

DESIGN OF MULTI-PORT NETWORK UTILIZING MICROSTRIP-SLOT  
TECHNIQUE FOR ULTRA WIDEBAND SYSTEM

KHAIRUL HUDA BINTI YUSOF

A thesis submitted in fulfilment of the  
requirements for the award of the degree of  
Doctor of Philosophy (Electrical Engineering)

Faculty of Electrical Engineering  
Universiti Teknologi Malaysia

JANUARY 2016

*Special dedicated and thankful, expecially to my beloved parents, Yusof Bin Suboh and Faridah Bin Sulaiman, my inspirational supervisor, Dr Norhudah Seman and also not forget to my brothers, sisters, friends, lecturers & WCC staffs for their endless support, encouragement and motivation throughout my doctoral study. A warm thanks to all*

## ACKNOWLEDGEMENT

First and foremost, grateful to the Allah SWT, with His permittance I succeed to complete this project eventually. Unforgotten, this dedication is also credited to my supervisor, Dr. Norhudah Binti Seman. She spent countless hours in advising my works. She is an extraordinary person, which her energy and excitement in research never seem to end. This work would not be possibly successful without her invaluable advices and guidance.

I would like to express my special thanks to my Co-Supervisor, Dr. Mohd Haizal Bin Jamaluddin for his guiding, patience and helpful discussions in this work, contributing me with ingenious ideas during discussion and providing information also advices to complete the thesis.

My deepest gratitude goes to my family especially to the most important people who always given their loves, support and encouragement, mother and father (Faridah Sulaiman and Yusof Suboh), to my sisters Khairul Fazariah, Khairul Rodhiah, and Khairul Aimi and to my brothers Khairil Amri, Khairil Hilmi and Khairil Annas and also, not forget to my brother and sister in-laws, Sarkawi, Zahidi and Siti Norbayu. Their endless love is the priceless treasure to give me light to overcome the darkest time.

Last but not least, I want to express my great appreciation to all my friends especially Nur Syazwani, Aliya Syaza, Nur Amirah, Nur Safura, Nur Affifah Omar, Nur Hidayu, and Nur Ayuni, for their support and help directly or indirectly. Thanks for supporting me extremely all the time.

## ABSTRACT

Nowadays, there is a lot of interest on the research and development related to ultrawideband system due to the increasing demands on the applications with low power, low cost and low interference. Thus, to cope with these demands, various researches are required for the development of front-end microwave components, which include six-port network as an alternative to a mixer-based design. The configuration of a six-port network is constructed by combining coupler and power divider. In the interest to have a simple design and convenient usage to form the six-port network with ultra wideband (UWB) operation, new power divider and coupler are designed by using microstrip-slot technique. All the proposed designs are simulated via the use of CST Microwave Studio 2010 and realized using Rogers TMM4 with a conductor coating of 35  $\mu\text{m}$ , thickness of 0.508 mm and dielectric constant of 4.5. The developed prototypes of the proposed designs are verified by measurement using a vector network analyser (VNA). In this thesis, a design of two-section power divider is proposed with a great UWB performance of  $-3.8 \text{ dB} \pm 0.5 \text{ dB}$  transmission coefficient and  $0^\circ \pm 2^\circ$  phase difference. This power divider has bandwidth improvement of 11.9% and size reduction of 23.33% compared to the conventional design. Meanwhile, for the coupler design, a UWB coupled-line coupler with zig-zag-shaped slot that has  $3 \text{ dB} \pm 2 \text{ dB}$  coupling coefficient and  $-90^\circ \pm 5^\circ$  phase difference is proposed. The proposed coupler has 109.5% bandwidth improvement with the length reduction of 20% compared to the conventional coupler. The proposed UWB coupler is then implemented into a new proposed structure of UWB  $90^\circ$  power divider. Then, three configurations of six-port networks formed by UWB coupler, two-section power divider and  $90^\circ$  power divider are designed; which are named as Type I, Type II and Type III. From the observation, Type III demonstrates the best UWB performance with magnitude imbalance of  $\pm 5 \text{ dB}$  and phase imbalance of  $\pm 10^\circ$  that achieving the specified UWB design goal. Furthermore, Type III has the respective size reduction of 57.16% and 34.67% compared to Type I and II. In addition, by comparing to the previous works, the proposed design has broadest bandwidth of 100% and smallest size of 50.92 mm x 35 mm. Hence, the proposed six-port network has very well UWB performance with relatively compact size and simple design, which is easy to be fabricated.

## ABSTRAK

Pada masa kini, terdapat banyak permintaan ke atas penyelidikan dan pembangunan yang berkaitan dengan sistem jalur lebar ultra (UWB) yang disebabkan oleh permintaan yang semakin meningkat terhadap aplikasi berkuasa rendah, kos yang rendah dan gangguan yang rendah. Oleh itu, untuk memenuhi permintaan ini, pelbagai penyelidikan diperlukan pada komponen gelombang mikro bahagian-depan, termasuk rangkaian enam-pangkalan sebagai alternative kepada reka bentuk berasaskan pencampur. Konfigurasi rangkaian enam-pangkalan dibina dengan menggabungkan pengganding dan pembahagi kuasa. Untuk memperolehi reka bentuk yang ringkas dan penggunaan yang mudah bagi membentuk rangkaian enam-pangkalan dengan operasi jalur lebar ultra (UWB), reka bentuk pembahagi kuasa dan pengganding yang baru telah direka dengan menggunakan teknik mikrojalur-alur. Kesemua reka bentuk yang dicadangkan disimulasi dengan menggunakan CST Microwave Studio 2010 dan dilaksanakan dengan menggunakan substratum Rogers TMM4 dengan  $35\text{ }\mu\text{m}$  salutan konduktor, 0.508 mm tebal dan 4.5 pemalar dielektrik. Prototaip reka bentuk yang dicadangkan ditentusahkan dengan menggunakan Penganalisis Rangkaian Vektor (VNA). Di dalam tesis ini, reka bentuk pembahagi kuasa dua-bahagian yang dicadangkan mempunyai prestasi UWB terbaik dengan pekali penghantaran  $-3.8\text{ dB} \pm 0.5\text{ dB}$  dan beza fasa  $0^\circ \pm 2^\circ$ . Pembahagi kuasa ini mempunyai 11.9% peningkatan jalur lebar dan 23.33% pengurangan saiz berbanding reka bentuk lazim. Manakala, bagi reka bentuk pengganding, pengganding UWB dengan menggunakan slot berbentuk zig-zag mempunyai  $-3\text{ dB} \pm 2\text{ dB}$  pemalar gandingan dan  $-90^\circ \pm 5^\circ$  beza fasa telah direka. Reka bentuk pengganding yang dicadangkan mempunyai 109.5% peningkatan jalur lebar dengan pengurangan panjang sebanyak 20% berbanding dengan reka bentuk lazim. Pengganding yang dicadangkan dilaksanakan ke dalam struktur baru pembahagi kuasa  $90^\circ$  UWB. Kemudian, tiga konfigurasi rangkaian enam-pangkalan direka daripada UWB pengganding, pembahagi kuasa dua-bahagian dan pembahagi kuasa  $90^\circ$ , dinamakan sebagai Jenis I, Jenis II dan Jenis III. Daripada pemerhatian, Jenis III menunjukkan prestasi UWB terbaik dengan ketidakseimbangan magnitud  $\pm 5\text{ dB}$  dan ketidakseimbangan fasa  $\pm 10^\circ$  yang mencapai matlamat reka bentuk UWB yang ditentukan. Tambahan pula, Jenis III mempunyai 57.16% dan 34.67% pengurangan saiz berbanding Jenis I dan II. Di samping itu, dengan membandingkan reka bentuk yang sebelumnya, reka bentuk yang dicadangkan mempunyai lebar jalur yang paling luas sebanyak 100% dan saiz terkecil dengan 50.92 mm x 35 mm. Oleh itu, rangkaian enam-pangkalan yang dicadangkan mempunyai prestasi jalur lebar ultra yang sangat baik dengan saiz yang padat dan reka bentuk yang mudah untuk difabrikasi.

## TABLE OF CONTENTS

<b>CHAPTER</b>	<b>TITLE</b>	<b>PAGE</b>
	<b>DECLARATION</b>	ii
	<b>DEDICATION</b>	iii
	<b>ACKNOWLEDGEMENT</b>	iv
	<b>ABSTRACT</b>	v
	<b>ABSTRAK</b>	vi
	<b>TABLE OF CONTENTS</b>	vii
	<b>LIST OF TABLES</b>	xii
	<b>LIST OF FIGURES</b>	xv
	<b>LIST OF ABBREVIATION</b>	xxiv
	<b>LIST OF SYMBOLS</b>	xxv
	<b>LIST OF APPENDICES</b>	xxvii
<b>1</b>	<b>INTRODUCTION</b>	<b>1</b>
	1.1 Research Background	1
	1.2 Problem Statement	3
	1.3 Objectives of the Research	6
	1.4 Scope of the Research	6
	1.5 Contributions of the Research	7
	1.6 Thesis Outline	9
<b>2</b>	<b>THE REVIEW ON THE MICROWAVE COMPONENTS AND SIX-PORT NETWORK</b>	<b>11</b>
	2.1 Introduction	11
	2.2 The basic concept of microstrip and slotline	11

