IMPROVED EQUIVALENT CIRCUIT MODEL FOR HIGH CAPACITY LITHIUM FERRO PHOSPHATE BATTERY

LOW WEN YAO

A thesis submitted in fulfilment of the requirements for the award of the degree of Master of Engineering (Electrical)

Faculty of Electrical Engineering
Universiti Teknologi Malaysia

DECEMBER 2012

Specially dedicated to my beloved father, mother and friends for their encouragement and support

ACKNOWLEDGMENT

In preparing this thesis, I got touch with many researchers and academicians in the field of electrochemical and energy storage. They have contributed towards my understanding and thoughts. In particular, I would like to express my sincerest appreciation to my main Supervisor, Dr. Mohd Junaidi Abdul Aziz, for his keen effort and insightful comments throughout the accomplishment of this project. I am also very thankful to my co-supervisor, Dr. Ahmad Saudi Samosir, for encouragement and guidance. Without their continuous support and interest, this thesis would not have been the same as presented here.

I would like to express my deep gratitude to the Universiti Teknologi Malaysia (UTM) and the Ministry of Higher Education for funding my study. My appreciation is also extended to PROTON Holdings Berhad for establishing UTM-PROTON satellite research laboratories in UTM. Practical experience of electric vehicle development is priceless to me.

Last but not least, my heartfelt gratitude also extended to my family for their supports along the way.

ABSTRACT

Electric Vehicle (EV) gets the attention and interest of scientists due to its advantages of zero green house gaseous emissions and higher efficiency. Battery pack is utilised as energy storage element in EV. Strict handling on battery pack is important to ensure battery pack performs in safe and consistent manner under various load demand and driving state. Therefore, an efficient Battery Management System (BMS) which can perform State Of Charge (SOC) estimation, cell equalisation and temperature control, should be put as the primary concern. In this aspect, an accurate battery model is required to give high quality SOC estimation and battery management. Equivalent circuit model is widely used as the battery model since it can be easily connected to external circuit in a simulation platform. However, the existing battery models are generally built for low capacity battery and do not take into account on nonlinear capacity effect. In this thesis, equivalent circuit model for 18 Ah Lithium Ferro Phosphates (LiFePO₄) battery is developed. LiFePO₄ battery is a good energy storage element for EV since it has good thermal and chemical stabilities. The thesis studies the existing battery modelling technique and investigates the dynamic characteristics of 18 Ah LiFePO₄ battery. A new battery modelling approach with consideration of nonlinear capacity effect has also been proposed for high capacity LiFePO₄ battery. Moreover, a simplified methodology for battery modelling is proposed to improve existing battery model. Parameter extraction is discussed and the proposed battery model is validated from the experiment data. The comparison between experiment and simulation results shows that the proposed model is capable of predicting dynamic behaviours of the battery with minimum error.

ABSTRAK

Kenderaan elektrik (EV) menarik perhatian dan minat daripada saintis kerana ia tidak menpunyai masalah pelepasan gas rumah hijau dan ia menpunyai kecekapan yang tinggi. Pek bateri diguna sebagai elemen simpanan tenaga dalam EV. Pengendalian bateri pek adalah sangat penting untuk memastikan bateri pek berfungsi secara selamat dan konsisten dalam pelbagai permintaan beban dan keadaan memandu. Maka, sistem pengurusan bateri (BMS) yang cekap dalam penganggaran status caj (SOC), pengimbangan sel dan pengawalan suhu perlu dijadikan sebagai fokus utama. Dalam aspek ini, model bateri yang tepat amat diperlukan dalam penganggaran SOC dan pengurusan bateri. Model litar setara banyak digunakan sebagai model bateri kerana ia mudah disambungkan kepada litar luar dalam platform simulasi. Walau bagaimanapun, model bateri yang wujud biasanya dibina untuk bateri yang berkapasiti rendah atau tidak mengambil kira kesan kapasiti tak linear. Dalam tesis ini, model litar setara yang sesuai bagi 18 Ah bateri Litium Ferro Fosfat (LiFePO₄) dibangunkan. Bateri LiFePO₄ merupakan alat penyimpanan tenaga yang sesuai untuk EV kerana ia mempunyai ciriciri yang stabil dari segi kimia dan terma. Tesis ini mengkaji teknik pemodelan bateri yang sedia ada serta mengkaji ciri-ciri dinamik pada 18 Ah LiFePO₄ bateri. Pemodelan model bateri yang baru untuk LiFePO₄ berkapasiti tinggi juga dicadangkan. Model baru ini mengambil kira kesan kapasiti tak linear. Selain itu, metodologi pemodelan bateri juga dipermudahkan dan dicadangkan dalam tesis. Langkah-langkah pengenalan parameter telah dibincangkan dan ketepatan model baru yang dicadangkan ini juga disahkan melalui data uji kaji. Perbandingan antara keputusan uji kaji dan simulasi menunjukkan bahawa model yang dicadangkan dapat mewakili ciri-ciri dinamik bateri dengan ralat yang minimum.

TABLE OF CONTENTS

CHAPTER		TITLE	PAGE
	DEC	LARATION	ii
	DED	ICATION	iii
	ACK	NOWLEDGEMENT	iv
	ABS	ГКАСТ	v
	ABS	ГКАК	vi
	TAB	LE OF CONTENTS	vii
	LIST	OF TABLES	xi
	LIST	OF FIGURES	xii
	LIST	OF SYMBOLS	xvii
	LIST	OF APPENDICES	xxii
1	INTE	RODUCTION	
	1.1	Background	1
		1.1.1 Electric Vehicle	2
		1.1.2 Battery Technologies	3
		1.1.3 Battery Management System	6
		1.1.4 Battery Model	7
	1.2	Statement of Problem	8
	1.3	Thesis Objectives and Contributions	9
	1.4	Thesis Organisation	10
	1.5	Summary	11

2	LITERATURE REVIEW				
	2.1	Dynan	nic Behaviours of Battery	12	
		2.1.1	Current Effect (C- Rate)	14	
		2.1.2	Temperature Effect	14	
		2.1.3	Relaxation Effect	15	
		2.1.4	Open Circuit Voltage and Hysteresis Effect	15	
		2.1.5	Nonlinear Capacity Effects	17	
	2.2	Battery	y Models	19	
		2.2.1	Electrochemical Model	20	
		2.2.2	Mathematical Model	21	
		2.2.3	Equivalent Circuit Model	26	
	2.3	Variati	on in Equivalent Circuit Model	27	
	2.4	Model	Development Technique for Equivalent		
		Circuit	Model	36	
	2.5	Summ	ary	43	
3	BATT	ERY T	EST AND EXPERIMENTAL SET UP		
	3.1	Introdu	uction	44	
	3.2	Experi	mental Set Up and Hardware	44	
		3.2.1	18 Ah LiFePO ₄ Battery	45	
		3.2.2	Electronic Load	47	
		3.2.3	DAQ Device and Data Logging System	47	
	3.3	Battery	y Tests	49	
		3.3.1	Continuous Discharge Test	49	
		3.3.2	Pulse Discharge Test	50	
	3.4	Summ	ary	51	

