

COMPARISON OF FLUIDISED BED AND SPOUTED BED
FOR THE COMBUSTION OF RICE HUSK

LOOI YAT SEONG

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Dedicated to my respected parents

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ABSTRACT

The purpose of this study was to evaluate the characteristics and performance of fluidised and spouted bed for the combustion of rice husk. With the annual generation rate of rice husk of approximately 0.4 million metric tones in Malaysia, disposal of the husk was a problem. The calorific value of the husk and the amorphousness of the ash make combustion the better option due to the vast reduction in volume of rice husk and control in combustion temperature. Numerous combustion systems are currently available but fluidised and spouted beds have numerous advantages over the other systems. Hydrodynamic studies show that sand size range of 0.30 mm to 0.50 mm and 0.50 mm to 0.71 mm are suitable as the bed material for fluidised and spouted bed respectively. Combustion studies were conducted in a 90 mm OD combustor fitted with a 60° conical base using commercial sand grade 20/30 and 30/60. Autogenous combustion could be achieved at air factor 0.7 to 1.5 (static bed height = $0.5D_c$) in a fluidised bed and at air factor 1.0 to 1.5 (static bed height = $1.5D_c$) for a spouted bed fitted with a draft tube (SBDT). However, the study showed that combustion could not be achieved with the conventional spouted bed. Fluidising velocities of $4.5U_{mf}$ to $6U_{mf}$ and spouting velocities of $1.75U_{ms}$ to $2.85U_{ms}$ were optimised for autogenous combustion. Higher bed temperature was observed for fluidised bed combustion of rice husk. XRD analysis further showed that fluidised bed fly ash was amorphous. Performance evaluation revealed that fluidised bed was a better option than spouted bed. Autogenous combustion and amorphous ash could also be achieved when combustion was conducted in a large-scale fluidised bed (210 mm ID, static bed height = $0.5D_c$, sand 30/60). This study demonstrated that fluidised bed was suited for the combustion of rice husk compared to the spouted bed.

ABSTRAK

Matlamat penyelidikan ini adalah untuk menilai ciri-ciri dan prestasi lapisan terbendalir dan lapisan terpancut untuk pembakaran sekam padi. Dengan kadar penghasilan sekam padi sebanyak 0.4 juta tan metrik setahun, pembuangan sekam padi merupakan satu masalah. Dengan nilai kalori sekam padi dan abu yang bersifat amorfus, pembakaran adalah pilihan yang baik kerana pengurangan isipadu yang ketara dan kawalan suhu pembakaran. Walaupun terdapat banyak sistem pembakaran, lapisan terbendalir dan lapisan terpancut memiliki beberapa kelebihan. Kajian hidrodinamik menunjukkan pasir bersaiz 0.30 mm ke 0.50 mm dan 0.50 mm ke 0.71 mm sesuai menjadi bahan nadir lapisan terbendalir dan lapisan terpancut. Pembakaran dilakukan dengan turus 90 mm yang mempunyai dasar kon bersudut 60° dan pasir komersial gred 20/30 dan 30/60 merupakan bahan nadir. Pembakaran sekam padi yang stabil dapat dilakukan pada faktor udara 0.7 hingga 1.5 (ketinggian bahan nadir = $0.5D_c$) untuk lapisan terbendalir dan pada faktor udara 1.0 hingga 1.5 untuk lapisan terpancut yang dipasang dengan “*draft tube*”. Kajian ini menunjukkan pembakaran sekam padi tidak dapat dilakukan dengan lapisan terpancut konvensional. Kelajuan terbendalir $4.5U_{mf}$ hingga $6U_{mf}$ dan kelajuan terpancut $1.75U_{ms}$ hingga $2.85U_{ms}$ sesuai untuk pembakaran sekam padi. Suhu pembakaran yang tinggi diperolehi untuk lapisan terbendalir. Analisis XRD menunjukkan abu sekam padi dari pembakaran dengan lapisan terbendalir berciri amorfus. Penilaian hasil kajian menunjukkan lapisan terbendalir adalah lebih baik dari lapisan terpancut. Pembakaran sekam padi dengan lapisan terbendalir skala-besar (210 mm OD, ketinggian lapisan nadir = $0.5D_c$, pasir komersial 30/60) juga memberi abu yang amorfus. Penyelidikan ini menunjukkan lapisan terbendalir adalah sesuai untuk pembakaran sekam padi berbanding dengan lapisan terpancut.

