DIRECT MODEL REFERENCE ADAPTIVE CONTROL OF COUPLED TANK LIQUID LEVEL CONTROL SYSTEM

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ABSTRACT

Industries such as petro-chemical industries, paper making industries, waste management and others are the vital industries where liquid level and flow control are essential. Liquids will be processed by chemical or mixing treatment in the tanks, but always the level fluid in the tanks must be controlled, and the flow between tanks must be regulated in the presence of nonlinearity and inexact model description of the plant. This project investigates the usage of Direct Model Reference Adaptive Control (DMRAC) in controlling the liquid level in the second tank of Coupled-Tank plant through variable manipulation of water pump in the first tank. It is to show that DMRAC could produce appropriate control signal to the coupled-tank system in response to the given desired water level with plant nonlinearity and measurement noise present simultaneously. The ability to use only input-output measurement of the plant in adaptation mechanism is the DMRAC's special characteristics that does not require the explicit identification of the model description nor the solution to linear(or nonlinear) equations of the respective plant dynamics. A dynamic model of the plant is initially developed. Simulation studies are then conducted based on the developed model using Matlab and Simulink. A series of tracking performance tests, disturbance rejection and plant parameter changes are conducted to evaluate the controller performance in comparison to PID controller. The outcome of the project reveals that DMRAC is more robust than PID controller when there is a change in system parameters despite of its sensitivity to measurement noise. The framework of this project is generic enough to have an overview of the possible outcome before implementing the DMRAC controller in real-time system in the future.

ABSTRAK

Industri petrokimia, industri pembuatan kertas, dan lain-lain merupakan industri utama dimana kawalan aras cecair dan arus adalah penting. Lazimnya, cecair-cecair itu akan diproses secara rawatan kimia atau pencampuran dalam tangki tetapi selalunya aras cecair dalam tangki tersebut perlu dikawal dan arus antara tangki perlu diteraturkan dalam keadaan sistem yang sememangnya tidak linear dan modelnya kurang maklumat. Projek ini menyelidik penggunaan Direct Model Reference Adaptive Control atau DMRAC dalam pengawalan aras cecair pada Tangki kedua dalam system tangki berkembar dengan memanipulasikan pam air di tangki pertama. Ini bagi menunjukkan bahawa DMRAC dapat menghasilkan isyarat kawalan yang munasabah dalam kawalan aras cecair bagi system, hasil daripada tindakbalas kepada titik rujukan aras cecair yang diberi dalam keadaan sistem yang tidak linear dan terdapatnya pengukuran hingar dalam proses secara serentak. Kebolehan menggunakan hanya pengukuran masukan-keluaran dalam mekanisma adaptasi ialah merupakan cirri-ciri istimewa bagi DMRAC dimana ia tidak perlukan pengenalanpastian eksplisit bagi sistem model. Ia juga tidak memerlukan penyelesaian terhadap dinamik persamaan linear (atau tidak linear) bagi system tersebut. Ujian prestasi penjejakian (tracking performance test), penyisihan gangguan dan perubahan parameter sistem telah dijalankan untuk menilai prestasi pengawal DMRAC dan dibandingkan dengan prestasi pengawal PID. Hasil daripada projek ini menunjukkan DMRAC lebih robust berbanding dengan PID dimana system perubahan parameter tidak memberi kesan pada DMRAC walaupun ia sedikit sensitif terhadap hingar. Rangka projek ini adalah umum dalam memberi gambaran keseluruhan pada kemungkinan yang akan berlaku apabila pengawal DMRAC dilaksanakan untuk sistem masa-nyata.