4	BATTERY MODELLING USING CONVENTIONAL				
	METHOD				
	4.1	Introd	uction	52	
	4.2	Param	eter Identification	52	
		4.2.1	Identification of SOC	53	
		4.2.2	OCV-SOC Relationship	54	
		4.2.3	Parameters of RC Parallel Networks	57	
		4.2.4	Series Resistance, R_S	61	
	4.3	Perfor	mance of Battery Model	63	
		4.3.1	Performance in PDT Tests	64	
		4.3.2	Performance in CDT Tests	66	
	4.4	Summ	ary	69	
5	BATT	TERY N	MODEL WITH CONSIDERATION OF		
5			MODEL WITH CONSIDERATION OF R CAPACITY EFFECT		
5			R CAPACITY EFFECT	70	
5	NONI	LINEA: Introd	R CAPACITY EFFECT	70 70	
5	NONI 5.1	LINEA Introd Nonlii	R CAPACITY EFFECT uction		
5	5.1 5.2	LINEA Introd Nonlii Param	R CAPACITY EFFECT uction near Capacity Effect	70	
5	5.1 5.2	LINEA Introd Nonlii Param	R CAPACITY EFFECT uction near Capacity Effect eters Identification	70 72	
5	5.1 5.2	Introd Nonlin Param 5.3.1	R CAPACITY EFFECT uction near Capacity Effect eters Identification Usable Capacity, α^U	70 72 73	
5	5.1 5.2	Introd Nonlin Param 5.3.1 5.3.2	R CAPACITY EFFECT uction near Capacity Effect eters Identification Usable Capacity, α^U SOC Increment, $\Delta \gamma$	70 72 73 74	
5	5.1 5.2	Introd Nonlin Param 5.3.1 5.3.2 5.3.3	R CAPACITY EFFECT uction near Capacity Effect eters Identification Usable Capacity, α^U SOC Increment, $\Delta \gamma$ OCV-SOC Relationship	70 72 73 74 77	
5	5.1 5.2	Introd Nonlin Param 5.3.1 5.3.2 5.3.3 5.3.4 5.3.5	R CAPACITY EFFECT uction near Capacity Effect eters Identification Usable Capacity, α^U SOC Increment, $\Delta \gamma$ OCV-SOC Relationship Parameters of RC Parallel Networks	70 72 73 74 77 79	
5	NONI 5.1 5.2 5.3	Introd Nonlin Param 5.3.1 5.3.2 5.3.3 5.3.4 5.3.5 Perfor	R CAPACITY EFFECT uction near Capacity Effect eters Identification Usable Capacity, α^U SOC Increment, $\Delta \gamma$ OCV-SOC Relationship Parameters of RC Parallel Networks Series Resistance, R_S	70 72 73 74 77 79	
5	NONI 5.1 5.2 5.3	Introd Nonlin Param 5.3.1 5.3.2 5.3.3 5.3.4 5.3.5 Perfor	R CAPACITY EFFECT uction near Capacity Effect eters Identification Usable Capacity, α^U SOC Increment, $\Delta \gamma$ OCV-SOC Relationship Parameters of RC Parallel Networks Series Resistance, R_S mance of Battery Model with Consideration	70 72 73 74 77 79 83	
5	NONI 5.1 5.2 5.3	Introd Nonlin Param 5.3.1 5.3.2 5.3.3 5.3.4 5.3.5 Perfor of Non	R CAPACITY EFFECT uction near Capacity Effect eters Identification Usable Capacity, α^U SOC Increment, $\Delta \gamma$ OCV-SOC Relationship Parameters of RC Parallel Networks Series Resistance, R_S mance of Battery Model with Consideration nlinear Capacity Effect	70 72 73 74 77 79 83	

6	SIM	SIMPLIFIED BATTERY MODEL WITH					
	TRA	TRANSIENT RESPONSE CORRECTION					
	6.1	Introduction		94			
	6.2	Propo	sed Simplified Battery Model	94			
	6.3	Param	neter Identification	97			
		6.3.1	Parameters for Unloaded Conditions	99			
		6.3.2	Parameters for Loaded Conditions	102			
		6.3.3	Increment of Series Resistance, ΔR_S	106			
	6.4	Perfor	rmance of Simplified Battery Model	107			
		6.4.1	Performance in PDT Tests	107			
		6.4.2	Performance in CDT Tests	110			
		6.4.3	Performance in Random Load Tests	113			
	6.5	Sumn	nary	116			
7	CON	CLUSI	ONS AND FUTURE WORK				
	7.1	Concl	usion	117			
	7.2	Future	e Work	118			
REFER	ENCES			119			
Appendi	ces A - C			125			

LIST OF TABLES

TABLE NO.	TITLE	PAGE
1.1	Characteristics of Lithium-based batteries	6
3.1	Specifications of battery [58]	46
4.1	Usable capacity of battery	54
4.2	OCV-SOC relationship	55
4.3	Parameters of curve fitting	58
4.4	Parameters of RC parallel networks	59
4.5	Series resistance, R_S	63
4.6	Statistic of modelling error in PDT tests	66
4.7	Statistic of modelling error in CDT tests	69
5.1	Usable capacity of battery	73
5.2	Recovered capacity of battery	75
5.3	OCV-SOC relationship	78
5.4	Parameters of RC parallel networks	81
5.5	Statistic of modelling error in PDT tests	88
5.6	Statistic of modelling error in CDT tests	91
6.1	Parameters of RC parallel networks for unloaded	99
	conditions	
6.2	Time constant gain for several current rates	106
6.3	Statistic of modelling error in PDT tests	110
6.4	Statistic of modelling error in CDT tests	111
6.5	Statistic of modelling error in random load tests	113

LIST OF FIGURES

FIGURE NO.	TITLE	PAGE
1.1	Ragone plot of energy storage element [4].	4
1.2	Battery management system (BMS)	7
2.1	Rate dependent of the battery voltage for several currents	13
	at a constant temperature [32]	
2.2	Temperature dependent of the battery voltage for several	13
	temperatures with a fixed discharge current [32]	
2.3	Relaxation Effect of battery	15
2.4	OCV hysteresis effect of LiFePO ₄ battery [35]	16
2.5	OCV hysteresis effect of NiMH battery [36]	17
2.6	Capacity recovery of battery	18
2.7	Kinetic Battery Model (KiBaM) [41]	23
2.8	Stochastic model [41]	26
2.9	Simple battery model [30]	27
2.10	Modified simple battery model [30]	28
2.11	PNGV model [2]	29
2.12	Improved PNGV model [44]	29
2.13	Energetical model of Li-ion battery [12]	30
2.14	Typical VRC model	31
2.15	Proposed VRC model in [11]	32
2.16	Enhanced second order VRC model [42]	33
2.17	Hybrid battery model [27]	34
2.18	Impedance of the proposed battery model in [37]	35