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LIST OF SYMBOLS

A	Surface reaction rate constant (87,100 kgm ⁻² s atm)
A	Frequency factor
A_o	Theoretical air volume (L)
Ar	Archimedes number = $\frac{d_p^3 \rho_g (\rho_s - \rho_g) g}{\mu^2}$, dimensionless
A_w	Area of the wall surface submerged in the annular bed, (m ²)
C_D	Drag coefficient = $\frac{4d_v g (\rho_s - \rho_f)}{3\rho_f U_m^2}$
CI	Combustion intensity (kg hr ⁻¹ m ⁻²)
C_o	Oxygen concentration inlet of the bed (g mole cm ⁻³)
C_R	Oxygen concentration at particle surface (g mole cm ⁻³)
C_b	Oxygen concentration in the bed (g mole cm ⁻³)
c_p	Oxygen concentration in the fluidising air within the bed (kmol m ⁻³)
d	Particle diameter, (m)
daf	Dry ash free
d_B	Density of the bed; cylinder bore, (kgm ⁻³)
d_i	Initial particle of coal or diameter of solid fuel of char particle (m)
d_p	Diameter of inert particle, (m)
d_p^*	Dimensionless particle size
d_{pc}	Diameter of particle collected with 50% efficiency, (m)
D	Body diameter of cyclone; Nominal screw diameter, (m)
D_d	Dust outlet of cyclone, (m)
D_e	Outlet diameter of cyclone, (m)

D_c	Column diameter, (m)
D_G	Binary molecular diffusion coefficient of oxygen in the air (m^2s^{-1})
D_i	Diameter of gas inlet orifice, (m)
D_o	Diameter of the orifice, (m)
D_g	Diffusivity of oxygen gas (cm^2s^{-1})
D_p	Diameter of carbon particle (mm)
E	Activation energy ($35,700 \text{ kcal mol}^{-1}$)
E	Activation energy of carbon
F_H	Main resistances as the material continue to progress
F_H	Mass flow rates of hydrogen
F_m	Horse power factor for screw conveyor
F_N	Resistances due to the operating at no load
F_O	Mass flow rates of oxygen
F_{St}	Resistances due to the inclination
FR	Feed rate ($gmin^{-1}$)
g	Acceleration of gravity, (9.81 ms^{-2})
H	Inlet height, (m)
H_c	Height of conical section, (m)
ΔH	Enthalpy of thermal decomposition of a fuel into char and volatile matter
H_m	Maximum spoutable bed depth, (m)
I_M	Capacity of the screw conveyor, ton hour^{-1}
k_c	Reaction rate constant (s^{-1})
$k_{ov, i}$	Frequency factor
L	Length (m)
L_B	Body length of cyclone, (m)
L_C	Cone length of cyclone, (m)
m_{ov}	Total volatile content (kg)
m_v	Volatile burned (kg)
m_{oc}	Total char content (kg)
m_c	Char burned (kg)