TABLE OF CONTENTS

CHAPTER	TITLE		
	DEC DED ACK ABS ABS TAB LIST LIST	LE PAGE CLARATION CONTENT CATION CONTENTS COF CONTENTS COF FIGURES COF SYMBOLS	i ii v vi vii viii ix xiii xv xvii
1	INTI	RODUCTION	1
	1.1	Overview	1
	1.2	Problem Statements	2
	1.3	Objectives	3
	1.4	Scope of the Project	4
	1.5	Summary	5
2	LITI	ERATURE REVIEW	
	2.1	Overview	6
	2.2	Genetic Algorithm (GA) tuning of a neuro-fuzzy	7
		controller on a coupled- tank system.	
	2.3	Current research studies on the application of self-	8
		tuning controller on coupled-tank system.	
	2.4	Current research studies on the application of PID	9
		controller on coupled-tank system.	
	2.5	Comparative study between two adaptive systems	10
		and Neural Network Control	

	2.5.1	Self-tuning regulator (STR) case	10
	2.5.2	Model Reference Adaptive Control	12
		(MRAC) case	
	2.5.3	Cerebellar Model Articulation Controller	14
		(CMAC) case	
2.6	Summa	ary	17
COU	PLED-T	ANK SYSTEM	
3.1	Overv	iew	18
3.2	Introdu	uction to Coupled-Tank Control Apparatus	18
	CT-10	0	
3.3	Funda	mental Control Principle of Coupled-Tank	20
	Systen	1	
3.4	Import	ant parameters of the coupled-tank system	23
3.5	Summ	ary	23
RESE	CARCH	METHODOLOGY	
4.1	Under	standing the coupled-tank system	24
4.2	Identif	ying dynamics of nonlinear plant	24
4.3	Contro	oller Design	25
4.4	Simula	ation	26
4.5	Metho	odology	27
MOD	EL REF	FERENCE ADAPTIVE CONTROL	
5.1	Introd	uction	28
5.2	Definit	ion	29
	5.2.1	Adaptive System	29
	5.2.2	Model Reference Adaptive System (MRAS)	29
5.3	Classif	ications of MRAC	30
5.4	Adapti	ve Laws	32
	5.4.1	Sensitivity Method	32
	5.4.2	Gradient and least squares methods based	33
		on estimation error cost criteria	

		5.4.3	Lyapunov and Positivity Design Approach	34
	5.5	Summar	у	34
6	MAT	HEMATI	CAL MODELLING OF THE	35
	COU	PLED-TA	NK SYSTEM	
	6.1	Overview	N	35
	6.2	Nonlinea	ar model of coupled-tank system	35
	6.3	A Linear	rised Perturbation Model	37
	6.4	First Ord	ler Single-Input Single Output (SISO) Plant	39
		System		
	6.5	Second (Order Single-Input Single Output (SISO)	41
		Plant Sys	stem	
	6.6	State Spa	ace Model of Coupled-Tank	45
		6.6.1	State Space Model with SISO configuration	45
7	DESI	GN OF		
	MOD	EL REFE	RENCE ADAPTIVE CONTROLLER	
	7.1	Overview	W	48
	7.2	Direct M	Iodel Reference Adaptive Control	49
		Algorith	m	
	7.3	Stability	analysis of the DMRAC algorithm	55
	7.4	Reference	ee Model Setup	59
		7.4.1	Reference Model (nominal type)	61
		7.4.2	Reference Model Type 2 (Slow response)	66
		7.4.3	Reference Model Type 3 (Fast response)	67
	7.5	Adaptatio	on Mechanism	69
	7.5.1	Adaptatio	on weights for nominal response	71
	7.5.2	Adaptatio	on weights for slow response	72
	7.5.3	Adaptatio	on weights for fast response	72
	7.6	Summar	у	73
8	SIMU	LATION	RESULTS	
	8.1	Overview		74
	8.2	Coupled-	tank system parameters	74

xi

8.3	Nonlin	ear model of the coupled-tank plant in	75
	Simuli	ink	
	8.3.1	Actuator dynamic	77
8.4	Simulati	ion of PID controlled coupled-tank	78
	8.4.1	Ziegler-Nichols on-line tuning method	80
	8.4.2	Setpoint Tracking performance	84
	8.4.3	Disturbance Rejection Performance	87
	8.4.4	Plant parameter changes	88
8.5	Simulat	tion of DMRAC controlled coupled-tank	89
	8.5.1	Setpoint tracking performance	90
	8.5.2	Disturbance Rejection Performance	98
	8.5.3	Plant parameter changes	101
8.6	Perform	nance comparison between DMRAC and PID	102
	8.6.1	Without measurement noise	103
	8.6.2	With measurement noise	103
	8.6.2.1	Setpoint tracking with measurement noise	104
	8.6.2.2	Disturbance rejection with noise	106
	8.6.2.3	Plant parameter changes	107
8.7	Discussi	on on performance of DMRAC and PID	108
	controlle	er	
CO	NCLUSI	ON AND FUTURE RECOMMENDATION	
9.1	Conclusi	ions	110
9.2	Recomm	endations	111
REI	FERENCI	ES	114

