RELATIONSHIP BETWEEN MICROSTRUCTURE AND MECHANICAL PROPERTY OF NICKEL-ALUMINUM BRONZE ALLOY SOLIDIFIED AT DIFFERENT COOLING RATE AND HEAT TREATED

NURHAULIA BINTI RAZALI

A thesis submitted in fulfillment of the requirements for the award of the degree of Master of Engineering (Materials Engineering)

> Faculty of Mechanical Engineering Universiti Teknologi Malaysia

This thesis is dedicated to my beloved Husband (Abdul Hakim Chow), my late Father (Razali Yahya)

Mother (Azizah Rosly), Family, and Friend

ACKNOWLEDGEMENT

At the most, I express my highest gratitude to Allah SWT for the blessing and kindness through all the days that I went through to complete my Master's degree and project in Universiti Teknologi Malaysia (UTM). Also I would like to thank to my supervisor, Dr. Muhamad Azizi Bin Mat Yajid and co-supervisor Prof. Dr. Hj. Mohd Hasbullah Bin. Hj. Idris for their encouragement and guidance throughout the entire research. Without their supports this thesis would not be able to complete on time.

Not to forget, to all UTM staff especially technicians from Faculty of Mechanical Engineering, and Post Doctorate student, Dr. Saeed Farahany, PhD student Azmah Noordin, for the countless assistance and contributed in teaching me throughout this research.

As well, very special thanks go to my husband Abdul Hakim Chow, daughter Nurin Aisyah and my mother, Mrs. Azizah Rosly for their support and dedication.

ABSTRACT

Nickel-Aluminium Bronze (NAB) is copper-based alloy, which widely used in marine applications because it provides high mechanical strength and low corrosion rates under turbulent flow conditions. Belongs to group of aluminium bronzes it contains 5-12 wt. % aluminium with additions of iron and nickel up to 6 wt. %. Presence of aluminium increases the mechanical properties of the alloy by the establishment of a face-centered cubic (FCC) phase that could improve the casting and hot working properties of the alloy. With the use of computer aided cooling curve thermal analysis (CA-CCTA) the phase transformation during casting can be revealed which can be done by the first derivation from the cooling curve data of the NAB alloy. This method is can be useful for designing the casting parameter of the NAB alloy in order to improve its mechanical property and obtained desired mechanical properties. In this research, the effect of cooling rate during solidification is demonstrated by using different mould during casting of NAB alloy whereby high cooling rate will produces finer grain as compare to slow cooling. Similarly, at higher cooling rate will result in higher hardness in comparison with the slower cooling rate. The mechanical properties of the as cast alloy will be further improved by applying heat treatment at temperature of 900 °C for two hours and water quenched followed by ageing at temperature of 350 °C -400 °C for 1-3 hours and air cooled. Aged samples from ceramic mould attained highest hardness after aged at 350 °C for 3 hours and samples from permanent mould gave higher hardness after aged at 350 °C for one hours. Prolonged soaking time and increasing ageing temperature resulted in reducing hardness due to over aged.

ABSTRAK

Nikel-Aluminium Gangsa (NAB) adalah aloi yang berasaskan tembaga telah digunakan secara meluas dalam aplikasi marin kerana ia memberikan kekuatan mekanikal yang tinggi dan kadar kakisan yang rendah di bawah keadaan aliran laju. Ianya tergolong dalam kumpulan aluminium gangsa mengandungi antara 5-12 wt. % aluminium dengan penambahan besi dan nikel sehingga 6 wt. %. Kehadiran aluminium meningkatkan sifat-sifat mekanik aloi dengan fasa berpusat muka (FCC) yang boleh meningkatkan kerja panas aloi. Dengan menggunakan bantuan komputer, analisis terma lengkung penyejukan (CA-CCTA) boleh melihatkan pembentukan fasa semasa kaedah tuangan dilakukan. Kaedah ini berguna untuk merekabentuk parameter kaedah tuangan aloi bagi meningkatkan kekuatan mekanik aloi. Dalam kajian ini, kadar penyejukan semasa pemejalan di tunjukkan dengan menggunakan acuan yang berbeza bagi menghasilkan kadar penyejukan cepat yang menghasilkan bijirin yang lebih halus berbanding dengan penyejukan perlahan. Dan juga, pada kadar penyejukan yang lebih cepat akan menyebabkan kekerasan yang tinggi pada aloi berbanding dengan kadar penyejukan perlahan. Nilai mekanikal aloi ini boleh diperbaiki dengan menggunakan rawatan haba dengan sampel dari kadar penyejukan yang berbeza telah dirawat pada suhu 900 °C selama dua jam dan disejuk cepat dengan menggunakan medium air dan kemudian dirawat haba dengan suhu 350 °C -400 °C selama 1-3 jam. Sampel terawat haba dari acuan seramik mencapai kekerasan tertinggi selepas rawatan haba pada suhu 350 °C selama 3 jam dan sampel dari acuan kekal memberikan kekerasan yang lebih tinggi pada 350 °C selama satu jam. Masa rawatan haba yang berpanjangan dengan peningkattan suhu rawatan haba menyebabkan mengurangkan kekerasan pada aloi.