m_c	Mass of the unburnt carbon, (kg)
	Mass flow rate for feeder, (kg hour^{-1})
N	Number of particles
n	Number of samples
Nu	Nusselt number = $\left(\frac{h_w d_p}{\lambda_f}\right)$
ΔP_b	Pressure drop across the bed, (Nm^{-2})
ΔP_{\max}	Peak pressure drop, prior to spouting, (Nm^{-2})
P_t	Fractional penetration
Q	Volumetric flow rate of the air supplied (liter/min)
R	Ideal gas characteristics, Universal gas constant ($1.986 \text{ kcal kmol}^{-1} \text{ K}^{-1}$)
r	Radius of solid fuel (m)
$Re_{p,mf}$	Reynolds number, (dimensionless)
S	Outlet length of cyclone, (m)
Sc	Schmidt number = $\mu_f / \rho_f D_g$, (dimensionless)
Sh	Sherwood number = $\frac{k_g d_c}{D_g}$, (dimensionless)
Sh_b	Mean Sherwood number in spouted bed
Sh_i	Intrinsic Sherwood number
S_p	Surface area of particle, (m^2)
T	Temperature, (K or $^{\circ}\text{C}$)
t_b	Burn-out time of a single char particle (s)
T_m	Temperature of the air flow meter, (K)
T_p	Solids temperature in the annulus
T_s	Absolute temperature of the carbon surface
t_d	Time for complete devolatilisation (s)
T_{bed}, T_d	Temperature of the bed and devolatilisation of solid fuel ($^{\circ}\text{C}$)
T_d, T_f	Temperature of the furnace and particle ($^{\circ}\text{C}$)
T_c	Combustion temperature ($^{\circ}\text{C}$)
T_p	Temperature of the particle ($^{\circ}\text{C}$)
u^*	Dimensionless gas velocity

U	Fluidising gas velocity, (ms^{-1})
U_{mf}	Minimum fluidising velocity-superficial, (ms^{-1})
U_{ms}	Minimum spouting velocity-superficial, (ms^{-1})
U_t	Terminal velocity $U_t = \left(\frac{4d\rho_p g}{3C_D \rho} \right)^{1/2}$ (ms^{-1})
V_i	Amount of volatile
V^*	From V_i when t approaches infinity
V_p	Volume of particle, (ms^{-1})
W	Inlet width of cyclone, (m)
X	Weight of sample left after thermal treatment (gm)
Y	Weight of sample used (gm)

Greek Letters

α, β	Molar flow rate of air supplied in the dry flue gas, (mol/min)
γ	Cone angle (radian)
λ	Particle shape factor
ϵ, ϵ_0	Bed voidage, Mean voidage around the burning char particle
ϵ_{mf}	Bed voidage at minimum fluidization
π	Constant, 3.142
ρ_b	Bulk density of the bed, (kgm^{-3})
ρ_g	Density of gas, (kgm^{-3})
ρ_f	Fluid density, (kgm^{-3})
ρ_m	Density of solid fuel (kgm^{-3})
ρ_i, ρ_c	Density of initial solid fuel and char (kgm^{-3})
ρ_s, ρ_p	Particle density, (kgm^{-3})

ϕ_s	Particle sphericity
θ	Effective number of turns made in traversing the cyclone, $\left[\frac{\pi}{H} (2L_b + L_c) \right]$
μ, μ_f	Fluid viscosity, ($\text{kgm}^{-1}\text{s}^{-1}$)
μ_g	Viscosity of fluidising gas ($\text{kgm}^{-1}\text{s}^{-1}$)
η_{CE}	Combustion efficiency, (%)
κ	Thermal conductivity ($\text{Wm}^{-1}\text{K}^{-1}$)
τ	Thermal diffusivity ($\text{K}\rho_i^{-1}\text{C}_p^{-1}$)
Ω	Air factor

Abbreviation

AR	Air factor
CSA	Cross sectional surface area (m^2)
CV	Calorific value, (kJkg^{-1})
CV _c	Calorific value of carbon, ($18.5 \text{ kJkg carbon}^{-1}$).
EA	Excess air
FB	Fluidised bed
HCV _f	Higher caloric value of the solid fuel (rice husk)
HHV	Higher heating value
ID	Internal diameter
LHV	Lower heating value
LPG	Liquefied petroleum gases
LPM	Liters per minute
OD	Outer diameter
RH	Rice husk

RHA	Rice husk ash
RT	Room temperature
SB	Spouted bed
SBDT	Spouted bed draft tube
SFBC	Spout-fluidised bed combustion
TGA	Thermogravimetric analysis
XRD	X-Ray Diffraction