LIST OF TABLES

Table		Page
no. 2.1	Summary of Comparative Study	16
3.1	Steady-state condition for the coupled-tank system.	22
7.1	Nominal Specification Reference Model	61
7.1a	Normalised rise time vs damping ratio for a second order	62
	underdamped response	
7.2	Reference Model with slow response specification	66
7.3	Reference Model with fast response specification	68
7.4	Adaptation Weightsfor nominal response profile	71
7.5	Initial values for adaptation gain	71
7.6	Adaptation Weights for slow response profile	72
7.7	Adaptation Weights for fast response profile	72
8.1	Coupled-Tank System Parameter (recalled)	75
8.2	Simulink Simulation Settings	78
8.3	Plant input-output description	79
8.4	A table of parameters tuned using closed-loop Ziegler-	81
	Nichols method for quarter decay ratio	
8.5	Updated PID controller parameter	82
8.6	Performance Index with various alpha settings for nominal	89
	response profile	
8.7	Performance index with various alpha settings for slow	91
	response profile	
8.8	Performance specification that defines reference model for	91

slow response

8.9	Performance index with various alpha settings for fast	93
	response profile	
8.10	Performance specification that defines reference model for	93
	fast response	
8.11	Performance Index for different setpoint tracking profile	98
8.12	Performance Comparison	103
8.13	Performance Comparison in terms of setpoint tracking in	105
	the presence of noise	
8.14	: Performance Comparison in terms of disturbance	106
	rejection in the presence of noise	
8.15	Performance comparison for plant parameter changes	107

LIST OF FIGURES

Figure		Page
no.		C
2.1	STR (tracking with noise)	11
2.2	STR tracking (nonlinear case)	12
2.3	MRAC parameters (with noise)	13
2.4	MRAC tracking (with model)	13
2.5	MRAC tracking (nonlinear case)	14
2.6	CMAC tracking (with noise)	15
3.1	Coupled-Tank Control Apparatus CT-100	19
3.2	Schematic diagram of CTS-100	21
4.1	Research methodology	27
5.1	Model Reference Adaptive Control	30
5.2	Indirect MRAC	31
5.3	Direct MRAC	31
6.2	Block Diagram of First Order Plant Model in Laplace representation	41
6.3	Block Diagram of Second Order Plant Model in Laplace representation	44
7.1	Systematic Procedure to setup reference model	60
7.2	Signal flow graph before modification	64
7.3	Modified Signal flow graph to express an output regulator	64
8.1	for reference model Modified Signal flow graph to express an output regulator for reference model	76
8.2	Saturation representation	76
8.3	Masked subsystem that contains the nonlinear model of the coupled-tank	77
8.4	Masked subsystem that contains the actuator dynamics	77
8.5	Saturation to the volumetric flow rates	78
8.6	Simulink diagram to simulate PID controlled coupled-tank	79
8.7	Response of the system showing the sustained oscillation	81
	where ultimate gain and period can be derived.	-
8.8	Response of the system after the controller have been updated with the values calculated.	82
8.9	Response of the system after the controller have been	83

