

DAMAGE EVOLUTION IN CARBON FIBER-REINFORCED POLYMER (CFRP)  
COMPOSITES UNDER SHEAR FATIGUE LOADING

MOHAMMADREZA ARJMANDI

A project report submitted in fulfilment of the  
requirements for the award of the degree of  
Master of Engineering (Mechanical)

Faculty of Mechanical Engineering  
Universiti Teknologi Malaysia

AUGUST 2012

To my beloved mom, dad, my brothers, and my lovely fiancée, Sara, who offered me  
unconditional love and support throughout the course of this thesis

## ACKNOWLEDGMENT

This dissertation would not have been possible without the guidance and the help of several individuals who in one way or another contributed and extended their valuable assistance in the preparation and completion of this study.

First and foremost, my utmost gratitude to Prof. Dr. Mohd Nasir Tamin, as well as Dr. Muhammad Adil Khattak, my supervisors whose sincerity and encouragement I will never forget. Prof. Nasir and Dr. Adil have been my inspiration as I hurdle all the obstacles in the completion this research work.

I would also like to appreciate Seyed Saeid Rahimian Kolor, PhD candidate, who helped me a lot during this research and spending a lot of his precious time and energy, teaching me FE software and composite structures concepts. The assistance and technical guidance of all computational solid mechanics laboratory (CSM Lab) members are also acknowledged, and the experiments conducted in this research was impossible without the support and help of mechanical testing laboratory staff, whom I would like to thank warmly.

Last but not the least, my family and the one above all of us, the omnipresent God, for answering my prayers for giving me the strength to plod on despite my constitution wanting to give up and throw in the towel, thank you so much Dear Lord.

## ABSTRACT

Composite structures present high strength, low weight and design flexibility in terms of fiber orientation and number of plies and used vastly in advanced and modern applications. Among them, carbon fiber-reinforced polymer composites (CFRP) are used widely in aeronautic and automotive industries in which components are subjected to different loading types and this will double the necessity of investigation on fatigue and fracture analysis using damage mechanics concepts. The reliability of structures made of composites, depends on continual process of damage initiation and propagation. In the current research, a specific CFRP composite is being tested and finite element simulated under monotonic loading and subsequent cyclic loading with dominant shear stress along its length. The specimen is designed so that the damage development can be tracked easily on the localized interface. The 3ENF experiments and FE simulation have been used simultaneously to investigate the damage under mode II fracture loading condition. Damage model used is cohesive zone model (CZM) which is developed and validated before. The key contribution of the current research is to present and describe a concept to extend current damage model to account for material behavior in cyclic loading in terms of development of damage. Damage is interpreted as degradation of penalty stiffness in normal and shear directions. Monotonic results showed that the CZM-based FE model is correlated well with experimental results and based on the experimental-computational approach, CZM parameters can be obtained and damage model will be characterized so that finite element method can be validated and stress and deformation analyses using FE results are feasible. The cyclic tests are also conducted for different load amplitude and number of cycles and necessary results are extracted to monitor and investigation on degradation in material stiffness and fracture energy as an effect of fatigue phenomenon and also being utilized to obtain presented fatigue damage model and as guidance and useful resource for future finite element simulation applying proper user-written subroutine into FE package.