TABLE OF CONTENTS

CHAPTER		TITLE	PAGE	
	DEC	LARATION	ii	
	DED	ICATION	iii	
	ACK	NOWLEDGEMENTS	iv	
	ABS	TRACT	v	
	ABS	TRAK	vi	
	TAB	LE OF CONTENTS	vii	
	LIST	T OF TABLES	xi	
	LIST	OF FIGURES	xiii	
	LIST	OF ABBREVIATIONS	xvii	
	LIST	T OF SYMBOLS	xviii	
	LIST	T OF APPENDICES	xix	
1	INTRODUCTION			
	1.1	Background	1	
	1.2	Objective of Study	2	
	1.3	Problem Statement of the Research	2	
	1.4	Scope of the study	2	
2	LITI	ERATURE REVIEW		
	2.1	Nickel-Aluminium Bronze (NAB) Alloy	4	
	2.2	Solidification of Nickel-Aluminium Bronze Alloy	5	
		2.2.1 The β -phase	8	
		2.2.2 The α -phase	8	
		2.2.3 The eutectoid $\alpha + \gamma_2$ phase	10	

				viii
		2.2.4	The intermetallic κ- phases	11
		2.2.5	Computer-Aided Cooling Curve Thermal	
			Analysis (CA-CCTA)	13
		2.2.6	Cooling Curve of Continuous Cooling of	
			NAB Alloy	16
	2.3	The H	eat Treatment of Nickel-Aluminium Bronze	
		(NAB) Alloy	18
		2.3.1	Solution Heat Treatment	19
		2.3.2	Ageing Treatment	20
		2.3.3	Effect of Ageing on Mechanical Properties	
			of Nickel-Aluminium Bronze (NAB) Alloy	20
		2.3.4	Summary of Solution Heat Treatment and	
			Ageing Treatment by Various Literature	25
3	RESI	EARCH	METHODOLOGY	
	3.1	Introd	uction	27
	3.2	Moulo	Selection and Preparation	28
	3.3	Gener	al Melting and Casting Process	31
	3.4	Coolin	ng Curve Thermal Analysis Technique	33
	3.5	Prepai	ration of the Samples for Further Analysis	33
	3.6	Heat 7	Treatment Process	35
		3.6.1	Solution Heat Treatment	35
		3.6.2	Ageing Treatment	36
	3.7	Analy	sis	37
		3.7.1	LECO Glow Discharge Spectrometer (GDS)	37
		3.7.2	Microstructural Analysis	38
		3.7.3	Phase analysis by X-Ray Diffractometer (XRD)	
			and Energy Dispersive X-Ray Analysis (EDX)	39
		3.7.4	Microhardness Testing	40