	2.2.1 Microstrip-line	12
	2.2.2 Slotline	15
	2.3 H-Hybrid	17
	2.3.1 Basic Concept	17
	2.3.2 Review on the Previous work of H-Hybrid	18
	2.4 Power Divider	22
	2.4.1 Basic Concept	23
	2.4.2 Review on Power Divider design	24
	2.5 Quadrature Coupler	39
	2.5.1 Basic Concept of Quadrature Coupler	39
	2.5.2 Review on the previous works of quadrature coupler	40
	2.6 Six-port Network	54
	2.6.1 Basic Concept	54
	2.6.2 Review on Previous Works of Six-port Network	57
	2.7 Summary	66
<b>3</b>	<b>RESEARCH METHODOLOGY</b>	<b>68</b>
	3.1 Introduction	68
	3.2 The specification of designed component	68
	3.3 Research Methodology and Flow Chart of the Research	71
	3.4 The Choice of Substrates	80
	3.5 Summary	82
<b>4</b>	<b>DESIGN AND ANALYSIS OF POWER DIVIDER</b>	<b>84</b>
	4.1 Introduction	84
	4.2 Characterization and Formulation of Microstrip-Slot Impedance	85
	4.3 Design of Power Divider	89

4.3.1	T-Shaped Power Divider without Radial Stub	90
4.3.2	T-Shaped Power Divider with Radial Stub by using Two Different Substrates and Cooper Thicknesses	97
4.3.3	U-Shaped Power Divider	105
4.3.4	Two-Section Ultra Wideband Power Divider	115
4.3.5	Comparison of the Designed Power Dividers	125
4.4	Summary	127

<b>5</b>	<b>DESIGN AND ANALYSIS OF QUADRATURE COUPLER</b>	<b>130</b>
5.1	Introduction	130
5.2	3 and 6 dB Coupled-Line Coupler with Different Grounding Techniques	131
5.2.1	Basic Coupled-Line Coupler	131
5.2.2	Coupled-Line Coupler with Slotted Ground- Plane	134
5.2.3	Coupled-Line Coupler with Floating Ground Plane Conductor	138
5.2.4	Performance Comparison of three Coupled- Line Coupler Designs	141
5.3	3-dB Coupler with Circular-Shaped Floating-potential Ground Plane	143
5.4	3-dB Coupler with Zig-zag-Shaped Slot	147
5.4.1	Analysis of the Proposed 3-dB Coupler with Zig-zag-Shaped Slot	151
5.4.2	The Performance of Proposed 3-dB Coupler- Line Coupler with Zig-zag-Shaped Slot	155
5.4.3	90 <sup>0</sup> Power Divider with Zig-zag-Shaped Slot	158
5.5	Comparison performance of the designed 3 dB coupled-line coupler	160

5.6	Summary	162
<b>6</b>	<b>DESIGN AND ANALYSIS OF SIX-PORT NETWORK</b>	<b>164</b>
6.1	Introduction	164
6.2	Ultra Wideband Six-port Network Type I	164
6.3	Ultra Wideband Six-port Network Type II	171
6.4	Ultra Wideband Six-port Network Type III	177
6.5	Summary of the Proposed Six-port Network	183
<b>7</b>	<b>CONCLUSION AND FUTURE WORKS</b>	<b>187</b>
7.1	Introduction	187
7.2	Conclusion	187
7.3	Future Works	190
	<b>REFERENCES</b>	<b>191</b>
	Appendices A-B	202-216

## LIST OF TABLES

<b>TABLE NO.</b>	<b>TITLE</b>	<b>PAGE</b>
2.1	The summary of UWB H-hybrid design	22
2.2	The summary of selected wideband power dividers	37
2.3	The summarized previous works of coupler	53
2.4	The open and short termination for six-port network for QPSK modulation	57
2.5	The summarized wideband six-port network	65
3.1	The parameters and specifications of proposed components	69
3.2	Five substrates and the properties	81
4.1	The used substrates in the study with different thickness and relative permittivity	87
4.2	The performance comparison between conventional and proposed design	96
4.3	Specification of investigation substrates	98
4.4	The step impedance, $Z_i$ of power divider depending on the substrate and thickness of copper (t)	100
4.5	The slot impedance, $Z_s$ of power divider depending on the substrate and thickness of copper (t)	100
4.6	The dimension (in mm) of power divider depending on the substrate and thickness of copper (t)	101
4.7	The performance comparison between two substrates, RO4003C and TMM4 with 35 $\mu\text{m}$ copper thickness	104

4.8	Comparison the performance of measurement result of the U-shaped power divider across 4 to 10.6 GHz	113
4.9	The performance comparison between U-shaped power divider and conventional power divider	114
4.10	Analysis of the effective length of the microstrip-slot quarter-wave section 1 and 2 that correspond to the electrical length	119
4.11	The comparison of the simulation and measurement results of the proposed two-section power divider	123
4.12	The performance comparison between proposed and conventional two-section power divider	124
4.13	The comparison performance of the designed Power Divider	126
5.1	The parameters and optimized dimensions of 3 and 6 dB basic coupled-line couplers at centre frequency of 6.85 GHz	132
5.2	The parameter and optimized dimension of 3 and 6 dB coupled-line coupler with slotted ground-plane at centre frequency of 6.85 GHz	136
5.3	The parameters and optimized dimension of 3 and 6 dB coupled-line coupler with floating-potential ground-plane at centre frequency of 6.85 GHz	139
5.4	The performance of 3 dB coupled-line couplers with different grounding techniques	141
5.5	The performance of 6 dB coupled-line couplers with different grounding techniques	142
5.6	The parameters and optimized dimension of coupled-line coupler with two circle slotted ground plane at centre frequency of 6.85 GHz	145
5.7	The performance comparison of the designed coupler with conventional coupled-line coupler	157

5.8	The performance comparison of the 3 dB coupler with circular-shaped floating-potential ground plane with 3 dB Coupler with zig-zag-shaped slot	161
6.1	The performance of UWB six-port networks	183
6.2	The comparison of proposed UWB six-port network of Types III to the previous six-port	185

## LIST OF FIGURES

FIGURE NO.	TITLE	PAGE
1.1	Block diagram of (a) conventional transceiver with mixer-based approach, and (b) transmitter and (c) receiver of six-port transceiver	3
2.1	The configuration of microstrip-line	12
2.2	The (a) configuration of slotline and (b) field distribution of slotline	15
2.3	Photos of (a) the microstrip rat race coupler, (b) the stepped-impedance rat race coupler with the broadside-coupled structure	19
2.4	Hybrid ring coupler	20
2.5	Photograph of a microstrip H-hybrid	21
2.6	The configuration of 180° hybrid	21
2.7	Configuration of Wilkinson power divider	24
2.8	Power divider implementing through ground via (TGV) technique	25
2.9	The designed power divider	26
2.10	Design of power divider using stub technique	26
2.11	Two-way Wilkinson power dividers using coupled line	27
2.12	The design of planar three-way power divider	27
2.13	Photograph of the 10:1 Wilkinson power divider, which is fabricated on RO4003 substrate	28
2.14	Fabricated NTL-based 1:2 Wilkinson power divider	29
2.15	Physical layout of the tapered-line power divider	29
2.16	The configuration of UWB microstrip power divider	30

2.17	Configuration of in-phase microstrip-slot power divider	31
2.18	Novel power combiner with coax balun transformer	32
2.19	Photograph of the designed power divider	32
2.20	Layout of the developed broadband quasi-lumped 3-dB coupled-line Wilkinson power divider. Top layer – blue color, bottom layer – pink color	33
2.21	Configuration of fabricated power divider	33
2.22	Photograph of the 1:3 unequal Wilkinson power divider	35
2.23	Photograph of the proposed three-way power divider	35
2.24	Photograph of designed power divider	36
2.25	Photograph of the power divider	36
2.26	The basic operation of quadrature coupler	39
2.27	The top view of the proposed coupler	41
2.28	Configuration of the directional coupler with the bend section of $45^\circ$	42
2.29	Three-cell 3-dB CRLH coupler prototype, which the spacing between the lines is $s = 0.3$ mm	42
2.30	Configuration of the CRLH CPW coupler with two backed conductors beneath the center strips of coupled CPW (dashed line areas)	43
2.31	The configuration of Interdigitated 3-dB Langer coupler	44
2.32	The configuration of coupler design using non-uniform technique	44
2.33	Photograph of a wideband nonuniform branch line coupler	45
2.34	Design of 3-dB coupler with two-section tandem connection	45
2.35	Configuration of separation parts of N-section parallel-coupled lines	46

2.36	A 3 dB coupler composed by two of 8.34 dB with seven sections in tandem for an operating central frequency of 3 GHz	47
2.37	Layout of the investigated UWB 3 dB coupler with a capacitive disk as produced with CST Microwave Studio	48
2.38	The fabricated UWB 3 dB and 180° fractal branch line coupler	49
2.39	Broadband quadrature coupler with slotted ground plane	50
2.40	3-dB Broadband parallel-coupled quadrature coupler with floating-potential ground plane conductor	50
2.41	Photograph of the manufactured three-section 3-dB microstrip-slot coupler	51
2.42	The configuration of the proposed coupler including microstrip ports	52
2.43	Block diagram the operation of six-port network as (a) modulator and (b) demodulator at the respective transmitter and receiver	55
2.44	The configuration of (a) top and (b) bottom layers of dual six-port design	58
2.45	Six-port reflectometer; (a) block diagram and (b) layout	58
2.46	Layout of proposed six-port network	59
2.47	Complete layout of the presented broadband six-port network, operated from 2 to 3.5 GHz; (a) block diagram and (b) layout	60
2.48	Configuration of six-port network proposed	60
2.49	Six-port network physical realization	61
2.50	Configuration of six-port network (a) conventional and (b and c) unconventional	62