## ABSTRAK

Struktur komposit memberikan kekuatan yang tinggi, berat yang rendah dan reka bentuk yang fleksibel terutamanya dari segi orientasi gentian dan bilangan lapisan gentian dan digunakan secara meluas dalam aplikasi maju dan moden. Di antara kebanyakan komposit, komposit polimer bertetulang gentian karbon (CFRP) digunakan secara meluas dalam industri aeronotik dan automotif. Di mana, komponen ini dikenakan beban yang berbeza-beza dan ini akan menggandakan keperluan dalam analisis kelesuan dan analisis patah menggunakan konsep mekanik kerosakan. Kebolehpercayaan struktur yang diperbuat daripada komposit ini bergantung kepada proses pemulaan dan peregangan kerosakan. Kajian pada masa kini, komposit CFRP tertentu telah diuji dan simulasi finite element telah dijalankan di bawah beban monotonik dan beban kitaran berikutan dengan tegasan ricih mendominasi panjangnya. Spesimen yang digunakan direka supaya kerosakan dapat dikesan dengan mudah pada antara muka setempat. Eksperimen 3ENF dan simulasi FE telah digunakan secara serentak untuk memeriksa kerosakan di bawah beban keadaan patah pada mod II. Model kerosakan yang digunakan ialah cohesive zone model (CZM) yang telah dibangunkan dan telah disahkan. Sumbangan utama penyelidikan ini adalah untuk menerangkan satu konsep untuk melanjutkan kerosakan model semasa dengan mengambil kira perilaku bahan di dalam beban berkitar dari segi pembangunan kerosakan. Kerosakan ditafsirkan sebagai penurunan kekakuan penalti pada arah normal dan ricihan. Keputusan monotonik menunjukkan model CZM berasaskan FE berhubung baik dengan keputusan eksperimen. Berdasarkan pendekatan eksperimen-pengiraan, parameter CZM boleh diperolehi dan model kerosakan boleh dikenalpasti. Oleh itu, kaedah FE boleh disahkan, tegasan dan pembentukan analisis menggunakan keputusan FE dapat dilaksanakan. Ujian kitaran dilaksanakan untuk beban amplitude yang berlainan dan bilangan kitaran dan keputusan yang diperlukan untuk memantau dan memeriksa penurunan di dalam kekakuan bahan dan tenaga patah sebagai kesan fenomena lesu dan juga digunakan untuk mendapatkan model kelesuan sebagai panduan dan sumber yang diperlukan untuk simulasi FE akan datang dengan menggunakan subrutin FE yang sesuai ke dalam perisian FE.

## TABLE OF CONTENTS

CHAPTER	TITLE	PAGE
	<b>DECLARATION</b>	ii
	<b>DEDICATION</b>	iii
	<b>ACKNOWLEDGEMENTS</b>	iv
	<b>ABSTRACT</b>	v
	<b>ABSTRAK</b>	vi
	<b>TABLE OF CONTENTS</b>	vii
	<b>LIST OF TABLES</b>	x
	<b>LIST OF FIGURES</b>	xi
	<b>LIST OF SYMBOLS AND ABBREVIATIONS</b>	xv
<b>1</b>	<b>INTRODUCTION</b>	
	1.1 Introduction	1
	1.2 Background of study	2
	1.2.1 Cohesive Zone Model (CZM)	3
	1.2.2 Composite materials	3
	1.2.3 Finite element method	4
	1.3 Statement of problem	4
	1.4 Research questions	5
	1.5 Objectives of study	5
	1.6 Scope of study	6
	1.7 Importance of study	7
	1.8 Research approach	8

1.9 Structure of research	8
<b>2 LITERATURE REVIEW</b>	
2.1 Introduction	10
2.2 Composite structures	10
2.2.1 Composite applications	13
2.2.2 Composite failure mechanisms	14
2.2.3 Failure criteria	15
2.3 Fatigue phenomenon in fiber-reinforced composite structures	19
2.3.1 Introduction to Fatigue Failure	19
2.3.2 Fatigue phenomena in fiber composites	23
2.4 Damage in composites	24
2.4.1 Shear fatigue properties of CFRP	27
2.4.2 Fatigue damage modeling in fiber-reinforced composites	29
2.4.3 Cohesive Zone Model	33
<b>3 METHODOLOGY</b>	
3.1 Introduction	37
3.2 Cohesive Zone Model	39
3.2.1 CZM for shear loading	39
3.2.2 Obtaining CZM parameters for monotonic loading	45
3.3 CFRP composite specimen geometry and material properties	48
3.4 Experimental procedure	51
3.4.1 3ENF test in monotonic loading condition	51
3.4.2 3ENF fatigue test for residual strength	52
3.5 New cohesive model for cyclic loading of interface	55
3.5.1 Obtaining CZM parameters for cyclic loading	57
3.5.2 Characteristic degradation of interface properties under cyclic loading	59
3.6 Finite element simulation	61

3.6.1 FE modeling procedure for monotonic loading	63
<b>4 RESULTS AND DISCUSSION</b>	
4.1 Introduction	69
4.2 Monotonic test of CFRP specimen	70
4.3 FE simulation of CFRP under shear loading	74
4.3.1 Perfect bonding simulation of 3ENF CFRP composite	74
4.3.2 CZM implementation in 3ENF CFRP composite simulation	79
4.3.2.1 Deformation Analysis	82
4.3.2.2 Stress and damage analyses	83
4.4 Experimental results of CFRP specimen subjected to cyclic loading	88
4.4.1 Load and displacement monitoring	88
4.4.2 Microscopic view	94
4.4.3 Load-deflection response of CFRP specimen after fatigue tests	101
4.5 Investigation on fatigue damage parameters for extended CZM	104
<b>5 CONCLUSION</b>	
5.1 Conclusions	109
5.2 Recommendation and future works	113
<b>REFERENCES</b>	116