2.19	(a) Battery test cycle and (b) Proposed model	37
	development technique in [46-48]	
2.20	Proposed rapid OCV determination technique in [34]	38
2.21	Equivalent circuit and impedance spectra [49]	39
2.22	Second order VRC model in [50]	41
2.23	Parameter identification from voltage response [50]	41
2.24	Relaxation curves for several SOC [15]	42
3.1	(a) Experimental set up and (b) block diagram for battery	45
	tests	
3.2	18 Ah LiFePO ₄ battery	46
3.3	IT8514C programmable electronic load	47
3.4	Data acquisition device NI9219	48
3.5	Block diagram in LabVIEW 2010	48
3.6	Voltage profiles for CDT with 6 A, 9 A and 18 A of	49
	current	
3.7	Voltage profile for PDT with 6 A, 9 A and 18 A of	50
	current	
3.8	Current profile for PDT with 6 A, 9 A and 18 A of	51
	current	
4.1	Second order VRC battery model [50]	53
4.2	Experimental results for 6 A, 9 A and 18 A PDT tests	54
4.3	Voltage responses in PDT	56
4.4	OCV-SOC relationships	56
4.5	Extracted parameters from 6 A, 9 A and 18 A PDT tests	60
4.6	Identify series resistance, R_S	62
4.7	Series resistances for 6 A, 9 A and 18 A	62
4.8	(a) Comparison between experiment and simulation	65
	results for 6 A PDT test	
	(b) Comparison between experiment and simulation	65
	results for 9 A PDT test	
	(c) Comparison between experiment and simulation	66

	results for 18 A PDT test	
4.9	(a) Comparison between experiment and simulation	67
	results for 6 A CDT test	
	(b) Comparison between experiment and simulation	68
	results for 9 A CDT test	
	(c) Comparison between experiment and simulation	68
	results for 18 A CDT test	
5.1	Comparison between PDT and CDT curves for (a) 6 A,	71
	(b) 9 A, and (c) 18 A without consideration of capacity	
	recovery	
5.2	Experimental results for 6 A, 9 A and 18 A CDT tests	73
5.3	Relationship between usable capacity and current	74
5.4	(a) Deviation exist between PDT and CDT curves, (b)	76
	PDT curve is shifted to left and the shifted capacity is	
	determined, (c) Vertical divergence exists between	
	shifted PDT curve and CDT curve	
5.5	Relationship between increment factor and current	77
5.6	OCV-SOC relationships	79
5.7	Extracted parameters from 6 A, 9 A and 18 A PDT tests	82
5.8	Identification of R_{S0}	83
5.9	R _{S0} -SOC relationships for 6 A, 9 A and 18 A	84
5.10	Identification of ΔR_S	85
5.11	ΔR_S -SOC relationships for 6 A, 9 A and 18 A	85
5.12	(a) Comparison between experiment and simulation	87
	results for 6 A PDT test	
	(b) Comparison between experiment and simulation	87
	results for 9 A PDT test	
	(c) Comparison between experiment and simulation	88
	results for 18 A PDT test	
5.13	(a) Comparison between experiment and simulation	89
	results for 6 A CDT test	

	(b) Comparison between experiment and simulation	90
	results for 9 A CDT test	
	(c) Comparison between experiment and simulation	90
	results for 18 A CDT test	
5.14	(a) Comparison of usable capacity between 6 A PDT and	91
	6 A CDT with consideration of nonlinear capacity effect	
	(b) Comparison of usable capacity between 9 A PDT and	92
	9 A CDT with consideration of nonlinear capacity effect	
	(c) Comparison of usable capacity between 18 A PDT	92
	and 18 A CDT with consideration of nonlinear capacity	
	effect	
6.1	Voltage curves for unloaded conditions	95
6.2	Voltage curves for loaded conditions	95
6.3	Simplified battery model for loaded and unloaded	96
	conditions	
6.4	Extracted (a) A , (b) B , (c) C , (d) D (e) E and (f) F from 9	100
	A PDT tests	
6.5	Determine $G(\gamma, I_L)$	101
6.6	Relationship between R_T and I_L	101
6.7	Voltage curves for V_{k1} , V_{k2} , and V_{k3}	103
6.8	Voltage curves for V_{k1} , V_{k2} , and V_{k3} after gain correction	104
6.9	Voltage curves for 4 th cycle of 9 A PDT test with gain	104
	correction $M_3=1.4854$	
6.10	Voltage curves for V_{k1} , V_{k2} , and V_{k3} after time constant	105
	correction	
6.11	Voltage curves for 4 th cycle of 9 A PDT test with time	106
	constant correction N_2 =2 and N_3 =3	
6.12	Relationship between ΔR_S and SOC	107
6.13	(a) Comparison between experiment and simulation	108
	results for 6 A PDT test	
	(b) Comparison between experiment and simulation	109

	results for 9 A PDT test	
	(c) Comparison between experiment and simulation	109
	results for 18 A PDT test	
6.14	(a) Comparison between experiment and simulation	111
	results for 6 A CDT test	
	(b) Comparison between experiment and simulation	112
	results for 9 A CDT test	
	(c) Comparison between experiment and simulation	112
	results for 18 A CDT test	
6.15	Comparison between experiment and simulation results	114
	for random load test I	
6.16	Comparison between experiment and simulation results	115
	for random load test II	

LIST OF SYMBOLS

Parameters of curve fitting

a' to e'

 C_{dl}

 C_S

A to FParameters for unloaded conditions in simplified model Battery capacity α α^{C} Consumed capacity α^F Full charged capacity α^U Usable capacity β Peukert's constant in Peukert's law **BMS** Battery management system Rate of current C-rate CCFCorrection factor for capacity fading **CDT** Constant discharge test CO_2 Carbon dioxides Capacitance in VRC model which used to represent battery C_{CAP} capacity C_{DL} Double layer capacitor in energetical model

Double layer capacitance

C_r
 Capacitance in RC network in energetical model
 C_I
 Capacitance in first RC parallel network
 C₂
 Capacitance in second RC parallel network
 C₃
 Capacitance in third RC parallel network
 C'₁
 Capacitance in first RC parallel network for unloaded conditions
 C'₂
 Capacitance in second RC parallel network for unloaded conditions
 C'₃
 Capacitance in third RC parallel network for unloaded condition