2.51	Configuration of six-port junction over 2-8 GHz; (a) block diagram and (b) layout	63
2.52	Fabricated six-port network; (a) block diagram, (b) top and (c) bottom view	64
3.1	The flow chart of the overall research framework	71
3.2	The flow chart of the power divider research framework	74
3.3	The measurement setup of the proposed power divider using a vector network analyzer (VNA)	75
3.4	The flow chart of the coupler research framework	77
3.5	The measurement setup of proposed coupler using a vector network analyzer (VNA)	78
3.6	The flow chart of the six-port network research framework	79
3.7	The measurement setup of proposed six-port networks using a vector network analyzer (VNA)	80
4.1	(a) The cross section and (b) CST layout of microstrip-slotline	85
4.2	The microstrip-slot impedance, $Z_{ms}$ versus the width of slot, $W_s$ for 0.508 mm thickness of substrate	87
4.3	The microstrip-slot impedance, $Z_{ms}$ versus the width of slot, $W_s$ for 0.762 mm thickness of substrate	88
4.4	The microstrip-slot impedance, $Z_{ms}$ versus the width of slot, $W_s$ for 1.524 mm thickness of substrate	88
4.5	(a) The configuration of ground-slotted T-shape power divider by using one substrates technique: (b) top layer of microstrip and (c) bottom layer of slotted ground plane	91
4.6	Dimensions of top view layout of T-junction power divider	93

4.7	The prototype of the fabricated T-shaped power divider: (a) top view, (b) bottom view and (c) perspective view	94
4.8	Measured and simulated $S_{11}$ performance of T-shaped power divider	95
4.9	Measured and simulated $S_{21}$ and $S_{31}$ performance of T-shaped power divider	95
4.10	Simulated and measured performance of $S_{21}$ and $S_{31}$ phase and its phase difference characteristic	96
4.11	(a) The configuration of ground-slotted power divider by using one substrates: (b) Top layer of microstrip and (c) bottom layer of slotted ground plane	98
4.12	The top view of T-shaped power divider and its dimensions	99
4.13	$S_{21}$ and $S_{31}$ performances of the proposed power divider by using different substrates and thickness of copper	102
4.14	$S_{11}$ performance of the proposed power divider by using different substrates and thickness of copper	103
4.15	The performances of $S_{21}$ and $S_{31}$ phase and its phase difference for different substrates and thickness of copper	104
4.16	The overall view of wideband U-shaped power divider by using microstrip-slot technique	106
4.17	(a) Top view of power divider and (b) bottom view of power divider at common ground plane	106
4.18	Equivalent circuit of the proposed wideband U-shaped power divider	107
4.19	Configuration of prototype proposed design of wideband U-shaped power divider with using resistors: (a) top, (b) bottom, and (c) perspective view	109

4.20	Simulated and measured performance of $S_{21}$ for the proposed wideband power divider design with and without using resistor between two output arms	110
4.21	Simulated and measured performance of $S_{31}$ for the proposed wideband power divider design with and without using resistor between two output arms	110
4.22	Simulated and measured performance of $S_{11}$ for the proposed wideband power divider design with and without using resistor between two output arms	111
4.23	Simulated and measured performance of $S_{23}$ of the proposed wideband power divider design with and without using resistor between two output arms	112
4.24	Simulated and measured performance of phase characteristics of the proposed wideband power divider design with and without using resistor between two output arms	112
4.25	The perspective view of the UWB two-section microstrip-slot power divider	115
4.26	The detail configuration of UWB two-section microstrip-slot power divider: (a) top and (b) bottom view	116
4.27	The equivalent circuit of UWB two-section microstrip-slot power divider	116
4.28	The (a) front and (b) back view of the proposed UWB two-section power divider prototype	121
4.29	Simulated and measured performance of the proposed UWB two-section power divider: (a) $S_{21}$ and $S_{31}$ , and (b) $S_{11}$ and $S_{23}$	122
4.30	The simulation and measurement results for phase difference between two output ports of the proposed two-section power divider	123
5.1	The configuration of basic coupled-line coupler	131

5.2	The S-parameters performance of 3 dB and 6 dB basic coupled-line couplers	134
5.3	The phase difference between two output ports of 3 dB and 6 dB basic coupled-line couplers	134
5.4	Configuration of coupled-line coupler with slotted-ground plane: (a) top layer and (b) bottom layer of ground plane	135
5.5	The S-parameters performance of 3 dB and 6 dB coupled-line coupler with slotted ground-plane	137
5.6	The phase difference between two output ports of 3 dB and 6 dB coupled-line coupler with slotted ground-plane	137
5.7	Configuration of coupled-line coupler with floating-potential ground plane: (a) top layer and (b) bottom layer of ground plane	139
5.8	The S-parameters performance of 3 and 6 dB coupled-line coupler with floating-potential ground plane conductor	140
5.9	The phase difference between two output ports of 3 and 6 dB coupled-line coupler with floating-potential ground plane conductor	141
5.10	The configuration of proposed coupler using two slotted-circle floating-potential ground plane; (a) top and (b) bottom view	144
5.11	The S-parameters performance of proposed 3 dB coupler using two floating-potential circle slotted ground-plane	146
5.12	The phase difference between port 2 and 3 of proposed 3 dB coupler using two floating potential circle slotted ground-plane	146

5.13	The (a) top and (b) bottom configuration of proposed coupled-line coupler with zig-zag shaped slot and its fabricated prototype of: (c) top and (d) bottom view	149
5.14	The equivalent network of: (a) even-mode and (b) odd-mode operation at the cross section of the coupled-line coupler with zig-zag slot at ground plane	150
5.15	Coupling factor, $C$ versus slot width, $W_s$ of proposed 3 dB coupled-line coupler at center frequency of 6.85 GHz, with varied gap spacing, $s$	153
5.16	$Z_{0e}$ and $Z_{0o}$ of proposed 3 dB coupled-line coupler at center frequency of 6.85 GHz with varied gap spacing, $s$	155
5.17	The performance of simulated and measured (a) S-parameters and (b) phase characteristic of proposed 3 dB coupled-line coupler with zig-zag-shaped slot	157
5.18	(a) Top and (b) bottom configuration of 90° power divider with zig-zag-shaped slot and its fabricated prototype of: (c) top and (d) bottom view	159
5.19	The performance of simulated and measured (a) S-parameters and (b) phase characteristic of proposed 90° power divider with zig-zag-shaped slot	160
6.1	The block diagram of the proposed six-port network Type I	165
6.2	The configuration of overall proposed six-port network type I (a) top layer and (b) bottom layer	165
6.3	The fabricated of overall proposed UWB six-port network type I (a) top layer and (b) bottom layer	167
6.4	The S-parameter performance of proposed six-port network Type I; (a) transmission coefficients of $S_{i1}$ , (b) transmission coefficients of $S_{i2}$ and (c) reflection coefficients and isolation at Port 1 and Port 2	169

6.5	The phase difference performance of proposed six-port network Type I	170
6.6	The block diagram of proposed UWB six-port network Type II	171
6.7	The overall layout of the proposed six-port network Type II operated at UWB frequency range; (a) top view and (b) bottom view	172
6.8	The fabricated of the proposed UWB six-port network Type II; (a) top view and (b) bottom view	173
6.9	The simulated S-parameter performances of the proposed six-port network Type II; (a) transmission coefficients of $S_{i1}$ (b) transmission coefficients of $S_{i2}$ and (c) reflection coefficients and isolation at Port 1 and Port 2	175
6.10	The phase characteristics of proposed UWB six-port network Type II	176
6.11	The configuration of proposed six-port network Type III formed by two coupler, one power divider and one 90° power divider	177
6.12	The configuration of proposed six-port network Type III; (a) top view and (b) bottom view	178
6.13	The fabricated prototyped of the proposed UWB six-port network Type III; (a) top view and (b) bottom view	179
6.14	S-parameter of proposed six-port network; (a) transmission coefficients of $S_{i1}$ (b) transmission coefficients of $S_{i2}$ and (c) the reflection coefficients and isolation	182
6.15	Phase difference of the proposed six-port network	182

## LIST OF ABBREVIATION

WiFi	-	Wireless Fidelity
DAS	-	Distributed antenna system
MIMO	-	Multiple input multiple output
FCC	-	Federal Communication Commission
UWB	-	Ultra wideband
Q	-	Quadrature coupler
D	-	Divider
CST	-	Computer Simulation Technology
VNA	-	Vector network analyzer
E	-	Electric
H	-	Magnetic
TGV	-	Through ground via
NTL	-	Non-uniform transmission line
MLS	-	Method of least squares
DGS	-	Defect ground-slotted
PMGA	-	Parallel micro-genetic algorithm
VBA	-	Visual Basic for Applications
CRLH	-	Composite right-/left-handed
BCC	-	Broadside-coupled capacitor
MSI	-	Meandering short-circuited stub inductor
IF	-	Intermediate frequency
QPSK	-	Quadrature phase shift keying
QAM	-	Quadrature amplitude modulation
DF	-	Direction finding
PCB	-	Printed circuit board
PTFE	-	Polytetrafluoroethylene