**LIST OF TABLES**

<b>TABLE NO.</b>	<b>TITLE</b>	<b>PAGE</b>
3.1	Mechanical properties of CFRP composite laminate	50

## LIST OF FIGURES

FIGURE NO.	TITLE	PAGE
2.1	Schematic of stages I (shear mode) and II (tensile mode) transcrystalline microscopic fatigue crack growth	21
2.2	Schematic representation of fatigue process	22
2.3	Degradation of composite strength by wear-out until the residual strength $\sigma_R$ falls from the normal composite strength $\sigma_c$ to the level of the fatigue stress, at which point failure occurs	25
2.4	Normalized plots of two types of damage, which occur during the fatigue cycling of a CSM/polyester laminate (redrawn from Howe and Owen).	26
2.5	Density of cracks in 45° plies in a [(±45,0 <sub>2</sub> ) <sub>2</sub> ]ST800/5245 CFRP laminate during cycling at a peak stress of 1 GPa and an R ratio of 0.1	27
2.6	Experimental observation and model prediction of damage Index for 810 O laminates a) 80% loading level b) 75% loading level	31
2.7	Sketch of a sample after a uniaxial traction test using the cohesive/volumetric finite element approach	34
3.1	Operational research framework	38
3.2	Bilinear representation of cohesive zone model	40
3.3	Result of 3ENF test as a tool for validation of FE simulation	46

3.4	Obtaining $K_s^0$ from FE simulation results and $\delta_s^f$ from both methods	47
3.5	a) the specimen geometry and dimensions in millimeters, b) Location of insert, made of Teflon tape as pre-crack	49
3.6	3ENF test setup and dimensions in millimeters	51
3.7	Nomenclature for constant amplitude cyclic loading	53
3.8	Test assembly for 3ENF monotonic testing of CFRP	53
3.9	Hydraulic testing machine for cyclic testing of CFRP	54
3.10	Cyclic 3-point bending test with lower rollers motion	54
3.11	Schematic of traction-separation curves for monotonic and cyclic loading	55
3.12	Schematic traction-separation curves for monotonic and cyclic loading based on simplified model.	56
3.13	Schematic of load-displacement curves of monotonic and cyclic loading.	57
3.14	Graphical representation of traction-separation plots for monotonic and cyclic loading	59
3.15	Graphical illustration of degradation in penalty stiffness as the number of cycles increases	60
3.16	Location of cohesive layer in front of crack tip in the middle of specimen	64
3.17	Finite element discretization of specimen and the location of (1) crack line and (2) crack tip and boundary conditions of rigid bodies	65
3.18	Boundary conditions of specimen to avoid rigid body motion effect	67
4.1	Load vs. displacement of 3-point bending test of CFRP composite	71
4.2	Micrographs of composite specimen before and after the monotonic test: a) side view of Teflon tape insert and composite body b) crack tip location c) delamination of	73

	top laminas after the test d) crack propagation after the test	
4.3	Deformed and undeformed shape of composite under 3ENF simulation	75
4.4	Interface shear stress contour with zooming on edges	76
4.5	Shear stress contour of interface in gray scale	77
4.6	Comparison of experimental and perfect bonding FE simulation results	78
4.7	Comparison of Experimental and different FE approach results in terms of load-deflection response	80
4.8	Characterized CZM bilinear representation for monotonic FE simulation	82
4.9	Deformed shape of composite interface using CZM	83
4.10	S13 contour of cohesive layer during different step periods	84
4.11	Shear stress distribution along longitudinal edge of cohesive layer	85
4.12	Shear stress distribution along transverse edge of cohesive layer ahead of crack tip	86
4.13	Damage progression of cohesive layer during different step periods	87
4.14	Maximum and minimum displacement recorded as function of No. of cycles (50K test)	90
4.15	Maximum applied load change vs. No. of cycles ( 50K test)	91
4.16	Minimum applied load change vs. No. of cycles ( 50K test)	91
4.17	Displacement amplitude vs. No. of cycles ( 50K test, 200N)	92
4.18	Displacement amplitude vs. No. of cycles ( 50K test, 400N)	92
4.19	CFRP specimen micrographs before the cyclic test	95
4.20	CFRP specimen micrographs after 50K cyclic test (200N)	96