Storage capacitor in energetical model

c - Fraction of total capacity for available capacity in KiBaM

DAQ - Data Acquisition

EIS - Electrochemical Impedance Spectroscopy

EKF - Extended Kalman Filer

EMS - Energy management system

EV - Electric vehicle ε - Faded capacity f - Discharge phase

 f_C - Capacity factor which related to capacity fading

 f_T - Temperature factor

 f_{max} - Frequency of the peak of semicircle

Voltage raise in the unloaded condition

GHGs - Green house gaseous

 h_1 - Height of available charge well h_2 - Height of bound charge well

I-V - Current-Voltage

ICE - Internal combustion engine

IEA - International Energy Agency

 I_L - Battery current KF - Kalman Filter

KiBaM - Kinetic battery model

K - Polarization constant in Sheperd equation

k - Fixed conductance

k' - Conductance

 κ - Coefficient for cycling effect

L - Total operating time

Li-ion - Lithium-ion

Li-P - Lithium Polymer

LiCoO₂ - Lithium Cobalt Oxide

LiFePO₄ - Lithium Ferro Phosphate

 M_1 - Gain correction for R_1

 M_2 - Gain correction for R_2 M_3 - Gain correction for R_3

m - Computational factor

N - Initial capacity or nominal capacity

NiCd - Nickel-Cadmium

NiFe - Nickel-Iron

NiMH - Nickel-Metal Hydride

NiZn - Nickel-Zinc

 N_1 - Time constant gain for first time constant in time constant

correction

 N_2 - Time constant gain for second time constant in time constant

correction

 N_3 - Time constant gain for third time constant in time constant

correction

n - Number of cycle

*n*_L - Estimated number of usable cycle

OCV - Open Circuit Voltage

OEC D - The Organisation for Economic Co-operation and Development

PDT - Pulse discharge test

PHEV - Plug-in hybrid vehicle

PNGV - Partnership for new generation of vehicle

p - Probability of recover one charge unit in one time slot,

 q_i - Probability of required i charge units in one time slot

RC - Resistor-Capacitor

RMSE - Root mean square error

 $R_{\mathcal{Q}}$ - Ohmic resistance

 R_F - Internal resistance for fully charged condition

 R_S - Series resistance

 R_{SO} - Initial of series resistance

 R_T - Total resistance in simplified model

 R_{ct} - Charge-transfer resistance

 R_{cycle} - Increment of internal resistance caused by the cycling effect

 R_{ex} - Resistive load for model development

 R_{int} - Internal resistance

R₁ - Resistance in first RC parallel network

R₂ - Resistance in second RC parallel network

 R_3 - Resistance in third RC parallel network

R'₁ - Resistance in first RC parallel network for unloaded conditions

R'₂ - Resistance in second RC parallel network for unloaded conditions

 R'_3 - Resistance in third RC parallel network for unloaded conditions

r - Probability of staying in the same SOC

r_{HF} - Ohmic resistance in energetical model

r_r - Resistance in RC network in energetical model

SOC - State-of-charge

SOH - State-of-health

SPKF - Sigma-point Kalman Filter

 S_I - Exponential zone amplitude in Sheperd equation

S₂ - Exponential zone time constant in Sheperd equation

T - Measured temperature

 $T_{AMBIENT}$ - Ambient temperature

 $T_{DEFINED}$ - Defined temperature

 T_{ref} - Reference temperature

t - Battery runtime

 t_E - Ending time of relaxation

 t_R - Ending time of loaded condition or starting time of unloaded

condition

t_S - Starting time of loaded condition

UPS - Uninterruptible power supply

VRC - Voltage-Resistor-Capacitor

VTF - Vogel-Tammann-Fulcher

 V_O - Battery constant voltage in Sheperd equation

 V_{SOC} - Voltage across C_{CAP} in VRC model

 V_S - Voltage relative to R_{S0}

 V_{S2} - Voltage relative to ΔR_S

 V_{kl} - Voltage across first RC parallel network

 V_{k2} - Voltage across second RC parallel network

 V_{k3} - Voltage across third RC parallel network

 V_t - Battery voltage

 v_1 and v_2 - Parameters of VTF equation

W - Warburg impedance

 ω - Frequency

 y_I - Amount of available charge

*y*₂ - Amount of bound charge

 $y_{1,0}$ - Initial available charge

*y*_{2,0} - Initial bound charge

γ - State of charge

 γ_D - Discharged SOC

 γ_0 - Initial SOC of battery

Z - Impedance of battery

 Z_{eq} - Equivalent impedance of battery model

Z_p - Faradic impedance in energetical model for characterising

electrode porosity

Z_t - Faradic impedance in energetical model for characterising

concentration impedance of electrolyte

 σ - Constant related to diffusion rate

 θ - Coefficient of discharge rate

 σ - Warburg coefficient

 λ - Time constant of SOC increment

 ϕ - Increment factor of capacity recovery

 $\Delta E(T)$ - OCV correction value for temperature effect

 $\Delta \gamma$ - SOC increment

 ΔR_S - Series resistance increment

LIST OF APPENDICES

APPENDIX	TITLE	PAGE
A	DATA SHEET OF GP18EVLF	125
В	MATLAB CODE OF BATTERY MODEL	126
C	PUBLICATIONS	129

CHAPTER 1

INTRODUCTION

1.1 Background

World energy supply is highly dependent on unsustainable resources, such as oil (33.2 %), coal (27 %) and natural gas (21.1 %) [1]. Resources of these fossil fuels are limited and expected could be exhausted within 40 years [2]. The consumption of these fossil fuels also produces green house gaseous (GHGs). For instance, fossil fuels are responsible for 85 % of anthropogenic carbon dioxides (CO₂) emissions [3]. International Energy Agency (IEA) has conducted a BLUE Map scenario by 2008, which describes the transformation on energy technology by 2050, in order to reduce the annual emissions of carbon dioxides (CO₂) [4].

According to the statistics provided by the Organisation for Economic Co-operation and Development (OECD) [1], there are approximately 27.3 % of the energy supplies consumed by the transportation sector. Moreover, it was stated that 61.4 % of the world oil is consumed by transportation while the price of oil is rising due to the depletion of oil resources. Therefore, the transformation of energy in this sector may greatly reduce the overall GHGs emissions and oil demands. These situations encourage the research and development activities to build up higher efficiency and cleaner transportation. Electric vehicle (EV) gets the attention and interest of scientists due to its advantages of zero GHGs emissions and higher efficiency. It has been proposed to replace internal combustion engine (ICE) as the mainstream vehicle in the near future. The renewable energy source can be used to

generate the energy sources of EV and thus help to reduce the reliance on fossil fuels and reduce the GHGs [5]. A technology roadmap for Electrical and Plug-in Hybrid Vehicle (EV/PHEV) is also carried out by IEA. The roadmap outlines the strategies to popularise the adoption of EV and PHEV worldwide and provide a significant reduction in light-duty vehicle CO₂ emissions by 2050 [4].

1.1.1 Electric Vehicle

The technology and idea of EV is not entirely new, but has existed for around three centuries. The world's first electric vehicle (EV) was made in 1830s and it used non-rechargeable batteries as the energy storage devices. The EV with rechargeable batteries was then released and it reached the first peak at the end of 19th century [2]. EVs were mass-produced and widely adopted as cars, taxis, buses and delivery vehicles. Even though the first internal combustion engine (ICE) vehicle was made in 1886, the ICE vehicle is not popularly implemented due to their frowziness and inconvenience of manual start [2, 6]. These limitations of ICE vehicle made EVs seem to be a more attractive choice. However, after the self starter of ICE was invented in 1911 and the cheap oil was broadly available, ICE vehicles became more attractive than EVs [6]. The poor EV's performances, such as the higher price of the battery compared to petrol, the long charging time of battery, and the short travel distance of EV, have cause the decline of the EVs' market after 1910s [2, 6]. The world crisis of fuel that happened by the mid of 20th century gave the second chance of EV development. However, the crisis was solved when the Middle East countries provided cheap fuel to the market [2]. The development of EV was aroused again at the beginning of 21st century due to the shortage of fuel resources and the issue of environmental pollution [2, 5].