4	RES	ULT AN	ND DISCUSSION	
	4.1	Introd	uction	42
	4.2	Micro	structural and Composition Analysis of NAB	
		Alloy		42
		4.2.1	Chemical Composition of Nickel	
			Aluminium Bronze (NAB) Alloy	43
		4.2.2	Optical Microscopy Analysis	44
	4.3	Comp	outer-Aided Cooling Curve Thermal Analysis	
		(CA-C	CCTA)	46
		4.3.1	Comparison Analysis of Different Cooling	
			Rate	46
			4.3.1.1 Solidification of NAB alloy in	
			ceramic mould	46
			4.3.1.2 Solidification of NAB alloy in	
			Permanent Mould	51
	4.4	Effect	s of Different Cooling Rates	55
		4.4.1	Effect of Cooling Rate on Mechanical	
			Property of As-Cast NAB Alloy	55
		4.4.2	Effect of Cooling Rate on Phase Formation	
			of As cast NAB Alloy	56
	4.5	Micro	structural Characterization of Heat Treated	
		Samp	les.	57
		4.5.1	Effect of Ageing Treatment on Sample	
			Microstructure	58
	4.6	Mech	anical Property of Aged Samples of NAB	
		Alloy		66
		4.6.1	Comparison Analysis of Ageing Treatment	
			on Property on samples from different	
			Cooling Rate (During Solidification)	68
5	CON	CLUSI	ON AND RECOMMENDATIONS	
	5.1	Concl	usions	70
	5.2	Recor	nmendations for Future Work	71

LIST OF REFERENCES	72
APPENDICES A-L	76

LIST OF TABLES

TABLE NO	TITLE	PAGE
2.1	The average chemical composition (wt. %) of constituent	
	phases of the NAB alloy [17].	9
2.2	The results of EDS analysis of Figure 2.4 (wt. %) [18]	11
2.3	The crystal structure and typical chemical composition of	
	the κ-phases in as-cast NAB alloy [21]	13
2.4	Comparison between literatures on solution-treatment	
	temperature and quenching method	25
2.5	Comparison between literatures on ageing temperature	
	and cooling method	26
3.1	As-received NAB Alloy composition in compare to	
	standard C95520 Alloy (%.wt)	27
3.2	Summary of heat treatment applied temperature and	
	holding time and cooling methods of as cast nickel	
	aluminium bronze (NAB) alloy for sand mould samples	36
3.3	Summary of heat treatment applied temperature and holding	
	time and cooling methods of as cast nickel-aluminium	
	bronze (NAB) alloy for permanent mould samples	37
4.1	As-cast NAB Alloy (ceramic mould) composition in compare	
	to standard C95520 Alloy (wt. %)	43
4.2	As cast NAB Alloy (permanent mould) composition in	
	compare to standard C95520 Alloy (wt. %)	43
4.3	Heat-treated NAB Alloy (ceramic mould) composition in	
	compare to standard C95520 Alloy (wt. %)	44
4.4	Heat-treated NAB Alloy (permanent mould) composition	

		xii
in	compare to standard C95520 Alloy (wt. %)	44
4.5	The results of EDX analysis of Figure 4.6 (wt. %)	51
4.6	The results of EDX analysis of Figure 4.12 (wt. %)	54
4.7	Comparison between both cooling rate effects on	
	Microhardness	56
4.8	The results of EDX analysis of Figure 4.15 for ceramic	
	mould sample (wt.%)	59
4.9	The results of EDX analysis of Figure 4.17 for ceramic	
	mould sample (wt. %)	61
4.10	The results of EDX analysis of Figure 4.20 for permanent	
	mould sample	62
4.11	The results of EDX analysis of Figure 4.22 for permanent	
	mould sample (wt. %)	64

LIST OF FIGURES

FIGURE NO	TITLE	
2.1	Vertical Section of the Cu-A1-5Ni-5Fe Equilibrium	
	Diagram [12]	6
2.2	Schematic representation of the distribution of phases in	
	cast NAB [12].	7
2.3	BSE-SEM image of the investigated NAB alloy, etched in	
	10% FeCl ₃ as constitutive phases are indicated [17]	9
2.4	(a) Alloy C95200 (b) alloy C95300; solution treated 30	
	min at 900 °C, water quenched, and ageing 2 hours at	
	350 °C, and water quenched [18].	10
2.5	Optical microscopy image of a fracture surface profile of a	
	tensile specimen show evidence of partial dissolution of	
	lamellar $\alpha+\kappa_{III}$ and transformation products of retained- β	
	phase [14]	12
2.6	Optical microscope image of the distribution of phases in	
	cast NAB [20].	13
2.7	The cooling, first and second derivative curves of the Bi-	
	containing alloy showing the characteristics parameters [13]	15
2.8	Cooling curve, first derivative and second derivative curves	
	of ADC12 alloy indicate the phase reaction and pouring	
	temperature, T_P and liquidus temperature, T_L [18]	16
2.9	The time-temperature curve recorded during the continuous	
	cooling of NAB alloy specimens from 1010 °C [21]	17
2.10	Hardness of the Aluminum Bronze Samples Plotted as a	
	function of the duration of solutionizing and ageing	
	treatments [8]	21