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CHAPTER 1

INTRODUCTION

1.1 Disposal of Rice Husk

With the country's economy mostly contributed by the agriculture sector, Malaysia will have an abundance of biomass for disposal (Table 1-1). An example of this biomass is rice husk. Rice husk weights approximately 20 % of the paddy weight (Natarajan *et al.*, 1998a). With the production of paddy in Malaysia of around 2.2 million metric tonnes (Paddy Statistics of Malaysia, 1996), the generated husk quantity is about 400,000 metric tonnes. Due to the vast volume of rice husk, disposal is a problem. As it has a low bulk density and high ash content, handling of the husk is also a problem (Jain *et al.*, 1995). The physical form of rice husk which is seldom homogenous caused it not to be free flowing.

Due to the large quantities of rice husk, it is also an environmental problem if it is not fully utilized (Lu and Woo, 1986) or not properly disposed (Yeoh and Ong, 1989). Currently, Beras Nasional (BERNAS, 2003) is looking into ways of disposing the rice husk such as landfilling, control burning for power generation, pulverized and reclamation of rice husk in other products. Landfilling however created environmental problems besides the shortage of suitable sites. The

pulverization plant is costly for BERNAS with each of the plant having an average cost of about RM250, 000.00. The reason for pulverization is to increase the density of the husk and making it readily available for marketing. Reclamation of rice husk by BERNAS such as the production of fertilizer, composite plastic and the manufacturing of fiber reinforce composite from black rice husk ash is not feasible due to the low market demand for these products.

The huge volume of rice husk also is also a management problem. This is due to open burning of the husks and the straws which would emit thick smoke and thus reduces the visibility range. As shown in Appendix A-1, the accident at Bukit Ko'bah was due to such practice.

Table 1-1: The planted area of main crops in Malaysia (Department of Statistics, 1996).

Crop	Biomass	Land area (hectares)	Production per year (tonnes)
Oil palm	Shell, fiber, empty fruit branches	2.69×10^6	* 8.35×10^6
Coconut	Husk, shell, copra cake	0.23×10^6	\$ 26.91×10^3
Rubber	Wood	1.64×10^6	1.08×10^6
Pineapple	Bran	7.1×10^3	121.91×10^3
Paddy	Husk	0.68×10^6	# 1.44×10^6

* As crude palm oil

\$ As coconut oil

As rice

However, with proper management of rice husk, amorphous silica could be obtained. In addition, the calorific value of rice husk makes it a potential renewable energy source. Further usage of amorphous silica, methods of obtaining amorphous

and the potential of rice husk as a replenish energy source are mentioned in Section 2.1.1 and Section 2.2.2.

1.2 Combustion of Rice Husk

With the vast volume of rice husk, disposal options that are currently available besides thermal treatment has many disadvantages such as time consuming, difficulty to find suitable sites for landfill and inability for fast volume reduction. In addition, if land filling is not carried out properly, it can be a major source of air, soil and water pollution for many years. Briquetting of rice husk is also not feasible due to the nature of the rice husk itself and it is costly to pulverize the husks. Since rice husk has low bulk density, transportation is a problem due to huge volume. Thus, combustion will be a good option as the reduction of volume can be done promptly and on the site in order to obtain rice husk ash residue that is useful for other commercial applications besides the production of heat energy for other on site applications such as power generation and drying processes.

1.2.1 Advantages of Combustion

The advantages of incineration are as follows (Hoi, 1996): -

- i) Hazardous components of the waste and toxic organic can be destroyed
- ii) Great volume reduction (up to 90 % from the original size) can be achieved and immediately disposal of waste can be carried out
- iii) Waste can be incinerated on site without much of transportation

- iv) The discharge of air can be controlled
- v) The obtained ash residue is sterile and non-hazardous
- vi) The production of heat energy can be used for other applications

There are many existing combustion technologies for rice husk. However, it is important to evaluate each technology before deciding on the technology to be used.