## LIST OF SYMBOLS

$Z_{ms}$	-	Impedance of microstrip-slot
$W_s$	-	Slot of width
$Z_m$	-	Microstrip-impedance
$W_m$	-	Width of conductor
$H$	-	Thickness of substrate
$E_r$	-	Relative permittivity
$\epsilon_e$	-	Effective dielectric constant
$L_m$	-	Length of microstrip line
$k_0$	-	Wave number in free space
$\theta$	-	Electrical length in degree
$f$	-	Cut off frequency
$c$	-	Velocity of light in free-space
$v_p$	-	Phase velocity
$\beta$	-	Propogation constant
$Z_s$	-	Impedance of slot
$\lambda_0$	-	Free-space wavelength
$A_i$ and $B_i$	-	Unknown complex constants
$V_i$	-	Output voltage
$J_o(.)$	-	Zeroth-order Bessel function
$k_0, k_1, k_2, k_{es}$ and $k_{em}$	-	Propagation constants
$\epsilon_{rem}$	-	Microstrip effective dielectric constant
$\epsilon_{res}$	-	Slot effective dielectric constant

$Z_{QT}$	-	Impedance of quarter-wave transmission lines
$C_g$	-	Fringe capacitances
$C_p$	-	Parallel-plate capacitance
$N$	-	The number of section of the quarter-wave transformer
$Z_L$	-	Load impedance
$C_n^N$	-	Binomial coefficients
$\lambda_{m-s}$	-	Microstrip-slot wavelength
$Z_{0e}$ and $Z_{0o}$	-	Even- and odd-mode characteristic impedance
$C$	-	Numerical value of coupling factor
$S$	-	Spacing
$F$	-	Slow wave factor
$C_e$	-	Even-mode capacitance
$C_o$	-	Odd-mode capacitance
$v_p$	-	Phase velocity of the propagation on the line
$S_i$	-	Emerging complex signal

**LIST OF APPENDICES**

<b>APPENDIX</b>	<b>TITLE</b>	<b>PAGE</b>
A	The list of Publication	202
B	Datasheets of Substrates	205

## **CHAPTER 1**

### **INTRODUCTION**

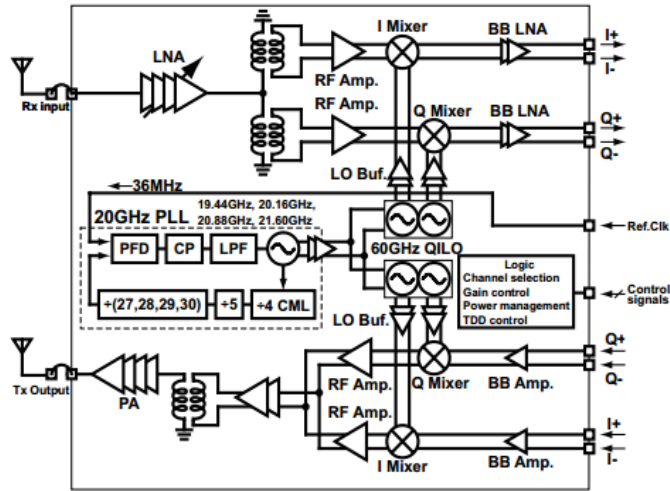
#### **1.1 Research Background**

An unlicensed low power spectrum of ultra wideband (UWB) covering from 3.1 to 10.6 GHz has been specified by Federal Communication Commission (FCC) in 2002 [1] [2]. It has given an high impact to the communication sector due to its benefits and attractive features. FCC in [2] defines ultra wideband (UWB) as a fractional bandwidth that greater than 0.25 or occupies 1.5 GHz or more frequency spectrums. The minimum 1.5 GHz bandwidth is relevant only when the centre frequency is higher than 6 GHz. The Commission has authorized frequency band of 3.1 to 10.6 GHz for radar and wireless communication applications, which the major standards for wireless local area networks (LANs) are specified by IEEE 802.11 family standards and the smaller-scale standards based on ultra-wideband (UWB) communication. Since then, rapid development had been conducted parallel to the technology invented nowadays. Thus, due to that, low power, low cost, and low interference have been the requirements in UWB system. One of the interests is on six-port network.

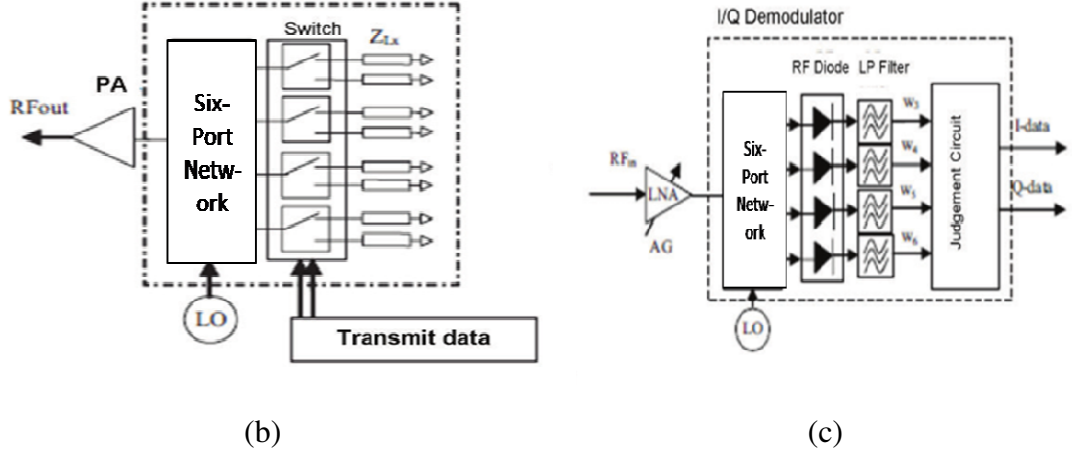
A six-port network, or in more general case also known as, multi-port provides an alternative method to determine the complex voltage ratio of two signals [3] by performing mathematical transformations on power values measured at the output ports. This multi-port network is build from N-port networks, where the N

should be greater than 5, equipped with scalar power detectors at its output ports. Where, the multi-port network is extensively implemented in many applications such as microwave parameter measurements [4], [5], [6], phase detectors in positioning systems [7], [8], [9], modulators and demodulators [10]-[11] in radar system [12]-[13] and wireless communications [14].

In order to support the requirement such in wireless communication system, various thorough research works are needed in component designs including alternative to mixer. Commonly, the design of mixer will involve active device, which needs a certain biasing voltage to be in an active state. In order to reduce the complexity of the design, the mixer-based approach can be replaced by using a six-port network in transceiver system particularly as modulator and demodulator as shown in Figure 1.1 [15]. A six-port, is formed by only using passive devices such as coupler, H-hybrid, and power divider [16]. By including these devices, it can reduce the complexity of the design and increase the performance of bandwidth.



(a)



**Figure 1.1** Block diagram of (a) conventional transceiver with mixer-based approach, and (b) transmitter and (c) receiver of six-port transceiver [15]

Thus, in this thesis, a new design of six-port network by using a single substrate with slots formed in the ground plane, that offers an ultra wideband performance, compact size and better fabrication tolerance is presented. The ultra-wideband operation of 3.1 to 10.6 GHz is chosen as the designated frequency band due to its unlicensed usage [17]. This led to the increment of spectral efficiency and more wireless applications can be introduced and enhanced. Besides, UWB can provide high data rate over a very short range and also UWB system consumes low power transmission and robustness against multipath fading and noise. By using operating frequency of 3.1 to 10.6 GHz (UWB), the proposed six-port can overcome the bandwidth limitation reported in Section 2.6.2 of Chapter 2. Design and the analysis on S-parameter performance of proposed six-port network, which formed by 3-dB coupler and power divider is implemented in CST Microwave Studio.

## 1.2 Problem Statement

Particularly, in transceiver communication system, to be in active state, the design of mixer involves a certain biasing voltage. Consequently, this requirement leads to a more complex design. Thus, to solve the problem, the mixer-based approach can be replaced by using a six-port network. Six-port network is a passive

linear circuit, which can be constructed by the combination of the coupler, power divider and/or H-hybrid. These components must be designed to operate in the UWB frequency range to permit construction of the UWB six-port network. In the interest to have ultra wideband component, there are important issues need to be concerned.

In the previous research, the designs of UWB quadrature coupler (Q) and divider (D) hybrids are accomplished by implementing a few of planar technologies such as multilayer microstrip-slot [18], [19], [20], [21], [22], [23] ground-slot technique [24], [25], [26] combination of step-impedance and parallel coupled-line approach [27], and floating potential method [28]. However, the configuration in [18], [19], [20], [21], [22], [23] which required two substrates, might difficult to be handled during fabrication process due to a very fine fabrication tolerance imposed by the air gap between each layer. The existence of the air gap degrades the actual measured performance and become incomparable to the simulated results. Even though, the best isolation performance is obtained by the design in [26], Bialkowski and Wang argued that this configuration requires a lot of care in aligning its two substrates [24]. This statement also supported by Zheng in [29]. Where, the author stated, the multilayer technology is difficult to be fabricated and the ineluctable gap between different layers may cause much more insertion loss, which is definitely undesirable in component designs.