2.11	Variation of Vickers hardness of the aged and non-aged	
	C95200 and C95300 alloys with aging temperature [18]	22
2.12	Brinell hardness with variation of ageing temperature [27]	23
2.13	Cu-Al-Fe-Ni alloy's microstructure (a) as cast, (b) aging 120	
	min at 450 °C [27]	24
3.1	Overall experimental procedure flowchart	28
3.2	(a) Permanent Mould (b) Ceramic Mould	29
3.3	The fine stucco as mould finish	30
3.4	(a) The binder. (b) The pattern dipped into the mix slurry	
	made of colloidal silica, binder, and water	30
3.5	The setup of the melting and pouring of molten NAB alloy	32
3.6	Electrical Furnace for melting	32
3.7	NAB alloy sample	34
3.8	(a) Sample grinding machine and (b) polishing machine	34
3.9	Temperature against time diagram for heat treatment of both	
	moulds specimen	35
3.10	The LECO Glow Discharge Spectrometer (GDS) Machine	38
3.11	(a) Optical Microscope (OM) and (b) Phillips XL40 Scanning	
	Electron Microscope (SEM)	39
3.12	X-Ray Diffractometer	40
3.13	Shimadzu Microhardness (Vickers) Testing Machine	41
4.1	As-cast microstructure of NAB alloy solidified in ceramic	
	mould (200x)	45
4.2	As-cast microstructure of NAB alloy solidified in permanent	
	mould (200x)	45
4.3	Cooling curve recorded for the ceramic mould (slow cooling rate)	48
4.4	Cooling and first derivative for the ceramic mould (slow cooling	
	rate)	48
4.5	As-cast microstructure of NAB alloy solidified in ceramic	
	mould (1000x)	49
4.6	SEM and EDX analysis of NAB Bronze alloy solidified in	
	ceramic mould	50
4.7	EDX spectrum analysis of NAB Bronze alloy solidified in	
	ceramic mould	50

4.8	Elemental mapping analysis of NAB Bronze alloy solidified in	
	ceramic mould	51
4.9	Cooling curve recorded for the permanent mould (fast cooling	
	rate)	52
4.10	Cooling and first derivative for the permanent mould (fast	
	cooling rate)	53
4.11	As-cast microstructure of NAB alloy solidified in permanent	
	mould	53
4.12	EDX analysis of NAB alloy solidified in permanent Mould	54
4.13	Elemental mapping analysis of NAB Bronze alloy solidified	
	in permanent mould	55
4.14	Comparison of XRD result for both as cast samples	57
4.15	Microstructure of NAB alloy solidified in ceramic mould aged	
	at temperature of 350°C (one hour).	59
4.16	EDX spectrum analysis of α -phase in aged sample for 350 $^{\circ}\text{C}$	
	for one hour	59
4.17	Microstructure of NAB alloy solidified in ceramic mould	
	aged at temperature of 350°C (2 hours).	60
4.18	Microstructure of NAB alloy solidified in ceramic mould aged	
	at temperature of 350°C (3 hours).	61
4.19	Microstructure of NAB alloy solidified in ceramic mould aged	
	at temperature of 400°C (3 hours).	61
4.20	Microstructure of NAB alloy solidified in permanent mould aged	
	at temperature of 350°C (one hour).	62
4.21	Microstructure of NAB alloy solidified in permanent mould aged	
	at temperature of 350°C (2 hours).	63
4.22	Microstructure of NAB alloy solidified in permanent mould aged	
	at temperature of 350°C (3 hours).	64
4.23	Microstructure of NAB alloy solidified in permanent mould aged	
	at temperature of 400°C (3 hours).	65
4.24	Comparison of XRD result for aged sample at 300 °C and	
	400 °C for 3 hours	66
4.25	Hardness value of as cast and after heat treated (ceramic mould)	67
4.26	Hardness value of as cast and after heat treated (permanent	