Advantages of EV include zero emissions of GHG and air pollutants, very low noise, very high efficiency, and relatively low cost of electric motor [4]. For EV, electric motor is used for electric propulsion system while battery is used as the energy storage device. The battery is recharged from grid electricity, regenerative

braking or photovoltaic panels [4]. However, the battery has lower specific energy and specific power than ICE fuel [4]. Therefore, the performance of battery becomes the key for EV development. New battery technology and battery management system are two important aspects that enhance the performance of battery [2].

1.1.2 Battery Technologies

Rechargeable battery is an electrochemical device which converts electrical energy to chemical energy during charging and converts chemical energy to electrical energy during discharging [7]. Although there are several devices, such as ultra-capacitor, super-capacitor and ultra-high speed flywheels that are potentially applied as the energy storage element in EV [7], battery is still preferable due to its high specific energy and its capability of recharged for regenerative braking practice [8]. Apart from EV, batteries are broadly used as an energy storage element for portable electronic device, uninterruptible power supply (UPS), distributed generation, and avionics system.

In the aspect of battery technology, the battery is improved from Lead Acid battery to Nickel-based battery and from Nickel-based battery to Lithium-based battery [2]. Even though the battery technology has significantly improved, the battery technology is still unable to keep up with the pace of the current technology [9-11]. Specific energy, specific power, efficiency, maintenance requirement, cost, management, environment friendliness and safety are the requirements for EV's energy storage element. In this aspect, specific energy is the most important consideration for EV since the rate of specific energy determines the travel range of EV. A heavier battery is required if the battery with lower specific energy is applied. Ragone plot of the energy storage element is shown in Figure 1.1. By referring to Figure 1.1, Lithium ion (Li-ion) battery has the highest specific power and specific energy compared to others [4, 12].

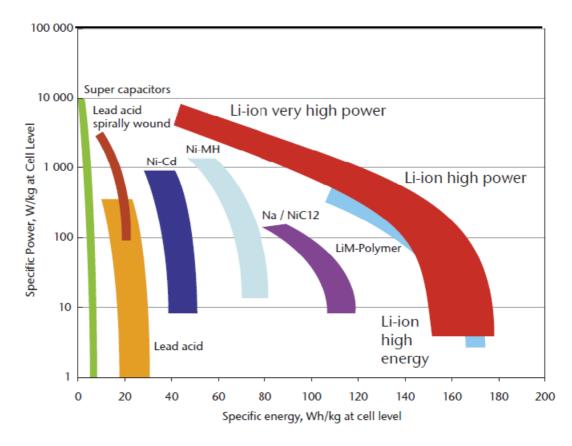


Figure 1.1 Ragone plot of energy storage element [4]

Lead Acid battery is constructed with lead, lead oxide and sulphuric acid. It is widely implemented in transportation sector due to low cost and maturity in technology. However, high molecular weight of lead has caused Lead Acid battery suffers from low specific energy. Additionally, Lead Acid battery also possesses poor temperature characteristic, especially at the low temperature (below 10 °C) [7]. Furthermore, the release of flammable hydrogen gas during self-discharging and the attendance of corrosive sulphuric acid may become safety threats to the vehicle [7].

Nickel-based battery can be categorized into several types, such as Nickel-Iron (NiFe), Nickel-Zinc (NiZn), Nickel-Cadmium (NiCd) and Nickel-Metal Hydride (NiMH). Nickel-based batteries possess higher specific energy and specific power than Lead Acid battery since nickel has lower molecular weight than lead. NiMH battery has highest rate of specific power and specific energy among all the Nickel-based battery. In addition to that, NiMH battery also has long cycle life, good temperature characteristics, low self-discharge rate, flat discharge profile and

negligible corrosion. However, NiMH battery has a high initial cost. Moreover, Nickel-based battery has suffers from memory effect [7]. In this aspect, the capacity of Nickel-based battery would be reduced because of it is not fully discharged before it is recharged [13]. NiMH battery has lesser extent of memory effect compared to NiCd battery [14].

Lithium Polymer (Li-P) and Li-ion are the two major technologies of Lithium-based battery. At the beginning of development, Li-ion battery suffered from safety issue due to the use of metal Lithium as negative electrode. This safety problem is then solved by using carbon material with Lithium insertion as the negative electrode material [12].

Lithium is the lightest metal and allows very high thermodynamic voltage. Therefore, Lithium-based battery has higher terminal voltage, higher specific energy and higher specific power compared to the other rechargeable batteries [12]. It is considered as the most promising battery in the future [7]. By referring to Ragone plot in Figure 1.1, the specific energy and specific power of Li-ion battery is the highest among all type of batteries. The specific energy of Li-ion battery is up to 150 Whkg⁻¹ whereas the specific power of Li-ion battery can reach above 5 kWkg⁻¹ [12]. The desired specific energy and specific power can be achieved by varying the thickness of electrodes [12]. In the field of portable electronic, the majority market of electronic devices is occupied by Lithium-based battery [12].

Lithium Ferro Phosphate (LiFePO₄) is one of the Lithium based battery which uses the phosphates as the cathode material. The theoretical capacity of LiFePO₄ battery is up to 170 mAh/g, which is the highest among lithium based batteries [15]. Moreover, the materials used in LiFePO₄ are widely available, economical and environmental friendly [15]. The handling of LiFePO₄ battery is safe and easy due to its excellent thermal stability in the fully charged condition and good humidity resistant [15]. The stability of LiFePO₄ effectively reduces the risk of explosion when the battery is accidentally overcharged and thus promises the safety of usage. Table 1.1 provides a comparison of Lithium-based battery according to their chemistry. For EV application, a good safety of the battery also ensures the

safety of usage. Hence, LiFePO₄ battery is more suitable to be applied as energy source in EV compared to another Lithium-based battery.

Table 1.1: Characteristics of Lithium-based batteries

Characteristics	Lithium cobalt	Lithium	Lithium ferro
	oxide (LiCoO ₂)	manganese oxide	phosphate
		(LiMn ₂ O ₂)	(LiFePO ₄)
Specific energy	Good	Average	Poor
Power	Good	Good	Average
Low temperature	Good	Good	Average
Calendar life	Average	Poor	Poor above 30°C
Cycle life	Average	Average	Average
Safety*	Poor	Average	Good
Cost/kWh	Higher	High	High
Maturity	High	High	Low

1.1.3 Battery Management System

Battery is the main energy storage device of EV. A handling of battery is necessary so that the battery performs as a safe, consistent and competent energy source under various load demand and driving state [16]. Besides, accurate battery information such as state-of-charge (SOC), state-of-health (SOH), current and voltage are vital for energy management system of EV [17]. Therefore, an efficient battery management system (BMS) which can perform SOC estimation, cell equalisation and temperature management should be put as the primary concern [17]. BMS gives battery protection, increases battery life and its performance. Figure 1.2 shows the block diagram of general BMS.