8.10 Figure no.	updated with the values adjust to meet satisfactory transient response Signal generator to apply different set point changes	84 Page
8.11	Response of the system with PID controller in terms of set point tracking performance	85
8.12	control effort in terms of volumetric flowrates	86
8.13	Response of the system by PID controller in the presence of load disturbance with 40 cm^3/s of flowrate	87
8.14	Response of the system by PID controller when outlet at tank 1 is closed	88
8.15	Response of the system for different operating level for nominal response	90
8.16	Response of the system for different operating level for slow response	92
8.17	Response of the system for different operating level for fast response	94
8.18	(a) Response of the system for setpoint tracking Profile 1(b) Control Effort in terms of volumetric flowrate for setpoint tracking Profile 1	95 96
8.19	(a)Response of the system for setpoint tracking profile 2(b) Control Effort in terms of volumetric flowrate for setpoint tracking Profile 2	96 97
8.20	(a) Response of the system for setpoint tracking profile 3(b) Control Effort in terms of volumetric flowrate for setpoint tracking Profile 3	97 98
8.21	(a) Response of the system for disturbance rejection with $d=20 \ cm^3/s$	99
	(b) Control effort in terms of volumetric flowrate for d=20 cm^3/s	
8.22	(a) Response of the system for disturbance rejection with $d=40 \ cm^3/s$	100
	(b) Control effort in terms of volumetric flowrate for d=40 cm^3/s	
8.23	(a) Response of the system when the outlet of tank 1 is closed.	101
	(b) Control effort in terms of volumetric flow rate when the outlet of tank 1 is closed	102
8.24	Simulated measurement noise	104
8.25	Performance of DMRAC and PID controller in terms of setpoint tracking in the presence of noise	105
8.26	Performance of DMRAC and PID controller in terms of disturbance rejection in the presence of noise	106

8.27 Response of the system by DMRAC and PID in response 107 to the outlet's closing

LIST OF SYMBOLS

A_{i}	-	Cross Sectional Area of the respective <i>i</i> coupled tank reservoir
$lpha_{_i}$	-	Proportionality constant that depends on discharge coefficient,
		orifice cross sectional area and gravitational constant
K _{sensor}	-	Sensor gain
K_{pump}	-	Pump gain
Qimax	-	Maximum allowable volumetric flowrate pumped by motor
TC	-	Pump motor(valve) time constant
H1, H2	-	height of liquid in tank 1 and tank 2 respectively
Q_{o3}	-	flow rate of liquid between tanks
Q_{i1}, Q_{i2}	-	pump flow rate into tank 1 and tank 2 respectively
Qol, Qo2	-	flow rate of liquid out of tank 1 and tank 2
$Q_c(t)$	-	computed or the commanded flow rate
$q_i(t)$	-	the time-varying input flow rate
$ au_a$	-	Time constant of actuator
V	-	Lyapunov function
\dot{V}	-	Time derivative of Lyapunov function
$K_e(t)$	-	Stabilizing gain (time varying)
$K_x(t)$	-	Adaptation gain from reference model state vector (time varying)
$K_u(t)$	-	Adaptation gain from commanded setpoint (time varying)
$u_p(t)$	-	Control law (time varying)

- *T* Adaptation weights for Integral adaptation
- \overline{T} Adaptation weights for Proportional adaptation (time varying)
- $K_I(t)$ Proportional adaptation (time varying)
- $K_p(t)$ Integral adaptation
 - σ Forgetting Factor
 - e_x State error

CHAPTER 1

INTRODUCTION

1.1 Overview

Nowadays, the process industries such as petro-chemical industries, paper making and water treatment industries require liquids to be pumped, stored in tanks, and then pumped to another tank. The control of liquid in tanks and flow between tanks is a basic problem in the process industries. The above mentioned industries are the vital industries where liquid level and flow control are essential. Many times the liquids will be processed by chemical or mixing treatment in the tanks, but always the level fluid in the tanks must be controlled, and the flow between tanks must be regulated. Level and flow control in tanks are the heart of all chemical engineering systems.

Due to the nonlinearity of the coupled tank system, MRAC or model reference adaptive control which is one of a kind in adaptive control techniques is implemented. It is regarded as an adaptive servo system in which the desired performance is expressed in terms of reference model, which gives the desired response to a command signal. The nonlinearity occurs because the system transfer function varies or changes with the height of the liquid in a tank and the controller ought to be adaptive and robust for these changes.

1.2 Problem statements

The first and foremost important step before formulating a controller, a mathematical relationship or the governing dynamics between the input and the output of the system should be known. The underlying principle and knowledge of the system should be investigated to comprehend the occurrence of nonlinearity in the system dynamics. There are wide arrays of control techniques that can be applied to meet the control objective of the system and these depend on the factors of which the proposed design objective might rely on. There are factors such as tracking, reducing the effects of adverse conditions and uncertainty, behaviors in terms of time response (e.g., stability, a certain rise-time, overshoot, and steady state tracking error) and lastly engineering goals such as cost and reliability which is vital in industrial perspective.