		xvi
	mould)	67
4.28	Comparison of hardness between both cooling rate samples	69

LIST OF ABBREVIATION

NAB Nickel Aluminium Bronze

XRD X-Ray Diffractometer

EDX Energy Dispersive X-ray Analysis

SEM Scanning Electron Microscope

GDS Glow Discharge Spectrometer

OM Optical Microscopy

CA-CCTA Computer-Aided Cooling Curve Thermal Analysis

FCC Face-centered cubic

BCC Body-centered cubic

Fe Iron

Cu Copper

Al Aluminium

Si Silicon

Ni Nickel

Mn Managanese

xviii

LIST OF SYMBOLS

B - Beta

A - Alpha

κ - Kappa

γ - Gamma

μm - Micrometer (micron)

° C - Degree Celsius

T - Temperature

T - Time

Hv - Microhardness (Vickers)

> - Greater than

LIST OF APPENDICES

APPENDICES	TITLE	PAGE
A	SEM-EDX Mapping result for as cast sample	76
	(ceramic mould)	
В	SEM-EDX Mapping result for as cast sample	77
	(permanent mould)	
C	SEM-EDX Mapping result for Aged 350 °C 1 hr	77
	sample (ceramic mould)	
D	SEM-EDX Mapping result for Aged 350 °C 2 hrs	
	(ceramic mould)	78
E	SEM-EDX Mapping result for Aged 350 °C 1 hr	
	sample (permanent mould)	78
F	SEM-EDX Mapping result for Aged 350 °C 2 hrs	
	sample (permanent mould)	79
G	XRD result for as cast sample (ceramic mould)	80
Н	XRD result for as cast sample (permanent mould)	80
I	XRD result for Aged 350°C 3 hrs (ceramic	81
	mould)	
J	XRD result for Aged 350°C 3 hrs (permanent	81
	mould)	
K	XRD result for Aged 400°C 3 hrs (ceramic	82
	mould)	
L	XRD result for Aged 400°C 3 hrs (permanent	82
	mould)	

CHAPTER 1

INTRODUCTION

1.1 Background

The phase transformation during solidification of cast Nickel-Aluminium Bronze (NAB) alloy can be revealed by using computer-aided cooling curve thermal analysis (CA-CCTA). The CA-CCTA method of analysis is more preferred since it is easier to use as well as low cost, faster, and simple. Moreover, the most important factor is its suitability for commercial applications in comparison with other thermal analysis techniques. Besides, it is suitable for investigating the non-equilibrium solidification for various industrial alloys [1, 2].

Currently, the usage of computer-aided cooling curve thermal analysis (CA-CCTA) is not being used extensively in determining the phase transformation during solidification of NAB alloys which important to predict and control the rate of cooling and produced better product especially in metal casting industries [3]. CA-CCTA technique also been used for other alloy in order to obtained the desired microstructure and prediction of the phases transformed in solidification which lead to improvement of better mechanical properties of the alloys [4, 5].

By applying heat treatment to the as-cast NAB alloy, it can significantly further improve its mechanical properties [6]. Consequently, a combination of heat treatment and micro-hardness testing with detailed microstructural analysis of samples before and after heat treatment will be conducted.

1.2 Objectives of the Study

This project is intended to study on the relationship of the microstructure of Nickel-Aluminium Bronze (NAB) alloy solidified at different cooling rate with the use of different mould types and subsequent heat treatment by:

- i. Evaluation on the effect of cooling rate on microstructure
- ii. To establish the relationship between microstructure and the hardness.