In last few years, there are efforts to design such ultra wideband device using only one substrate [24], [25], [26], [27], [28]. This will eliminate some of multilayer design technique limitations such as air gap and misalignment. Unfortunately, designing a device across ultra wideband frequency range using only one substrate is not an easy task. Many researchers faced difficulty in dealing with a very small design size such as too thin width of transmission line [26] and extremely narrow spacing between coupled-lines [27]. The design of H-hybrid presented by Aikawa and Ogawa in [26] has very thin size of coupled slot-lines and must be fabricated carefully to avoid an undesired result. While, the visible discrepancy shown by power divider design in [27] is mainly due to the zero fabrication tolerance in etching the tight coupled-line with small spacing of 0.06 mm. The design presented in [26] and [27] are difficult to be fabricated in common fabrication laboratory due to the

width and gap are tremendously thin. Thus, generally each dimension size of the fabricated designs must be accurate to ensure that the device can be operated across the desired operating frequency of 3.1 to 10.6 GHz. Meanwhile, in [25], the microstrip-slot technique is used to design power divider component. From the result between simulation and measurement, the proposed divider operated at UWB frequency range. However, the isolation between output ports is no better than 10 dB, which commonly required in the divider design [25]. Then, for the coupler design, in [30], the rectangular slot underneath coupled lines is proposed. The proposed design has increased the spacing between coupled lines to 0.12 mm. However, the design of [30] has some limitation of the leaked field, which may affecting the performance of device and at once cause unwanted interference with the other devices in the integrated system. Also, in [28], the 3 dB coupler using floating-potential method is proposed. Even though the performance is good across UWB frequency range, but the width of spacing must be exactly 0.13 mm to avoid the degradation of performance, when the spacing is increased or decreased more than 0.02 mm.

Meanwhile, in six-port network design, there are several techniques have been proposed in order to produce a six-port network that can operate in ultra wideband operating frequency range. Such as in [31], the multilayer techniques is proposed. The excellent performance has been achieved across UWB frequency band. However, due to the use of two substrates in the multilayer structure, it is facing the challenges of misalignment and air gap problem. Then, in [32], Palencia et. al used a combination technique of planar and coaxial technology. The proposed design has achieved good performance, which operates in the frequency band of 0.7 to 6 GHz. However, the appearance is bulky, as it uses a power divider and couplers connected with the coaxial cables. Then, in [33]-[34], several six-port network designs employing single layer technique has been designed, where the good result has been obtained across wider frequency range. However, the UWB coverage is still not achievable.

Therefore, by considering these problems in designing UWB components, new coupler and power divider with the consideration of simple design shape and

method will be proposed with the goal to have simple design and convenient usage to form a multi-port network.

### **1.3 Objective of the Research**

The works undertaken in this thesis are aiming on the following objectives:

- 1) To design new UWB coupler and power divider that will be used to form a six-port network.
- 2) To apply the designed coupler and power divider in constructing the six-port network.
- 3) To investigate the performance of six-port network across UWB frequency band of 3.1 to 10.6 GHz.

By achieving the stated objectives, the new designed six-port network with very well UWB performance can be used in many applications. One of the applications is to replace mixer-based approach in the communication transceiver design to act as modulator and demodulator. Thus, this will subsequently reduce the design complexity and increase the bandwidth performance. Therefore, communication transceiver with capability of wideband operating frequency, low power consumption, lower manufacturing cost and low interference can be accomplished.

### **1.4 Scope of the Research**

This research focuses on the design of a UWB six-port network that can be operated within the UWB frequency range from 3.1 GHz to 10.6 GHz. A UWB six-port network, is comprised of UWB power divider and UWB coupler. In order to develop a UWB six-port network, the scope of this research is divided into five parts. Firstly,

the characterization and formulation of a microstrip-slot impedance are studied. The study are performed in order to derive new equations of microstrip-slot impedance,  $Z_{ms}$ . Then, the various structures of couplers and power dividers are designed, simulated, optimized, fabricated, and measured. The novel components of UWB power divider and UWB coupler will be selected to form a UWB six-port network. The simulation and optimization process of individual components and the six-port network is performed using Computer Simulation Technology (CST). Next, the analytical study of coupler and power divider will be performed to observe the behaviour of UWB performance, which also has been carried out using Computer Simulation Technology (CST).

Planar dielectric materials, also known as substrates play an important role in designing microwave circuits and sub-system. As it is crucial to select the best substrate, this proposed study will also look into the investigation of substrates. Followed by that, fabrication of the designed power divider and coupler will be carried out by implementing the most suitable substrate.

The performance of the fabricated components are then verified and experimentally tested by using a vector network analyzer (VNA). The last stage is to use the designed power divider and coupler to form the six-port network. The performance of six-port network will be investigated across UWB frequency band. All simulated and measured results, including transmission coefficients, reflection coefficients and phase differences between the output ports of all designed components, are analyzed and carefully discussed.

## **1.5 Contributions of the Research**

In this thesis, there are five major contributions are presented. The first contribution is the characterization and formulation of a microstrip-slot impedance, which not yet done by other researchers and reported in other works. The equations are derived by using completing square curve fitting method, in which, the relation

between characteristic impedance of microstrip-slot ( $Z_{ms}$ ) with the slot of width ( $W_s$ ) and microstrip-impedance ( $Z_m$ ) is studied based on the substrates with different thickness of 0.508 mm, 0.762 mm and 1.542 mm and relative permittivity between 2 to 5.

The second contribution is a compact design of two-section power divider, which operates over ultra wideband frequency range of 3.1 - 10.6 GHz. The microstrip-slot technique is applied to reduce the size of circuit and achieve wide bandwidth coverage. Where, the rectangular slots are implemented at the ground plane, which positioned symmetrically underneath second and third arms of each microstrip quarter-wave transformer to reduce its length up to 33.34%. This attribute leads to a compact and reduced-size power divider by 23.33% with the dimension of 20 mm x 23 mm and ease of fabrication. The bandwidth performance is improved up to 11.94% compared to the conventional divider.

The third contribution is a new design and analysis of compact ultra wideband (UWB) 3 dB coupled-line coupler. The design of proposed coupled-line structure with zig-zag-shaped slot at the ground plane has shown a greater efficiency for allowing operation at a wider bandwidth, producing a compact size component and minimizing the need of narrow spacing between the coupled lines, which lead to easier fabrication process. In addition, the proposed structure of 3 dB coupled-line coupler is analyzed in order to achieve a strong coupling factor. From the analysis, by adjusting the dimension of the proposed 3-dB coupled-line coupler, the coupling strength can be varied in order to satisfy the strong coupling of 3 dB.

The fourth contribution is a new 90° power divider design that requires an appropriate phase difference of -90° with equal power division, which has being implemented from the proposed ultra wideband 3 dB coupler. The 90° phase difference between the output ports is maintained, which contributed by the quarter wavelength of coupled-line and slotted line underneath.

Then, for the last contribution is concerning the design of new UWB six-port network. The designed six-port is formed by the designed individual components which are proposed divider and coupler. The performance of the proposed six-port is observed and analysed.

## 1.6 Thesis Outline

This section discusses the thesis outline, where the outline is divided into seven chapters. For Chapter 1, the overview of the whole project is discussed, which includes the research background, problem statement, objectives of the research, scope of the research, contributions of the research, and lastly, thesis outline.

Meanwhile in Chapter 2, it is focusing on the literature reviews, where the basic concept of microstrip line, slotline, power divider, H-hybrid, coupler, and six-port network are discussed. Furthermore, the previous related works are reviewed, which mainly focus on the design techniques and characteristics in designing power divider, H-hybrid, coupler, and six-port network.

In Chapter 3, the methodology of this research is discussed. The research work flows of the whole research are presented, which includes design specifications, flow charts and substrate used.

Next, in Chapter 4, the characterization and formulation of a microstrip-slot impedance is presented. The equations are derived by using completing square curve fitting method, based on the relation between characteristic impedance of microstrip-slot ( $Z_{ms}$ ) with the slot of width ( $W_s$ ) and microstrip-impedance ( $Z_m$ ) with different thickness of substrates and relative permittivity. These proposed equations are used in the design of power divider. Next, in this chapter, four designs of power dividers are presented. A simple analysis on suitable length of two-section quarter-wave transformer that formed by microstrip-slot lines is conducted and elaborated in detail.

In Chapter 5, there are several designs of quadrature couplers are proposed. All the performance of the designed quadrature coupler is observed across the designated frequency range. In the quadrature coupler design, several analyses are performed, which are the effect of the techniques, the coupling and the even- and odd-mode characteristic impedance. The analysis and performance of the designed quadrature couplers are described and discussed thoroughly in this chapter.

Furthermore in Chapter 6, three types of six-port networks are designed and presented. The results of the whole six-ports are elaborated and analysed. The comparison of the designs and the performances is further conversed in this chapter.

Lastly, in Chapter 7, the conclusion is drawn. The findings from the research, contributions and recommendations for future works are proposed and described. Moreover, the list of references and appendices are provided at the end of this thesis.