4.21	CFRP specimen micrographs after mode II fracture test (200N)	98
4.22	CFRP specimen micrographs after 50K cyclic test (400N)	99
4.23	CFRP specimen micrographs after mode II fracture test (400N)	100
4.24	Load-displacement response of fatigue-affected composite specimens in comparison with none-damaged specimen	102
4.25	Critical Energy release rate as a function of number of cycles	103
4.26	Comparison of traction-separation curves of monotonic and 50K-180N cyclic loading	105
4.27	Comparison of traction-separation curves of monotonic and 50K-90N cyclic loading	106
4.28	Penalty stiffness in shear direction as a function of fatigue and load amplitude	107
4.29	Interface residual shear strength as a function of fatigue and load amplitude	108

## LIST OF SYMBOLS

$a$	-	Crack length
$A$	-	Area
$b$	-	width
$D$	-	Damage variable
$E$	-	Young`s modulus of elasticity
$f$	-	frequency
$G$	-	Shear modulus
$G_c$	-	Critical energy release rate
$K_n$	-	Penalty stiffness in normal direction
$K_s$	-	Penalty stiffness in shear direction
$K_s^f$	-	Penalty stiffness in shear direction, fatigue loading
$L$	-	length
$N$	-	Number of cycles
$N_f$	-	Fatigue life
$N_0$	-	Nominal stress in normal mode
$P$	-	Load
$R$	-	Load ratio
$S$	-	Maximum interfacial strength in shear mode
$S_0$	-	Nominal stress in shear mode
$S_a$	-	Alternating stress
$S_m$	-	Mean stress
$S_{max}$	-	Maximum cyclic load
$S_{min}$	-	Minimum cyclic load
$t$	-	thickness
$V_f$	-	Fiber volume fraction
$\alpha$	-	Delamination length

$\beta$	-	Mode mixity
$\delta$	-	Deflection , separation
$\delta_0$	-	Relative displacement at damage onset
$\delta_f$	-	Relative displacement at fracture
$\delta_m$	-	Total mixed-mode relative displacement
$\delta_{shear}$	-	Tangential displacement
$\Delta S$	-	Stress range
$\phi$	-	Diameter
$\eta$	-	Power at B-K criterion
$\nu$	-	Poisson ratio
$\sigma_c$	-	Composite normal strength
$\sigma_R$	-	Residual strength
$\tau$	-	Shear stress, traction force

## **CHAPTER 1**

### **INTRODUCTION**

#### **1.1 Introduction**

In this chapter, the background of the study and some discussions on key issues relating to damage mechanics of advanced composite structures, under cyclic loading condition will be presented and briefly described. Moreover, the finite element method as a key numerical procedure to study the behavior of material during evolution of damage under shear stress will be shortly discussed. Subsequently, the objectives of the study will be either presented or followed by a discussion on the scope and significance of the study. The chapter ends with a description of the framework and supports exploited in this study and the operational definition.

The current research will focus on modeling and finite element (FE) simulation of a specific carbon fiber reinforced polymer (CFRP) with specific number of plies and fiber orientation with pre-existing crack and in three point flexural cyclic loading condition and tries to predict the dominant damage mechanisms and evolution of damage in such situations. The FE simulation should then validated with real-world conditions, therefore a systematic experimental procedure will be conducted and the results of both numerical modeling and simulation and also



experimental data will be compared with each other to investigate on accuracy and reliability of numerical method.

## **1.2 Background of the study**

The increasing use of fiber-reinforced materials, especially carbon fiber-reinforced plastics, for load-bearing components which may be subjected to vibratory conditions, such as in aerospace applications, necessitates knowledge of the fatigue behavior of these materials. Research into the fatigue response of fiber composites has been carried out since the materials themselves first began to be a subject of serious study. Some of the first papers on the fatigue behavior of glass-reinforced plastics, for example, were published in the USA by Boller in the 1950s and 60s, and shortly after this Owen and his collaborators at Nottingham University in the UK were reporting the results of work on early carbon-fiber reinforced plastics (CFRPs).[1]

Unlike metals, composite materials are inhomogeneous (on a gross scale) and anisotropic. They accumulate damage in a general rather than a localized fashion, and failure does not always occur by the propagation of a single macroscopic crack. The micro-structural mechanisms of damage accumulation, including fiber breakage and matrix cracking, debonding, transverse-ply cracking, and delamination, occur sometimes independently and sometimes interactively, and the predominance of one or the other may be strongly affected by both materials variables and testing conditions.