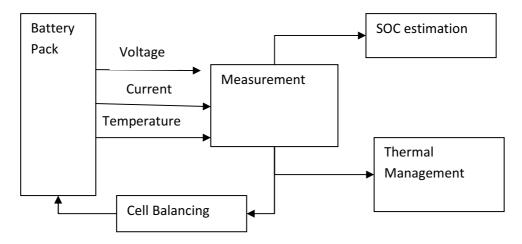


Figure 1.2 Battery management system (BMS)

SOC is the most important parameter to be realised since it demonstrates remaining capacity of the battery. The best performance of battery can be achieved by accurate assessment of SOC [18]. Unwanted harm of battery will occur if the value of SOC is extremely high (overcharged) or low (undercharged). The value of SOC is not readily measurable and thus estimation is required [16]. Several algorithms for SOC estimation have been proposed, such as Kalman Filter (KF) [19], Extended Kalman Filer (EKF) [20-21] and Sigma-point Kalman Filter (SPKF) [22-23]. High accurate performance of these SOC estimation algorithms is proven. These SOC estimation algorithms are model-based techniques which require a battery model that can provide current-voltage (I-V) information of the battery [17]. An accurate battery model is required since the accuracy of battery model would affect the quality of the SOC estimation [24]. Hence, accurate battery model should become the first issue in BMS design.

1.1.4 Battery Model

Battery model is important not only for SOC estimation, but also it is equally important for EMS controllers design, manage charge/discharge process, and lengthening the life of battery [5, 17]. By using accurate battery model, the

characteristics of battery under various charge/discharge conditions can be effectively forecasted and thus optimize the usage of battery [18].

Numerous studies conducted on battery modelling techniques are published in various scientific journals. The battery models can be categorised into analytical, electrochemical and equivalent circuit models [25]. Electrochemical model is complex and involve time-varying spatial partial differential equations. It is also impossible to connect to the rest of the system directly [25]. On the other hand, analytical model is unable to give a good view of the internal electrochemical process of the battery [26] whereas equivalent circuit model has lower accuracy compared to electrochemical model [25]. However, equivalent circuit model is popularly used by circuit designers since the effective battery control is permitted by applying the mathematical equations that derived from equivalent circuit model.

1.2 Statement of Problem

UTM-PROTON Future Drive Laboratory, which was established in UTM Johor Bahru campus, is actively involved in the research and development of the EV's technologies. Research in areas such as battery management system, energy management system, machine controller and power converter are conducted.

Model of battery is vital as a guide for system designer to forecast the electrical characteristics of battery. By applying an accurate battery model, BMS can estimate the SOC and the runtime of the battery efficiently and optimise the performance of battery [27].

Generally, high capacity lithium based batteries pack is applied as energy sources of electric vehicle. LiFePO₄ is potentially to be implemented in electric vehicle since it promises safe usage. However, the research on battery model for LiFePO₄ is still limited. Moreover, most of the battery models in previous research are focus on low capacity battery and only suitable for certain type of battery.

Additionally, battery model that provided by MATLAB/Simulink does not able to accurately simulate the dynamic behaviours of the actual battery as presented in [28-29].

The lack of suitable and accurate battery model would lead to unreliable control of battery. Since battery model is the key of BMS design, it is important to develop an accurate battery model for high capacity LiFePO₄ battery in order to capture the nonlinearity of battery in term of I-V characteristic, SOC and runtime of high capacity LiFePO₄ battery.

1.3 Thesis Objectives and Contributions

The objectives of this study are:

- 1. to study the existing techniques used in battery modelling.
- 2. to investigate the dynamic characteristics of 3.2 V, 18 Ah LiFePO₄ battery.
- 3. to propose a new model for Lithium Ferro Phosphate battery.
- 4. to propose a simple yet significant method of improvement in existing battery modelling techniques.

While performing this study, the thesis makes the following contributions:

- 1. It develops modified model with nonlinear capacity effects consideration to improve the performance of the existing battery model. A novel method to capture nonlinear capacity effects is proposed.
- 2. It introduces a simple battery model which expresses parameters as a function of SOC and current. Parameters for loaded conditions are differentiated from parameters of unloaded conditions. This is because the characteristics of battery can be different in loaded and unloaded conditions as stated in [17], [30], and [31]. This will be discussed further in Chapter 6. Transient response correction is used to determine the

parameters for loaded conditions. The technique is simple, yet it improves the performance of battery model significantly.

1.4 Thesis Organisation

The rest of the thesis is organised as follows:

Chapter 2 discusses the dynamic behaviours and classifications of battery model. This chapter briefly discusses on the proposed battery model in previous researches, such as mathematical models, electrochemical models and equivalent circuit model. Model development for equivalent circuit model is reviewed.

Chapter 3 describes the experimental set-up used in the project. The procedures of battery tests, which are used to identify the parameters of the battery model are presented and described.

Chapter 4 discusses conventional battery model. In this chapter, conventional battery modelling technique is presented briefly. Simulation and the experimental results on the conventional battery model are also presented. The performance of conventional battery model is discussed.

Chapter 5 proposes a modified battery model with consideration of nonlinear capacity effect. In this model, a new approach of capturing nonlinear capacity effect is presented in detail. Simulation and the experimental results on the proposed battery model are also presented. The performance of modified battery model is discussed.

Chapter 6 proposes a simplified battery model. In this model, parameters are expressed as a function of SOC and current to eliminate the usage of look-up table in the model. Simulation and the experimental results on the simplified battery

model are also presented. The performance of simplified battery model is presented. The simplified model is further validated with random load tests.

Chapter 7 gives the conclusions of the thesis and possible directions of further research on this work.

1.5 Summary

As a prelude to the thesis, a brief background of electric vehicle that includes its history and its environmental benefits has been presented. Several issues that related to energy storage system, starting from battery technologies to battery management system, have been presented. Battery model which serves as the key of monitoring EV energy sources is briefly discussed. An equivalent circuit model has been chosen to use for this work due to its simplicity, accuracy and suitability for battery-powered system design.