1.3 Problems Statement of the Research

Microstructures of the NAB alloy can be varied by different cooling rate during casting as well as after heat treatment. Then, those variations in microstructures are expected to affect the mechanical property of the NAB alloy. Therefore, by applying good prediction method on the phase development and transformation during solidification of the alloy can be useful in order to attain the desire microstructure through controlling the cooling rate.

The heat treatment process will improve the mechanical property but also it may provide poor result and later reduce the alloy performance in service. Therefore, selection of the correct heat treatment process is vital in order to have the NAB alloy with better mechanical properties.

1.4 Scope of the Study

- i. To prepare casting of Nickel-Aluminium Bronze by using the electrical induction furnace and let to solidify by ceramic and permanent mould.
- ii. To apply the computer-aided cooling curve thermal analysis (CA-CCTA) during solidification of the NAB alloy.

- iii. To conduct heat treatment processes on the material; solution treatment at 850 °C (2 hours) followed by ageing at 350 °C 400 °C (1 3 hours)
- iv. To conduct hardness test on material before and after heat treatment.
- v. To study and analyse the microstructural of the Nickel-Aluminium Bronze by using optical microscope (OM), SEM and EDX as well as XRD.

REFERENCES

- [1] S. Farahany, N.Azmah, R.Kamal, A.Ourdjini (2013). "Thermal Analysis and Microscopic Characterization of the Al-20%Mg2si In-Situ Composite" The 21st Scientific Conference of the Microscopy Society of Malaysia.
- [2] S. Farahany, A. Ourdjini, M.H. Idris, S.G. Shabestari (2013) "Evaluation of the effect of Bi, Sb, Sr and cooling condition on eutectic phases in an Al–Si–Cu alloy (ADC12) by in situ thermal analysis" Thermochimica Acta, Vol. 559 pp. 59–68.
- [3] S. M. Jigajinni, K. Venkateswarlu and S. A. Kori (2011). "Computer aided cooling curve analysis for Al-5Si and Al-11Si alloys". International Journal of Engineering, Science, and Technology Vol. 3, No. 6, pp. 257-272.
- [4] S.G. Shabestari, M. Malekan. (2010) "Assessment of the effect of grain refinement on the solidification characteristics of 319 aluminum alloy using thermal analysis" Journal of Alloys and Compounds vol.492 pp.134–142.
- [5] S. Farahany, A. Ourdjini, T.A.A Bakar, M. H. Idris.(2013) "A new approach to assess the effects of Sr and Bi interaction in ADC12 Al–Si die casting alloy" Thermochimica Acta vol.575 pp. 179–187.
- [6] M. M. Shirazabad, A. Karimi and A. Babakhani (2012) "The Effects of Aging Treatment Parameters on Microstructure and Hardness of Aluminium- Bronze Alloy". 3rd International on Material Heat Treatment.

- [7] A. Al-Hashem, W. Riad (2002) "The role of microstructure of nickel—aluminium—bronze alloy on its cavitation corrosion behaviour in natural seawater". Materials Characterization vol.48, pp.37–41.
- [8] A.H Khan and P.K Singh (2013.) "Influence of Heat Treatment on Microstructure and Mechanical Properties of Aluminum Bronze" International Journal of Metallurgical & Materials Science and Engineering (IJMMSE), ISSN 2278-2516, Vol. 3, Issue 1, pp 57-66.
- [9] J.A. Wharton et al (2005). "The corrosion of nickel-aluminium bronze in seawater" Corrosion Science 47, pp. 3336–3367. 2005
- [10] M.S Rizi, A.H Kokabi (2014). "Microstructure evolution and microhardness of friction stir welded cast aluminum bronze". Journal of Materials Processing Technology, vol. 214, pp.1524–1529
- [11] R.C. Strang, "Nickel-Aluminium Bronze for Seawater: Flattered by Comparison" Shipham Valves.
- [12] F. Hasan, A. Jahanafrooz, G.W. Lorimer, and N. Ridley (1982) "The Morphology, Crystallography, and Chemistry of Phases in As-Cast Nickel-Aluminum Bronze" American Society For Metals And The Metallurgical Society of AIME Volume 13A, pp.1337
- [13] B. Thossatheppitak et al (2013). "Mechanical Properties at High Temperatures and Microstructures of a Nickel Aluminum Bronze Alloy" Advanced Materials Research Vol. 683, pp 82-89.
- [14] M.D. Fuller, S. Swaminathan, A.P. Zhilyaev, T.R. McNelley (2007) "Microstructural transformations and mechanical properties of cast NiAl-bronze: Effects of fusion welding and friction stir processing" Materials Science and Engineering A 463, pp. 128–137.