## REFERENCES

1. Nokia Siemens Networks. "2020 : Beyond 4G Radio Evolution for the Gigabit Experience Executive summary," *White Paper*, 2011.
2. D. Fiske, "New Public Safety Applications and Broadband Internet Access Among Uses Envisioned by FCC Authorization of Ultra-Wideband Technology," 2002.
3. N. Seman, "Multi-port reflectometer in multilayer microstrip-slot technology for ultra wideband applications," Ph.D. dissertation, The University of Queensland, Australia, 2010.
4. G. F. Engen, "A ( Historical ) Review of the Six-Port Measurement Technique," *IEEE Transactions on Microwave Theory and Techniques*, vol. 45, no. 12, pp. 2414–2417, 1997.
5. M. E. Bialkowski, A. M. Abbosh, and J. Swayn, "Design of a Compact Microwave Six-port Vector Voltmeter for UWB Applications," *IEEE MTT-S Int. Microwave Symp. Dig.*, 2007, pp. 999–1002.
6. N. Seman and M. E. Bialkowski, "Design of a Uwb Microwave Reflectometer with the use of a Microstrip-Slot Technique," *Microwave and Optical Letters*, vol. 51, no. 9, pp. 2169–2175, 2009.
7. Z. Hui, L. Lin, and W. Ke, "Software-defined six-port radar technique for precision range measurements," *IEEE Sensors Journal*, vol. 8, no. 10, pp. 1745–1751, 2008.
8. B. Boukari, E. Moldovan, S. Affes, K. Wu, R. G. Bosisio, and S. O. Tatu, "A heterodyne six-port FMCW radar sensor architecture based on beat signal phase slope techniques," *Journal of Electromagnetic Waves and Applications. PIER*, vol. 93, pp. 307-322, 2009.
9. A. Koelpin, G. Vinci, B. Laemmle, D. Kissinger, R. Weigel, A. Koelpin, G. Vinci, B. Laemmle, D. Kissinger, and R. Weigel, "The six-port in modern society," *Microwave Magazine. IEEE*, vol. 11, no. 7, pp. 35–43, 2010.
10. R. G. Bosisio, Y. Y. Zhao, X. Y. Xu, S. Abielmona, E. Moldovan, Y. S. Xu, M. Bozzi, S. O. Tatu, C. Nerguizian, J. F. Frigon, C. Caloz, K. Wu, "New-wave radio," *Microwave magazine. IEEE*, vol. 9, no. 1, pp. 89-100, 2008.

11. W. Periodicals, F. Integrated, C. Symposium, R. Mahmoudi, A. Van Roermund, A. M. Conference, H. Kong, T. Meeting, E. Solid, S. Circuits, M. Karlsson, A. Serban, S. Gong, J. Haartsen, and P. Karlsson, "Six-Port Transceiver for 6 – 9 Ghz Ultra wideband Systems," *Microwave and Optical Technology Letters*, vol. 52, no. 3, pp. 740–746, 2010.
12. S. Xu, and F. L. Liu, "Multi-target Detection in FMCW Radar based on Six-Port Technology," *Infrared Milimeter Waves and 14th International Conference on Terahertz Electronics*, 2005. pp. 1–4.
13. G. Vinci, A. Koelpin, and R. Weigel, "Employing six-port technology for phase-measurement-based calibration of automotive radar," *APMC 2009 - Asia Pacific Microw. Conf. 2009*, 2009, pp. 329–332.
14. S. O. Tatu, E. Moldovan, K. Wu, and R. G. Bosisio, "A new direct millimeter-wave six-port receiver," *IEEE Transactions on Microwave Theory and Techniques*, vol. 49, no. 12, pp. 2517-2522, 2001.
15. N. Seman, M. E. Bialkowski, S. Z. Ibrahim, and A. A. Bakar, "Design of an integrated correlator for application in ultra wideband six-port transceivers," *Antennas Propag. Soc. Int. Symp. 2009. APSURSI '09. IEEE*, 2009. pp. 1–4.
16. C. A. Hoer, and K. C. Roe, "Using an arbitrary six-port junction to measure complex voltage ratios," *IEEE Trans. Microw. Theory Tech.*, vol. 23, no. 12, pp. 978–984, 1975.
17. D. Fiske, "New Public Safety Applications and Broadband Internet Access Among Uses Envisioned by FCC Authorization of Ultra-Wideband Technology," 2002.
18. N. Seman, M. E. Bialkowski and W. C. Khor, "Ultra wideband vias and power dividers in microstrip-slot technology," in *in proc. Asia-Pacific Microwave Conference*, 2007, pp. 1383 – 1386.
19. N. Seman and M. E. Bialkowski, "Microstrip-slot transitions and its applications in multilayer microwave circuits," in *in Passive Microwave Components and Antennas, Vienna: In-Tech*, 2010.
20. A. M. Abbosh, M. E. Bialkowski, and J. Mazierska, "An UWB planar out-of-phase power divider employing microstrip-slot and parallel stripline-microstrip transitions," *Asia-Pacific Microw. Conf. Proceedings, APMC*, vol. 2, no. 1, pp. 905–908, 2006.
21. D. N. A. Zaidel, S. K. A. Rahim, and N. Seman, "Design of compact single-section directional coupler for butler matrix beam-forming MIMO," *2011 30th URSI Gen. Assem. Sci. Symp. URSIGASS*, 2011, pp. 1–4.
22. A. M.. Abbosh, M. E. Bialkowski, and D. Thiel, "Ultra wideband bandpass filter using microstrip-slot couplers combined with dumbbell slots and H-shaped stubs," *2009 Asia Pacific Microw. Conf.*, 2009, pp. 909–912.

23. M. E. Bialkowski, N. Seman, and M. S. Leong, "Design of a Compact Ultra Wideband 3 dB Microstrip-Slot Coupler with High Return Losses and Isolation," in *Asia Pacific Microwave Conference, 2009 (APMC 2009)*, 2009, pp. 1334–1337.
24. M. E. Bialkowski and Y. Wang, "Wideband Microstrip 180° Hybrid Utilizing Ground Slots," *IEEE Microw. Wirel. Components Lett.*, vol. 20, no. 9, pp. 495–497, 2010.
25. L. Xiao, H. Peng, and T. Yang, "The Design of a Novel Compact Ultra-wideband (UWB) Power Divider," *Prog. Electromagn. Res. Lett.*, vol. 44, pp. 43–46, 2014.
26. M. Aikawa and H. Ogawa, "A new MIC magic-T using coupled slot lines," *IEEE Trans. Microw. Theory Tech.*, vol. MTT-28, no. 6, pp. 523–528, 1980.
27. S. W. Wong and L. Zhu, "Ultra-wideband power divider with good in-band splitting and isolation performances," *IEEE Microw. Wirel. Components Lett.*, vol. 18, no. 8, pp. 518 – 520, 2008.
28. A. M. Abbosh, "Broadband Parallel-Coupled Quadrature Coupler with Floating-potential Ground Plane Conductor," *Microw. Opt. Technol. Lett.*, vol. 50, no. 9, pp. 2304–2307, 2008.
29. Z. Zhang, Y. Jiao, S. Cao, and F. Zhang, "Design of a broadband three-way power divider using modified microstrip-slotline," *Proc. 2011 IEEE CIE Int. Conf. Radar*, 2011, pp. 1205–1207.
30. A. M. Abbosh, "Broadband Quadrature Coupler with Slotted Ground Plane," *Microw. Opt. Technol. Lett.*, vol. 50, no. 2, pp. 328–331, 2008.
31. G. F. Engen, "An introduction to the description and evaluation of microwave systems using terminal invariant parameters," NBS Monograph 112, 1969.
32. C. M.-Álvarez-Palencia, M. B.-Garcia, and D. R.-Aparicio, "Three Octave Six-Port Network for a Broadband Software Radio Receiver," in *Proceedings of the 40th European Microwave Conference*, 2010, pp. 1110–1113.
33. L. Chang, C. Liao, L. L. Chen, W. B. Lin, X. Zheng and Y.-L. Wu, "Design of an ultra-wideband power divider via the coarse-grained parallel microgenetic algorithm," *Prog. Electromagn. Res.*, vol. 124, pp. 425–440, 2012.
34. A. Abbosh, M. Bialkowski, and S. Z. Ibrahim, "Design of wideband six-port network formed by in-phase and quadrature Wilkinson dividers," *IET Microwaves, Antennas Propag.*, vol. 6, no. 11, pp. 1215–1220, 2012.
35. D. M. Pozar, *Microwave Engineering*. New York: Wiley, 2005.
36. R. Gorg, I. Bahl, and M. Bozzi, *Microstrip Lines and Slotlines*. United States of America, 2013.

37. S. A. Maas, *Microwave mixers*. Artech House, 1993.
38. A. S. Vijayaraghavan, and L. Dunleavy, "Design and optimization of lumped element hybrid couplers," in *High Frequency Electronic, Summit Technical Media, LLC*, 2011.
39. G. Valente, A. Navarrini, and T. Pisanu, "Double Ridged 180 Hybrid Power Divider With Integrated Band Pass Filter," *IEEE Microw. Wirel. components Lett.*, vol. 21, no. 1, pp. 2010–2012, 2011.
40. Y-C. Chiou, C-H. Tsai, J-S. Wu, and J.-T. Kuo, "Miniaturization Design for Planar Hybrid Ring Couplers," in *IEEE MTT-S International Microwave Workshop Series on Art of Miniaturizing RF and Microwave Passive Components*, 2008, pp. 19–22.
41. M. H. Murgulescu, E. Mosan, P. Legaud, E. Pernard, and I. Zaquine, "New wideband  $0.67\lambda_g$  Circumference  $180^\circ$  hybrid ring coupler," *Electron. Lett.*, vol. 30, no. 4, pp. 299–300, 1994.
42. A. Das and S. K. Das, *Microwave Engineering*, 2nd ed. New Delhi: McGraw-Hill, 2009.
43. E. J. Wilkinson, "An N-Way Hybrid Power Divider," *IEEE Trans. Microw. Theory Tech.*, vol. 8, no. 1, pp. 116–118, 1960.
44. D. D. Harty, "Novel design of a wideband ribcage-dipole array and its feeding network," The Worcester Polytechnic Institute, 2010.
45. Y. Lu, G. Dai, X. Wei and E. Li, "A broadband out-of-phase power divider for high power applications using through ground via (TGV)," *Prog. Electromagn. Res.*, vol. 137, pp. 653–667, 2013.
46. J. Guan, L. Zhang, Z. Sun, Y. Leng, and Y. Peng, "Designing power divider by combining Wilkinson and Gysel structure," *Electron. Lett.*, vol. 48, no. 13, p. 769, 2012.
47. A. Sanadhya, A. Mathur, M. S. Chouhan, and K. Singh, "Design of wilkinson power divider using stubs," in *IEEE Microwave radar and wireless communixcation Conference*, 2010, pp. 1–4.
48. X. Tang and K. Mouthaan, "Analysis and design of compact two-way wilkinson power dividers using coupled lines," in *IEEE Asia-Pacific Microwave Conference*, 2009, pp. 1319–1322.
49. J. C. Chiu, J. M. Lin, and Y. H. Wang, "A novel planar three-way power divider," *IEEE Microw. Wirel. Components Lett.*, vol. 16, no. 8, pp. 449–451, 2006.