1.2.2 Existing Combustion Technologies for Rice Husk

With the increasing of waste worldwide and in Malaysia coupled with the publics' concern on the quality of the environment, new technologies are needed for volume reduction of waste. Numerous incineration technologies are available for the disposal of rice husk. The available technologies for the treatment of rice husk are as below:-

- a) Rotary kiln
- b) Cyclonic combustor
- c) Plasma technology
- d) Grate-fired furnace
- e) Furnace
- f) Fluidised bed combustors

The disadvantages of the current technologies besides the fluidised bed combustors are mentioned in Section 2.1. The types of fluidised bed available are mentioned in Section 2.1.1.

1.2.3 Advantages of Fluidised and Spouted Bed

With the advancement of fluidisation technology, the fluidised and spouted bed would have the potential to be used for combustion of rice husk. Both these system do offer some advantages. Fluidised bed combustors are suitable for recovery of energy from biomass and have successfully burned a wide variety of wastes like agricultural wastes, sludges, wood wastes, and hazardous wastes.

Spouted bed had also been shown to be able to combust solid, liquid and gases fuels (Khosnoodi and Weinberg, 1978; Arbib and Levy, 1982; Lim *et al.*, 1988; Khosnoodi and Rozana, 1994). Therefore, spouted bed also has the potential for the combustion of rice husk. The advantages of spouted bed (SBC) and fluidised bed are shown in Table 1-2 (Zhao *et al.*, 1987; Ho *et al.*, 1988; Howard, 1989b; Affendi *et al.*, 1991; Olazar *et al.*, 1994; Werther *et al.*, 2000).

1.3 Purpose of the Study

In general, the purpose of this research is to evaluate between fluidised and spouted bed which system has the potential to combust rice husk within a short period besides obtaining amorphous ash. Preliminarily, hydrodynamic studies would be performed to determine the optimum operating parameter for the combustion of rice husk.

Table 1-2: Advantages of fluidised and spouted bed technology.

Features	Fluidised Bed	Spouted Bed
1) Simplicity in design	No moving parts.	No distributor. Could be used in scarcely located paddy schemes. Economically to construct due to lower pressure drop.
2) Versatile Operation	All types of fuel could be burned. Fluctuation in the feed rate is easily tolerated.	Has the ability to burn lower quality fuel and fuel with high ash content.
3) Combustion efficiency	Up to 99 %. 96 % of sludge waste can be combusted within the first minute of incineration	Above 90 %.
4) Stable Continuous Combustion	Large heat capacity of the sand helps to maintain the operation.	Large heat capacity of the sand helps to maintain the operation.
5) Uniform temperature	Turbulent mixing of solids prevents hot spots.	No hot spots and thus materials of thermal sensitive could be treated.
6) Low Air Pollution Emission	Due to low combustion temperature (below 850°C), NO _x formation and evaporation rate of heavy metals could be minimised. The highly mixed oxygen-rich environment is good for complete combustion.	Due to low combustion temperature (below 850°C), NO _x formation could be minimised.
7) High Heat-Transfer	Possible for energy recovery.	Possible for energy recovery.
8) Material Handling	Could be fed either with over-bed or under-bed feeding.	Could be fed either with over-bed or under-bed feeding.

1.4 Justification and Objectives of the Study

With the disposal problem of rice husk in rice producing countries such as Malaysia coupled with the potential of amorphous rice husk ash and energy recovery from rice husk, combustion of rice husk rather than direct disposal is a better option. Therefore, evaluation of combustion system for rice husk is important in order to provide a better option for vast volume reduction, energy recovery and obtaining amorphous silica. This could be achieved by studying the mixing pattern of the bed as bad mixing would give rise to incomplete combustion, causing detrimental effect to the environment besides giving low quality ash.

With the setbacks of other combustion systems, fluidised and spouted bed has the potential to be used for rice husk combustion besides these two systems had been successfully applied in the field of combustion of a variety of fuel. However, no evaluation study on these two systems had been carried out for combustion of rice husk. In addition, previous studies on combustion of rice husk with fluidised bed were also carried out in different geometric shape and did not present the details of the bed hydrodynamics, the effect of fluidising air and the characteristics of the obtained fly ash.