Sophistication of controller scheme primarily depends on the degree of how the nonlinearity can be tolerated and assumed using the linearization theory. Moreover, apart from nonlinearities, there may be a consequence of unknown parameters which hinders the objective to obtain a complete detail model of a process available for control purpose. The factors that abstained many researchers to use conventional control theory and techniques can be listed as follows:-

- i. Systems are nonlinear and may contain unknown parameters. That unknown parameters may not be estimated accurately if reliable experimental data is absent.
- ii. The delays present in the process of system (coupled tank system specifically) might complicate achieving high performance control.
- iii. There are several cases such as that of couple tank in industry where the process or disturbance characteristics are changing continuously. This requires simultaneous regulation of various variables in order to maintain the desired liquid level. Thus, a model must account for all of the most significant variables of the process.

Due to the above mentioned factors, it might be difficult to formulate a control strategy based on the analytical model because the mathematical model is usually linearised to account for complexity and nonlinearity which are inevitable in a complicated system. PID(proportional-integral-derivative) control is one of a kind of control scheme that uses the approach of linearised model. However, the PID controller might not capable to satisfy the control objectives or requirement at all times as it need to be regularly tuned due to the varying system dynamics.

Hence, it is desirable to have a robust and reliable control technique for modeling the complex and nonlinear system that prevails in all industrial process. MRAC or model reference adaptive control is chosen as the coupled tank's control scheme. It is regarded as a novel approach in parameter adjustment for a system where process dynamics are nonlinear.

1.3 Objectives

The objectives of the project can be outlined likewise:

- To develop an adaptive system for a couple tank system using DMRAC (Direct Model Reference Adaptive Control).
- ii. To investigate the performance of DMRAC (Lyapunov and Positivity concept) in control of coupled-tank and compare with the system controlled by PID controller.

1.4 Scope of the project

The purpose of this project can be divided into four parts, the first part is to develop and validate a mathematical dynamic model that represents the coupledtank control apparatus. This includes models for first order and second order system as well as the nonlinear model of the system.

Then, after the models are approved of its validity, simulation will be performed using engineering simulation software like Matlab Simulink to simulate its dynamic characteristic using the actual plant parameters obtained from laboratory. A step test was performed on the nonlinear model of the coupled-tank system by simulation to observe various important dynamic characteristics at different operating conditions(water level). This is to investigate the behaviour of the system at certain range of operating conditions and thus, will give a guideline in the development of a reference model for the system to track.

The third part of the project will follow consequently after the second part and this involves the design of the controller; firstly normal PID control, then followed by the adaptive controller (DMRAC). Normal PID control, with expectation in mind, will exhibits its limitation in coping with nonlinearities and changes in process gain. DMRAC will be developed by implementing a suitable adaptive algorithm that will make the nonlinear system be able to adapt to set point changes(servo) and sudden load disturbances (regulator). The final part will comprise of brief comparative study based on performance of the two controllers.

1.5 Summary

This section explains the objective as well as the scope of the project in order to give an insight and the sense of direction of this project. The next subsequent chapter will be literature review section, discussing on the research works previously done by other researchers concerning on the liquid level control of coupled tank system. Different control strategies are demonstrated by various researchers in the literatures and are evaluated in comparison with other controllers. The augmentation of feedforward compensator in all three configurations can guarantee stability of more realistic systems. Special attention must be given on the method of designing these extended DMRAC algorithms.

Finally, it is of great interest to implement the DMRAC algorithm on the real time system for future works purpose. The real time implementation requires the DMRAC algorithm to be in digitized form. Therefore, special care should be taken in the digital domain and some of them can be summarized as follows,

- i. The gains may be computed at the same frequency as the control update frequency or slower. Euler type algorithm should be adequate for computing the integral gain K_I .
- ii. The reference model output and state vectors can be computed digitally at any assigned sampling frequency.
- iii. It is desirable for the outputs to be sensed sufficiently fast with adequate computing power in order for all the functions to be computed at the same frequency.
- iv. If the reference model time constants are relatively small and demand control frequency faster than the sensor frequency, then the sensed outputs may have to be interpolated to give values at intermediate times.

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