50. B. Li, X. Wu, and W. Wu, "A 10:1 unequal wilkinson power divider using coupled lines with two shorts," *IEEE Microw. Wirel. Components Lett.*, vol. 19, no. 12, pp. 789–791, 2009.
51. D. Hawatmeh, K. Al Shamaileh, and N. Dib, "Design and analysis of compact unequal-split Wilkinson power divider using non-uniform transmission lines," *2011 IEEE Jordan Conf. Appl. Electr. Eng. Comput. Technol.*, 2011, pp. 1–6.
52. C.-T. Chiang and B.-K. Chung, "Ultra Wideband Power Divider Using Tapered Line," *Prog. Electromagn. Res.*, vol. 106, no. 13, pp. 61–73, 2010.
53. D. Kim, "Planar Magneto-Dielectric Metasubstrate for Miniaturization of a Microstrip Patch Antenna," *Microw. Opt. Technol. Lett.*, vol. 54, no. 12, pp. 2781–2784, 2012.
54. Y. Wu, Y. Liu, and Q. Xue, "An analytical approach for a novel coupled-line dual-band Wilkinson power divider," *IEEE Trans. Microw. Theory Tech.*, vol. 59, no. 2, pp. 286–294, 2011.
55. Q. Guo, Y. Ma, and J. Ju, "A novel broadband high-power combiner," *Asia-Pacific Microw. Conf. Proceedings, APMC*, 2005, pp. 31–34.
56. D. Kang, Y. Pang, and H. Chen, "A Compact Wilkinson Power Divider / Combiner with Two-Section Coupled Lines for Harmonics Suppression," in *IEEE Asian Proceeding Microwave Conference*, vol. 2, no. 1, pp. 995–997, 2012.
57. S. Gruszczynski and K. Wincza, "Miniaturized Broadband Multisection Coupled-Line Wilkinson Power Divider Designed with the use of Quasi-Lumped Element Technique," in *IEEE International Caribbean Conference on Devices, Circuits and Systems*, 2012, pp. 1–4.
58. S.-W. Lee, C.-S. Kim, K. S. Choi, J.-S. Park, and D. Ahn, "A General design formula of multi-section power divider based on Singly Terminated Filter design Theory," in *IEEE International Microwave Symposium Digest*, 2001, pp. 1297–1300.
59. X. P. Ou and Q. X. Chu, "A modified two-section UWB Wilkinson power divider," *2008 Int. Conf. Microw. Millim. Wave Technol. Proceedings, ICMMT*, vol. 3, pp. 1258–1260, 2008.
60. Y. Y. Yao and Z. F. Feng, "A band-notched ultra-wideband 1 to 4 wilkinson power divider using symmetric defected ground structure," *2007 IEEE Antennas Propag. Soc. Int. Symp.*, pp. 860–864, 2007.
61. F. Tao, X. Jun, and W. M. Yan, "Design of 1:3 unequal Wilkinson power divider with defected ground structure," *2010 Int. Conf. Microw. Millim. Wave Technol.*, pp. 646–648, 2010.

62. L. Xiao, H. Peng, T. Yang, and J. Dong, "Power Divider Based on Stepped-Impedance Slotline," *Prog. Electromagn. Res. C*, vol. 50, pp. 147–154, 2014.
63. D. Paolino, "MIC overlay coupler design using spectral domain technique," *IEEE Trans Microw. Theory Tech*, vol. 26, pp. 646–649, 1978.
64. D. H. Werner and S. Ganguly, "An overview of fractal antenna engineering research," *IEEE Antennas Propag. Mag.*, vol. 45, no. 1, pp. 38–57, 2003.
65. I. Bahl, *Lumped elements for RF and microwave circuits*. Boston: Artech House, 2003.
66. L. G. Ji and J. W. Chong, "A new directional coupler design with high directivity for PCS and IMT-2000," *ETRI J.*, vol. 27, no. 6, pp. 697–707, 2005.
67. C. Caloz, A. Sanada, T. Itoh, "A novel composite right-/lefthanded coupled-line directional coupler with arbitrary coupling level and broad bandwidth," *IEEE Trans. Microw. Theory Tech.*, vol. 52, no. 3, pp. 980–992, 2004.
68. S. G. Mao and M. S. Wu, "A novel 3-dB directional coupler with broad bandwidth and compact size using composite right/left-handed coplanar waveguides," *IEEE Microw. Wirel. Components Lett.*, vol. 17, no. 5, pp. 331–333, 2007.
69. M. Dydyk, "Accurate design of microstrip directional couplers with capacitive compensation," in *IEEE MTT-S Int. Microw. Symp. Dig.*, 1990, pp. 581–584.
70. L. F. Franti, and G. M. Paganuzzi, "Wideband high directivity microstrip couplers for microwave integrated circuits," in *Proceeding of 10th Eur. Microw. Conf.*, 1980, pp. 377–381.
71. M. Dydyk, "Microstrip directional couplers with ideal performance via single-element compensation," *IEEE Trans. Microw. Theory Tech.*, vol. 47, no. 6, pp. 956–964, 1999.
72. J. L. Chen, S. F. Chang, and C. T. Wu, "A high-directivity microstrip directional coupler with feedback compensation," in *IEEE MTT-S Int. Microw. Symp. Dig*, 2002, pp. 101–104.
73. R. Phromlounsri, M. Chongcheawchamnan, and I. D. Robertson, "Inductively compensated parallel coupled microstrip lines and their applications," *Microw. Theory Tech. IEEE Trans.*, vol. 54, no. 9, pp. 3571–3582, 2006.
74. R. Phromlounsri, V. Chamnanphrai, and M. Chongcheawchamnan, "Design high-directivity parallel-coupled lines using quadrupled inductive-compensated technique," *2006 Asia-Pacific Microw. Conf.*, pp. 1380–1383, 2006.

75. J. Lange, "Inter digitated stripline quadrature hybrid," *IEEE Trans. Microw. Theory Tech.*, vol. 17, no. 12, pp. 1150–1151, 1989.
76. R. Waugh, and D. LaCombe, "Unfolding the Lange coupler," *IEEE Trans. Theory Tech.*, vol. 20, no. 11, pp. 777–779, 1972.
77. C. Tresselt, "The design and construction of broadband, high directivity, 90-degree couplers, using nonuniform line techniques," *IEEE Trans. Microw. Theory Tech.*, vol. 14, pp. 647–657, 1966.
78. Y. K. Ningsih, M. Asvial, and E. T. Rahardjo, "Design and Analysis of Wideband Nonuniform Branch Line Coupler and Its Application in a Wideband Butler Matrix," *Int. J. Antennas Propag.*, vol. 2012, pp. 1–7, 2012.
79. H. J. Hindin and A. Rosenzweig, "3-db Couplers Constructed from Two Tandem Connected 8.34-dB Asymmetric Couplers," *IEEE Trans. Microw. Theory Tech.*, vol. 16, no. 2, pp. 125 – 126, 1967.
80. H.-H. Ta and A.-V. Pham, "Development of a compact broadband folded hybrid coupler on multilayer organic substrate," *Microw. Wirel. Components Lett. IEEE*, vol. 20, no. 2, pp. 76–78, 2010.
81. J.-H. Cho, H.-Y. Hwang, and S.-W. Yun, "A design of wideband 3-dB coupler with N-section microstrip tandem structure," *Microw. Wirel. Components Lett. IEEE*, vol. 15, no. 2, pp. 113–115, 2005.
82. H.-C. Lu and T.-H. Chu, "Port reduction methods for scattering matrix measurement of an  $n$ -port network," *IEEE Trans. Microw. Theory Tech.*, vol. 48, no. 6, pp. 959–968, 2000.
83. J.-S. Hong, *Microstrip filter for RF/Microwave applications*, 2st ed. Willey, 2011.
84. R. P. Piña, A. D. Jiménez, and C. A. B. Barragán, "The Circuit and Network Analysis of Some Signal Separation Structures Constituting Microwave Six-Port Reflectometers," *Univers. J. Electr. Electron. Eng.*, vol. 2, no. 4, pp. 183–196, 2014.
85. E. G. Cristal and L. Young, "Theory and Tables of Optimum Symmetrical TEM-Mode Coupled-Transmission-Line Directional Couplers," *IEEE Trans. Microw. Theory Tech.*, vol. 13, no. 5, pp. 544 – 558, 1965.
86. J. P. Shelton, R. V. Wagoner and J. J. Wolfe, "Tandem couplers and phase shifters: a new class of unlimited bandwidth components," in *14th Ann. Symp., USAF Antenna Res. Dev. Program, Spons. by Air Force Lab., Wright-Patterson AFB, Dayton, Ohio, held Monticello, Ill., or Microw.*, 1965, pp. 14–19.