### **1.2.1 Cohesive zone model**

The Cohesive zone Model (CZM) offers an alternative way to view failure in materials or along material interfaces. It is a phenomenological model instead of an exact physical representation of material behavior in the fracture process zone, where distributed micro cracking or void formation takes place (Atkinson [2]). The original proposal of the strip yield zone model of Dugdale [2] idealized the plastic region as a narrow strip extending ahead of the crack tip, and a relation is obtained between the extent of plastic yielding and external load applied. This concept has been regarded as a cohesive zone type model with the strip yield zone treated as a cohesive zone. Based on the underlying atomic nature of the fracture process, Barenblatt [2] assumes a nonlinear cohesive force to be distributed over a sufficiently large zone (relative to atomic dimensions) along the crack plane instead of infinitesimally concentrated along a line. Later applications have related the cohesive zone to the plastic zone or the process zone. Despite various definitions of the cohesive zone, the physical meaning is still up to individual understanding.

### **1.2.2 Composite material**

According to the definition a composite consists of two or more chemically distinct materials which when combined have improved properties over the individual materials. Composite materials have advantageous over metals such as high strength, light weight, design flexibility, consolidation of parts etc. Advanced composite materials are finding increasing application in aerospace, automotive, marine and many other industries due to the advantages in performance, structural efficiency and cost they provide. Composite structures have different classifications, such as Particle-Reinforced, Fiber-Reinforced and Structural composites. From these categories; fiber-reinforced composites have wide range of application in modern and advanced structures. Carbon Fiber-Reinforced Polymer (CFRP) composites are

commonly employed in modern structural application such as aircraft wing, rotor blades, and automobile chassis.

### **1.2.3 Finite element method**

The finite element method (FEM) is a numerical method seeking an approximated solution of the distribution of field variables in the problem domain that is difficult to obtain analytically. It is done by dividing the problem domain into several elements. Known physical laws are then applied to each small element, each of which usually has a very simple geometry. A continuous function of an unknown field variable is approximated using piecewise linear functions in each sub-domain, called an element formed by nodes. The unknowns are then the discrete values of the field variable at the nodes. Next, proper principles are followed to establish equations for the elements, after which the elements are ‘tied’ to one another. This process leads to a set of linear algebraic simultaneous equations for the entire system that can be solved easily to yield the required field variable.[3]

### **1.3 Statement of the problem**

Simply supported laminated composite specimen under three point flexural cyclic loading is considered. This laminate can be generally in any type of angle-ply or cross-ply. The task is to investigate the process of damage first in static and then under cyclic flexural loading. The investigation should be done on how the damage initiates and will propagate in composite laminas under fatigue loading condition. The method which is applied is finite element method (FEM). Moreover, simulation on the damage mechanism of specimen will be done with one of the commercial CAE

packages, namely, ABAQUS. The method of monitoring damage in composite laminate and its reliability should also be investigated.

#### **1.4 Research Question**

- What are the damage mechanisms in CFRP composites under cyclic loading?
- What are the current models for deformation and failure of CFRP under shear fatigue loading condition?
- How can these models be used effectively to result in life prediction of composite part under mentioned load?
- What is the suitable testing procedure for establishing model parameters and damage evolution characteristics?
- How could the FEA be validated for damage tolerance and reliability of CFRP composite component?

#### **1.5 Objective of study**

Main research objectives are briefly as below:

- To identify dominant damage mechanisms and their interactions during failure process of CFRP laminates.
- To study and determine damage evolution characteristics of CFRP composites under shear cyclic loading.

- To demonstrate a model for fatigue life prediction of CFRP composites under cyclic loading using finite element method (FEM).
- To validate damage mechanics model for the composite laminate failure.