Therefore, the objectives of this study were:-

- i) To design and develop a laboratory-scale rig for fluidised and spouted bed studies. Initial hydrodynamic studies were conducted with the developed rig. Then, combustion studies of rice husk were performed on the same rig.
- ii) To evaluate between fluidised and spouted bed the system of choice for combustion of rice husk.
- iii) To conduct a trial run of the system of choice in a large-scale combustor.

1.5 The Scopes of the Study

The scopes of this study were presented. Initial determination of characteristics of the research materials (rice husk, rice husk ash and sand) were carried out to assist in the feeding of the husk and isolation of the ash. The chemical properties of rice husk were to assist in combustion studies.

This was followed by the development of the rig optimum design parameters of the laboratory-scale fluidised and spouted bed combustor system (column geometry and height, distributor design, cyclone design and feeding system).

Upon completion, hydrodynamic studies were performed to determine the operating bed height and the sand size to be used as the bed material for fluidised and spouted bed. Once this had been known, the determination of the optimum operating parameters for the combustion of rice husk in fluidised and spouted bed (such as fluidising/spouting number, combustion temperature profiles and air factors) were investigated. During the combustion studies, the collected fly ash would be analysed to determine on the combustion performance of the fluidised and spouted bed.

Upon the completion of the combustion studies, evaluation between fluidised and spouted bed were conducted to determine the system for the combustion of rice husk in a large-scale combustor. Once the system had been chosen, further verification on the system of choice was carried out in a large-scale combustor with pre-fixed operating parameters. The collected fly ash from the large-scale combustion would be analysed to determine any improvement on the combustion with a large-scale rig.

1.6 Outline of the Thesis

This thesis describes the research work to evaluate the system of choice for rice husk combustion between spouted bed and fluidised bed in term so overcoming the environmental problem besides obtaining amorphous ash. This study investigates the fundamental operating parameters of spouted bed and fluidised bed at a laboratory scale and applying the obtained results to a large-scale rig.

Chapter 1 described a brief introduction on the problem of rice husk as a waste in countries like Malaysia It also briefly describes the available thermal treatment technologies for rice husk. and its disadvantages. The purpose, the objectives, scope and an outline of the study are also mentioned.

Chapter 2 briefly describes the disadvantages of the available thermal treatment technologies for rice husk. The importance of rice husks as a source for amorphous ash and energy is also mentioned. The chapter also describes a review of the related theories of fluidisation in a bubbling fluidised bed and spouted bed. A review on the combustion of rice husk in spouted bed and fluidised bed is also mentioned. This chapter also covers the related theories on combustion of solids.

Chapter 3 described research design, the rig description of the laboratory scale and the large scale, the materials in the present study and the research methodology. The basis of design for the main components of the rig starting from the distributor plate, the cone, the column, the cyclone and the fuel feeding system are also described besides the method of start-up. The characteristics of the research materials (rice husk, rice husk ash and sand) were also described.

Chapter 4 presented the results on the hydrodynamics of spouted bed and fluidised bed for sieved sand to determine the sand size. The result on hydrodynamics of draft tube on the spouted bed with commercial sand is also mentioned. Results from hydrodynamic studies on commercial sand for fluidised bed were also disclosed.

Chapter 5 covered the combustion results for conventional spouted bed, effect of draft tube (SBDT) and fluidised bed. The effect of air supply, primary inlet velocity and the optimum operating spouted bed height are discussed. The quality of the obtained fly ash is also presented. Finally, an evaluation on the performance of fluidised and spouted bed is presented.

Chapter 6 disclosed combustion performance and the quality of the fly ash from a trial run on the selected system of choice (fluidised bed) for the combustion of rice husk in a large-scale 210 mm ID column.

Chapter 7 provided the conclusion on the overall studies and recommendations of the study.

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