87. N. Seman and M. E. Bialkowski, "Design and analysis of an ultrawideband three-section microstrip-slot coupler," *Microw. Opt. Technol. Lett.*, vol. 51, no. 8, pp. 1889–1892, 2009.
88. A. M. Abbosh and M. E. Bialkowski, "Design of Compact Directional Couplers for UWB Applications," *IEEE Trans. Microw. Theory Tech.*, vol. 55, no. 2, pp. 189–194, 2007.
89. Z. Zhang, Y. C. Jiao, X. M. Wang, L. N. Chen, and F. S. Zhang, "Microstrip slotline yields tiny divider," *Microwaves RF*, vol. 50, no. 7, pp. 72–78, 2011.
90. M. Jahanbakht and M. T. Aghmyoni, "Optimized Ultrawideband and Uniplanar Minkowski Fractal Branch Line Coupler," *Int. J. Antennas Propag.*, Hindawi Publ. Corp., pp. 1–4, 2012.
91. N. Seman and M. E. Bialkowski, "Microstrip-slot transitions and its applications in multilayer microwave circuits," in *Passive Microwave Components and Antennas, Vienna: In-Tech*, 2010.
92. A. M. Abbosh, "Broadband Parallel-Coupled Quadrature Coupler with Floating-potential Ground Plane Conductor," *Microw. Opt. Technol. Lett.*, vol. 50, no. 9, pp. 2304–2307, 2008.
93. M. D. C. V-Ahumada, J. Martel and F. Medina, "Parallel Coupled Microstrip Filters with Floating Ground-Plane Conductor for Spurious-Band Suppression," *IEEE Trans. Microw. Theory Tech.*, vol. 53, no. 5, 2005.
94. N. Seman and M. E. Bialkowski, "Design and analysis of an ultrawideband three-section microstrip-slot coupler," *Microw. Opt. Technol. Lett.*, vol. 51, no. 8, pp. 1889–1892, 2009.
95. A. M. Abbosh and M. E. Bialkowski, "Design of compact directional couplers for UWB application," *IEEE Trans. Microw. Theory Tech.*, vol. 55, no. 2, 2007.
96. A. M. Abbosh, M. E. Bialkowski, and D. Thiel, "Ultra Wideband Bandpass Filter Using Microstrip-Slot Couplers Combined with Dumbbell Slots and H-Shaped Stubs," in *IEEE, Microwave conference*, 2009.
97. M. Jahanbakh and M. T. Aghmyoni, "Optimized Ultra wideband and Uniplanar Minkowski Fractal Branch Line Coupler," *Int. J. Antennas Propag.*, Hindawi Publ. Corp., pp. 1–4, 2012.
98. A. M. Abbosh, "Broadband Quadrature Coupler with Slotted Ground Plane," *Microw. Opt. Technol. Lett.*, vol. 50, no. 2, 2008.
99. A. M. Abbosh, "Broadband Parallel-Coupled Quadrature Coupler with Floating-potential Ground Plane Conductor," *Microw. Opt. Technol. Lett.*, vol. 50, no. 9, 2008.

100. D. N. A. Zaidel, S. K. A. Rahim, N. Seman, A. A. Adam, T. A. Rahman, and P. S. Hall, "Compact Uwb Multilayer 3 dB Directional Coupler Design and Analysis on Coupler Performances," *Microw. Opt. Technol. Lett.*, vol. 55, pp. 2214–2219, 2013.
101. D. N. A. Zaidel, S. K. A. Rahim, N. Seman, T. A. Rahman and A. Abdulrahman, "Low cost and compact directional coupler for ultrawideband applications," *Microw. Opt. Technol. Lett.*, vol. 54, pp. 670–674, 2012.
102. N. Seman and M. E. Bialkowski, "Fully integrated UWB microwave reflectometer in multi-layer microstrip-slot technology," *2008 Asia-Pacific Microw. Conf.*, vol. 1, pp. 1–4, 2008.
103. H.-S. Lim, W.-K. Kim, J.-W. Yu, H.-C. Park, W.-J. Byun, and M.-S. Song, "Compact Six-Port Transceiver for Time-Division Duplex Systems," *IEEE Microw. Wirel. Components Lett.*, vol. 17, no. 5, pp. 394–396, 2007.
104. W. L. M. E. V. Valkenburg, *Reference data for engineering Radio, Electronics, Computer, and Communications*, 9th ed. Butterworth-Heinemann, 2002.
105. G. F. Engen, "The six port reflectometer: an alternative network analyzer," *IEEE Trans. Microw. Theory Tech.*, vol. 25, no. 12, pp. 1075–1080, 1977.
106. N. Seman and S. N. A. M. Ghazali, "Quadrature Phase Shift Keying (QPSK) Modulator Design using Multi-Port Network in Multilayer Microstrip-Slot Technology for Wireless Communication Applications," *Radioengineering*, vol. 24, no. 2, pp. 527–534, 2015.
107. R. C. Yob, N. Seman, and S. N. a M. Ghazali, "Error Vector Magnitude Analysis for Wideband QPSK and QAM Six-Port Modulator," *2011 IEEE Int. RF Microw. Conf. (RFM 2011)*, 2011, pp. 149–153.
108. R. Hussain and M. S. Sharawi, "A Dual Six-Port with two-Angle Resolution and Compact Size for Mobile Terminals," in *IEEE Radio and Wireless Symposium (RWS)*, 2014.
109. S. O. Tatu and T. A. Denidni, "A new beam direction finding circuit based on six port technology," in *in Microwave Symposium Digest, 2005 IEEE MTT-S International. IEEE*, 2005, pp. 581–584.
110. A. S. Mohra, "Six-Port Reflectometer based on four 0°/180° Microstrip Ring Couplers," *Microw. Opt. Technol. Lett.*, vol. 40, no. 2, 2004.
111. J. Hughes and K. Wilson, "High Power Multiple Impatt Amplifiers," *Microw. Conf. 1974. 4th Eur.*, vol. 150, pp. 118–122, 1974.
112. X.-T. Fang, X.-C. Zhang, and C.-M. Tong, "A Novel Miniaturized Micro-Strip Six-Port Junction," *Prog. Electromagn. Res. Lett.*, vol. 23, pp. 129–135, 2011.

113. Rogers Corporation, "RO4003® high frequency circuit material insertion loss comparison with other material types," 1997.
114. Rogers Corporation, "Advance Circuit Material Division, RO4000® thermoset microwave materials," 2008.
115. Rogers Corporation, "Advance Circuit Material Division, RO4000® series high frequency circuit materials," 2010.
116. Rogers Corporation, "Advance Circuit Material Division, RO3000® series high frequency laminates," 2010.
117. P. & M. S. (Rochdale), "FR4 Data Sheet," 2011.
118. S. M. Mahmood and A. M. Jassim Al-Hindawi, "Theoretical and Experimental Results of Substrate Effects on Microstrip Power Divider Designs," *Int. J. Microw. Sci. Technol.*, vol. 2011, pp. 1–9, 2011.
119. N. K. Das, "Generalized multiport reciprocity analysis of surface-to-surface transitions between multiple printed transmission lines," *IEEE Trans. Microw. Theory Tech.*, vol. 41, no. 6–7, pp. 1164–1176, 1993.
120. L. G. Maloratsky, "Microstrip Circuits with a Modified Ground Plane," *High Frequency Des., Summit Technical Media*, pp. 38–47, 2009.
121. N. C. Karmakar, *Handbook of smart Antennas for RFID system*, 1st ed. Canada, 2010.
122. I. J. Bahl, *Fundamentals of RF and microwave transistor amplifiers*, 1st ed. Canada: Wiley, 2009.
123. R. Janaswamy and D. Schaubert, "Characteristic Impedance of a Wide Slotline on Low-Permittivity Substrates," *IEEE Trans. Microw. Theory Tech.*, vol. 34, no. 8, pp. 900–902, 1986.
124. K. H. Yusof, N. Seman, and M. H. Jamaluddin, "Design of U-Shaped In-Phase Power Divider Employing Ground-Slotted Technique for Wideband Applications," *Wirel. Pers. Commun.*, vol. 81, no. 1, pp. 359–371, 2015.
125. R. Janaswamy and D. H. Schaubert, "Characteristic Impedance of a Wide Slotline on Low- Permittivity Substrates," *IEEE Trans. Microw. Theory Tech.*, vol. MTT-34, no. 8, 1986.
126. C. S. Kim, J. S. Park, D. Ahn, and J. B. Lim, "A novel 1-D periodic defected ground structure for planar circuits," *IEEE Microw. Guid. Wave Lett.*, vol. 10, no. 4, pp. 131–133, 2000.
127. C. S. Kim, J. S. Lim, J. S. Park, D. Ahn, and S. Nam, "A 10 dB Branch Line Coupler Using Defected Ground Structure," *30th EUMC*, vol. 3, pp. 68–71, 2000.

128. M. Winebrand and R. Vladimir, "Slot spiral miniaturized antenna," 6,791,497B2, 2004.
129. S. Zhao, C. Fumeaux, and C. Coleman, "Evolutionary Optimization of Zig-Zag Antennas Using Gaussian and Multiquadric Radial Basis Functions," *In: Proceeding of Asia-Pacific Microwave Conference*, 2011, pp. 1594–1597.
130. D. N. A. Zaidel, "Ultra Wideband Butler Matrix for Beam-Forming Network," Ph. D. Dissertation, Universiti Teknologi Malaysia, 2014.