- [15] E.A. Nelson (2009). "Microstructural Effects of Multiple Passes during Friction Stir Processing Of Nickel Aluminum Bronze" Postgraduate Thesis, Naval Postgraduate School, Monterey, CA
- [16] M. Moradlou, N. Arab, R. Emadi3, M. Meratian (2011). "Effect of Magnesium and Nickel on the Wear and Mechanical Properties of Casting Bronzes" Journal of American Science,pp.717-722.
- [17] D. Nakhaie, A. Davoodi, A. Imani (2014). "The role of constituent phases on corrosion initiation of NiAl bronze in acidic media studied by SEM–EDS, AFM and SKPFM" Corrosion Science vol. 80, pp. 104–110
- [18] M. Yasar, Y. Altunpak (2009) "The effect of aging heat treatment on the sliding wear behaviour of Cu–Al–Fe alloys". Materials and Design Vol.30, pp.878–884.
- [19] B. Sabbaghzadeh et al (2014). "Corrosion evaluation of multi-pass welded nickel-aluminum bronze alloy in 3.5% sodium chloride solution: A restorative application of gas tungsten arc welding process". Materials and Design, vol. 58, pp. 346–356.
- [20] E.A Culpan, G. Rose (1978). "Microstructural characterization of cast nickel aluminium bronze" Journal of Materials Science Vol. 13, Issue 8, pp 1647-1657.
- [21] A. Jahanafrooz et al (1983). "Microstructural Development in Complex Nickel-Aluminum Bronzes" Metallurgical Transactions A, Vol. 14a
- [22] S. Farahany, A. Ourdjini, M. H. Idris, S. G. Shabestari (2013). "Computer-aided cooling curve thermal analysis of near eutectic Al–Si–Cu–Fe alloy Effect of silicon modifier/refiner and solidification conditions on the nucleation and growth of dendrites" J Therm Anal Calorim,

- [23] W.D Callister Jr., D.G. Rethwisch., (1940). "Materials Science and Engineering: An Introduction". 8th Edition, ISBN 978-0-470-41997-7, pp 422-442
- [24] J. Anantapong et al (2014). "Effect of hot working on microstructure evolution of as-cast Nickel Aluminum Bronze alloy" Materials and Design vol. 60 pp.233–243
- [25] B.A. Dewhirst (2005). "Optimization of the Heat Treatment of Semi Solid Processed A356 Aluminum Alloy" Masters Thesis, Worcester Polytechnic Institute.
- [26] R.P. Chen et al (2007) "Effect of heat treatment on microstructure and properties of hot-extruded nickel-aluminum bronze" Trans. Nonferrous Met. Soc .China 17 pp.1254-1258
- [27] G.Mi, a, J.Z. Zhang, and H.Y. Wang (2011). "The Effect of Aging Heat Treatment on the Mechanical Properties of Cu-Al-Fe-(x) Alloys" Key Engineering Materials Vols. 467-469, pp 257-262.
- [28] A.V.Takaloo, M.R.Daroonparvar, M.M.Atabaki, K.Mokhtar (2011). "Corrosion Behavior of Heat Treated Nickel-Aluminum Bronze Alloy in Artificial Seawater" Materials Sciences and Applications, Vol. 2 pp. 1542- 1555.
- [29] L. E. Collins and V. Mitrovic-Scepanovic (1988). "Improved Corrosion Resistance of Rapidly Solidified Fe-AI Bronzes" Materials Science and Engineering, vol. 99 pp.493-96
- [30] Y.S. Sun, G.W. Lorimer, and N. Ridley (1990). "Microstructure and Its Development in Cu-AI-Ni Alloys" Metallurgical Transactions A, vol. 21A, pp.575-588