REFERENCES

- International Energy Agency. Key World Energy Statistics 2010. France: IEA. 1-78; 2010
- 2. Li, S., and Zhang, C. Study on Battery Management System and Lithium-ion Battery. *Proceedings of the 2009 International Conference on Computer and Automation Engineering, ICCAE 2009.* March 8-10, 2009. Bangkok: IEEE, 2009. 218-222.
- Sims, R. E. H., Schock, R. N., Adegbululgbe, A., Fenhann, J., Konstantinaviciute, I., Moomaw, W., Nimir, H. B., Schlamadinger, B., Torres, M. J., Turner, C., Uchiyama, Y., Vuori, S. J. V., Wamukonya, N. and Zhang, X. Energy supply. In Climate Change 2007: Mitigation. Contribution of Working Group III to the Fourth Assessment Report of the Intergovernmental Panel in Climate Change. Cambridge, United Kingdom and New York, NY, USA: Cambridge University Press. 253-315; 2007
- 4. International Energy Agency. *Technology Roadmap: Electric and Plug-in Hybrid Electric Vehicles*. France: IEA. 1-42; 2011
- Zhang, H., and Chow, M.Y. Comprehensive Dynamic Battery Modelling for PHEV Applications. *Proceedings of the 2010 IEEE Power and Energy* Society General Meeting. July 25-29, 2010. Minneapolis, USA: IEEE, 2010. 1-6.
- 6. Larmine, J. and Lowry, J. *Electric Vehicle Technology Explained*. UK: John Wiley & Sons, Ltd. 1-293; 2003
- 7. Ehsani, M., Gao, Y., Gay, S. E. and Emadi, A. *Modern Electric, Hybrid Electric, and Fuel Cell Vehicles-Fundamental Theory, and Design.* USA: CRC Press. 1-385; 2005

- 8. Shafiei, A., Momeni, A., and Williamson, S. S. Battery Modeling Approaches and Management Techniques for Plug-in Hybrid Electric Vehicles. *Proceedings of the* 2011 *IEEE Vehicle Power and Propulsion Conference* (VPPC). September 6-9, 2011. Chicago, IL: IEEE, 2011. 1-5.
- 9. Rao, R., Vrudhula, S., and Rakhmatov, D. Battery Modeling for Energy-Aware System Design. *Computer*. December 2003, vol. 36, no. 12: 77-87.
- 10. Zhang, J., Ci, S., Sharif, H., and Alahmad, M. Modeling Discharge Behavior of Multicell Battery. *IEEE Transactions on Energy Conversion*. December 2010, vol. 25, no. 4: 1133-1141.
- 11. Chen, M. and Mora, G. A. R. Accurate Electrical Battery Model Capable of Predicting Runtime and I-V Performance. *IEEE Transactions on Energy Conversion*. June 2006, vol. 21, no. 2: 504-511.
- 12. Urbain, M., Hinaje, M., Rael, S., Davat, B. and Desprez, P. Energetical Modeling of Lithium-Ion Batteries Including Electrode Porosity Effects. *IEEE Transactions on Energy Conversion*. September 2010, vol. 25, no. 3: 862-872.
- 13. Gilles, T. Automotive Service: Inspection, Maintenance, Repair. 4th edition. USA: Cengage Learning. 101; 2011
- 14. Vijayasaran, P. R. Engineering Chemistry. 2nd Edition. Connaught Circus, New Delhi: PHI Learning Pvt. Ltd. 48; 2011
- 15. Liao, C., Li, H. and Wang, L. A dynamic Equivalent Circuit Model of LiFePO₄ Cathode Material for Lithium Ion Batteries on Hybrid Electric Vehicles. *Proceedings of the 2009 IEEE Vehicle Power and Propulsion Conference (VPPC)*, September 7-10, 2009. Dearborn, MI: IEEE, 2009. 1662-1665.
- 16. Hu, X., Li, S. and Peng, H. A comparative study of equivalent circuit models for Li-ion batteries. *Journal of Power Sources*. 2012, 198: 359-367.
- Hu, Y., Yurkovich, S., Guezennec, Y., Yurkovich, B. J. A technique for dynamic battery model identification in automotive applications using linear parameter varying structures. *Control Engineering Practice*. 2009, vol. 17: 1190-1201.
- 18. Coleman, M., Lee, C. K., Zhu, C., Hurley, W. G. State-of-Charge Determination From EMF Voltage Estimation: Using Impedance, Terminal Voltage, and Current for Lead-Acid and Lithium-Ion Batteries. *IEEE*

- Transactions on Industrial Electronics. October 2007, vol. 54, no. 5: 2550-2557.
- 19. Plett, G. L. Extended Kalman filtering for battery management systems of LiPB-based HEV battery packs. Part 1: Background. *Journal of Power Sources*. 2004, 134: 252-261.
- 20. Plett, G. L. Extended Kalman filtering for battery management systems of LiPB-based HEV battery packs. Part 2: Modeling and identification. *Journal* of Power Sources. 2004, 134: 262-276.
- 21. Plett, G. L. Extended Kalman filtering for battery management systems of LiPB-based HEV battery packs. Part 3: State and parameter estimation. *Journal of Power Sources*. 2004, 134: 277-292.
- 22. Plett, G. L. Sigma-point Kalman filtering for battery management systems of LiPB-based HEV battery packs. Part 1. Introduction and state estimation. *Journal of Power Sources*. 2006, 161: 1356-1368.
- 23. Plett, G. L. Sigma-point Kalman filtering for battery management systems of LiPB-based HEV battery packs. Part 2. Simultaneous state and parameter estimation. *Journal of Power Sources*. 2006, 161: 1369-1384.
- 24. Kim, I. S., The Novel State of Charge Estimation Method for Lithium Battery Using Sliding Mode Observer. *Journal of Power Sources*. 2006, 163: 584-590.
- 25. Lam, L., Bauer, P. and Kelder, E. A Practical Circuit-based Model for Li-ion Battery Cells in Electric Vehicle Applications. *Proceedings of the IEEE 33rd Telecommunications Energy Conference (INTELEC)*. October 9-13, 2011. Amsterdam: IEEE, 2011. 1-9.
- 26. Rakhmatov, D. Battery Voltage Modeling for Portable Systems. *ACM Transactions on Design Automation of Electronics Systems*. March 2009, vol. 14, no. 2, Article 29: 1-36.
- 27. Kim, T. and Qiao, W. A Hybrid Battery Model Capable of Capturing Dynamic Circuit Characteristics and Nonlinear Capacity Effects. *IEEE Transactions on Energy Conversion*. December 2011, vol. 26, no. 4: 1172-1180.
- 28. Tremblay, O., Dessaint, L. A. and Dekkiche, A. I. A Generic Battery Model for the Dynamic Simulation of Hybrid Electric Vehicles. *Proceedings of the*

