings of the 2010 ICCIS International Conference on Computational and Information Sciences*. 17-19 December. Chengdu, 1122-1125.
- Yang, Y. (2010). *Experimental Investigations of Vortex Induced Vibration of a Flat Plate in Pitch Oscillation*. Master Thesis, Texas A&M University, US.
- Yen, K. M., Magee, A., Aramanadka, S. B., Abdul Malik, A. M., Abdul Ghani, M. P., Ismail, N., Ahmad Zukni, N. and Teng, Y. J. (2013) Riser VIV Suppression Device Tests for Application to a Southeast Asia TLP. *In: Proceedings of the 32nd ASME*

2013 International Conference on Ocean, offshore and Arctic Engineering. 9-14 June. Nantes, France, 1-12.

- Zdravkovich, M.M. (1981). Review and Classification of Various Aerodynamic and Hydrodynamic Means for Suppressing Vortex Shedding. *Journal of Wind Engineering and Industrial Aerodynamics.* 7(2), 145-189.
- Zhou, T., Razali S. F. M., Hao, Z. and Cheng, L. (2011). On The Study of Vortex-Induced Vibration of a Cylinder with Helical Strakes. *Journal of Fluids and Structures.* 27(7), 903-917.
- Zhang, M. M., Cheng, L. and Zhou, Y. (2004). Closed-Loop Control of Fluid-Structure Interactions on a Flexibly Supported Cylinder. *European Journal of Mechanics - B/Fluids.* 23(1), 189-197.
- Ziegler, J. G. and Nichols, N. B.(1942). Optimum Settings for Automatic Controllers. *Trans. ASME.* 64(8), 759-768.