- 2007 IEEE Vehicle Power and Propulsion Conference (VPPC). September 9-12, 2007. Arlington, TX: IEEE. 2007. 284-289.
- 29. Tremblay, O. and Dessaint, L. A. Experimental Validation of a Battery Dynamic Model for EV Applications. *World Electric Vehicle Journal*. 2009, vol. 3: 1-10.
- 30. Chan, H. L. and Sutanto, D. A New Battery Model for use with Battery Energy Storage System and Electric Vehicle Power Systems. *Proceedings of the 2000 IEEE Power Engineering Society Winter Meeting*, vol. 1. January 23-27, 2000. Singapore: IEEE, 2000. 470-475.
- 31. Hentunen, A., Lehmuspelto, T. and Suomela, J. Electrical Battery Model for Dynamic Simulations of Hybrid Electric Vehicles. *Proceedings of the IEEE Vehicle Power and Propulsion Conference (VPPC)*. September 6-9, 2011. Chicago, IL: IEEE, 2011. 1-6.
- 32. Gao, L., Liu, S., Dougal, R. A. Dynamic Lithium-Ion Battery Model for System Simulation. *IEEE Transactions on Component and Packaging Technologies*. September 2002, vol. 25, no. 3: 495-505.
- 33. Benger, R., Wenzl, H., Beck, H. P., Jiang, M., Ohms, D. and Schaedlich, G. Electrochemical and thermal modelling of lithium-ion cells for use in HEV and EV application. *World Electric Vehicle Journal*. 2009, vol. 3: 1-10.
- 34. Suleiman, A. S. and Doerffel, D. Rapid test and non-linear model characterisation of solid-state lithium-ion batteries. *Journal of Power Sources*. 2004, 130: 266-274.
- 35. Roscher, M. A. and Sauer, D. U. Dynamic electric behaviour and open-circuit-voltage modelling of LiFePO₄- based lithium ion secondary batteries. *Journal of Power Sources*. 2011, 196: 331-336.
- 36. Ota, Y. and Hashimoto, Y. Modeling of Voltage Hysteresis and Relaxation of HEV NiMH Battery. *Electrical Engineering in Japan*. 2011, vol. 175, no. 1: 1-7.
- 37. Erdinc, O., Vural, B. and Uzunoglu, M. A dynamic lithium-ion battery model considering the effects of temperature and capacity fading. *Proceedings of the 2009 International Conference on Clean Electrical Power*. June 9-11, 2009. Capri: IEEE, 2009. 383-386.
- 38. Rakhmatov, D. N. and Vrudhula, S. B. K. An Analytical High-Level Battery Model for Use in Energy Management of Portable Electronic System.

- Proceedings of the 2011 IEEE/ACM International Conference on Computer Aided Design (ICCAD). November 4-8, 2001. San Jose, CA: IEEE, 2001. 488-493.
- 39. Bauer, P., Stembridge, N., Doppler, J. and Kumar, P. Battery Modeling and Fast Charging of EV. *Proceedings of the 2010 14th International Power Electronics and Motion Control Conference (EPE/PEMC)*. September 6-8, 2010. Ohrid: IEEE, 2010. S11-39 S11-45.
- 40. Kroeze, R. C. and Krein, P. T. Electrical Battery Model for Use in Dynamic Electric Vehicle Simulations. *Proceedings of the 2008 IEEE Power Electronics Specialists Conference (PESC)*. June 15-19, 2008. Rhodes: IEEE, 2008. 1336-1342.
- 41. Jongerden, M. R. and Haverkort, B. R. Which battery model to use? *IET Software*. July 3-4, 2008, vol. 3, issue 6: 445-457.
- 42. Zhang, J., Ci, S., Sharif, H. and Alahmad, M. An Enhanced Circuit-Based Model for Single-Cell battery. *Proceedings of the 2010 Twenty-Fifth Annual IEEE Applied Power Electronics Conference and Exposition (APEC)*. February 21-25, 2010. Plam Sprints, CA: IEEE, 2010. 672-675.
- 43. Chiasserini, C. F. and Rao, R. R. Energy Efficient Battery Management. *IEEE Journal on Selected Areas in Communications*. July 2001, vol. 19, no. 7: 1235-1245.
- 44. Gao, W., Jiang, M. and Hou, Y. Research on PNGV Model Parameter Identification of LiFePO₄ Li-ion Battery Based on FMRLS. *Proceedings of the IEEE 6th Industrial Electronics and Applications (ICIEA)*. June 21-23, 2011. Beijing: IEEE, 2011. 2294-2297.
- 45. Wey, C. L., Chang, K. C., Hsu, C. H. and Chen, S. W. Lithium battery Models for Battery Charging and System Loading. *Proceedings of the IEEE* 54th International Midwest Symposium on Circuits and Systems (MWSCAS). August 7-10, 2011. Seoul: IEEE, 2011. 1-4.
- 46. Norian, K. H. Transient-boundary voltage method for measurement of equivalent circuit components of rechargeable batteries. *Journal of Power Sources*. 2011, 196: 2360-2363.
- 47. Norian, K. H. Equivalent circuit components of nickel-cadmium battery at different state of charge. *Journal of Power Sources*. 2011, 196: 5205-5208.

- 48. Norian, K. H. Equivalent circuit components of nickel-metal hydride battery at different state of charge. *Journal of Power Sources*. 2011, 196: 7812-7815.
- 49. Rodrigues, S., Munichandraiah, N. and Shukla, A. K. A review of state-of-charge indication of batteries by means of a.c. impedance measurements. *Journal of Power Sources*. 2000, 87: 12-20.
- 50. Schweighofer, B., Raab, K. M. and Brasseur, G. Modeling of high power automotive batteries by the use of an automated test system. *IEEE Transactions on Instrumentation and Measurement*. August 2003, vol. 52, no. 4: 1087-1091.
- 51. Zhang, C. P., Liu, J., Sharkh, S. M. and Zhang, C. N. Identification of dynamic model parameters for lithium-ion batteries used in hybrid electric vehicles. *Proceedings of the International Symposium on Electric Vehicles* (ISEV). September 2009. Beijing, China: ISEV, 2009. 1-11.
- 52. He, H., Xiong, R., Zhang, X., Sun, F. and Fan, J. State-of-charge Estimation of Lithium-ion Battery using and Adaptive Extended Kalman Filter Based on an Improved Thevenin Model. *IEEE Transactions on Vehicular Technology*. May 2011, vol. 60, no. 4: 1461-1469.
- 53. He, H., Xiong, R. and Guo, H. Online estimation of model parameters and state-of-charge of LiFePO₄ batteries in electric vehicles. *Applied Energy*. 2011, vol. 89: 413-420.
- 54. He, H., Zhang, X., Xiong, R., Xu, Y. and Guo, H. Online model-based estimation of state-of-charge and open-circuit voltage of lithium-ion batteries in electric vehicles. *Energy*. 2012, vol. 39: 310-318.
- 55. Lee, S., Kim, J., Lee, J. and Cho, B.H. State-of-charge and capacity estimation of lithium-ion battery using a new open-circuit voltage versus state-of-charge. *Journal of Power Sources*. 2008, 185: 1367-1373.
- 56. Schweiger, H. G., Obeidi, O., Komesker, O., Raschke, A., Schiemann, M., Zehner, C., Gehnen, M., Keller, M. and Birke, P. Comparison of Several Methods for Determining the Internal Resistance of Lithium Ion Cells. *Sensors*. 2010, vol. 10: 5604-5625.
- 57. Yuan, X., Song, C., Wang, H. and Zhang, J. *Electrochemical Impedance Spectroscopy in PEM Fuel Cells: Fundamentals and Applications*. London: Springer. 129; 2009
- 58. Gold Peak Group. GP Batteries Data Sheet. Model No: GP18EVLF.