## **1.6 Scopes of the study**

- Carbon fiber-reinforced polymer (CFRP) composite laminates with specific lay-up will be used as representative material.
- Testing procedure and specimen preparation will be according to ASTM standard (D709-07).
- Damage Model of material will be based on existing damage-based formulations, with some modifications when needed.
- Damage model will be validated using data from standard test procedure on cyclic loading.
- Finite Element software, ABAQUS ver. 6.9 EF will be used for simulation and analysis.

## **1.7 Importance of the study**

Considering that fatigue is the main failure mechanism under cyclic loading and difficulties in fatigue analysis and consequent life prediction since the difference between material properties of constituents and possible fatigue behavior affection of one constituent by the presence of other constituents and also the interfacial regions between the fibers and matrix, it can easily be understood that study in this field is of prime importance and necessary. Many composites are far more sensitive to being loaded in shear than in tension, since their ratio of tensile to shear strength is high (20 is typical for CFRP). Therefore a unified approach should account for various damage and fracture modes in the design phase with the aid of numerical modeling and validation testing of the composite sample coupons.

This project proposes the development of a framework for establishing CFRP composite laminates behavior under cyclic loading conditions. The benefit of the extended framework is visible in providing guidelines on interpretation of data for conditions other than those under which they were obtained. Reliability test data generated through the proposed experimental program is indispensable during both initial material selection and detailed engineering design stage of CFRP composite structures. The outcome of the proposed research; a validated unified methodology for assessing composite fatigue failure process by the various damage mechanisms could be directly employed for predicting structural integrity of composite parts in service and under cyclic loading. This proposed project is in-line with industry-led R&D theme in aero composite structural design and development under university-industry collaboration with the establishment of Aero structure Manufacturing Innovation Center (AMIC) in Malaysia. The significance of composite research is reflected in a continual increase of EADS/Airbus average annual sourcing in Malaysia from USD 50m in 2004-2007 to USD 120m in 2010-2012.

## **1.8 Research approach**

After that the problem is defined and the research questions, objectives, and project scope are well understood, the research will begin by referring to and exploring in previous works and other researchers` findings, firstly to get sufficient information and data about the peer works and also finding the less considered aspects of our interest.

Next, the research will be continued by establishing a systematic methodology for solving the research problem which needs to be evaluated and after that being validated.

Based on the specified methodology, the experimental and finite element simulation and analysis will be conducted and when the numerical study is validated and its accuracy is sufficient for our purpose, the results will be presented with deep analysis.

## **1.9 Structure of research**

In chapter 1, the background of the study, statement of the problem, objectives, research questions, significant of study, scope of project and research approach are described.

In chapter 2 review of the literature related to damage mechanics of composite structures and also fatigue in fiber reinforced composites as well as introduction to cohesive zone model will be covered with more details.

In Chapter 3 the author will present and evaluate the methodology used within the research. The used material, experimental and numerical techniques, specimen geometry, data acquisition approaches, theoretical frameworks used in the study, preliminary results and many more will be covered and discussed.

Chapter 4 will cover the key research findings and present detailed discussions on results with the aid of description and interpretation of acquired data, comparison and data analysis that can come to main research conclusions.

Finally, in chapter 5 conclusion and summary of results will be presented briefly



## REFERENCES

1. Harris, B. (Ed.). *Fatigue in composites, science and technology of the fatigue response of fiber-reinforced plastics*. 2<sup>nd</sup> ed. Boca Raton, USA: CRC Press. 2003
2. Haodan Jiang. *Cohesive zone model for carbon nanotube adhesive simulation and fracture/fatigue crack growth*. Doctor of Philosophy. University of Akron, USA; 2010
3. Liu, G. R. and Quek, S. S. *The Finite Element Method: A Practical Course*. 2<sup>nd</sup> edition. Oxford, UK: Butterworth-Heinemann; 2003
4. Kaw, Autar K. *Mechanics of composite materials*. (2<sup>nd</sup> ed). Boca Raton, USA: CRC Press; 2006
5. Niu, M. C. Y. *Composite Airframe Structures*. Hong Kong: Hong Kong Conmilit Press Ltd; 1992
6. Orifici, A.C., Herszberg, I. and Thomson, R.S. Review of methodologies for composite material modeling incorporating failure. *Composite Structures*, 2008, 86: 194–210.
7. Puck, A. and Schürmann, H. Failure analysis of FRP laminates by means physically based phenomenological models. *Composite Science Technology*, 1998, 58: 1045–1067.
8. Cuntze, R.G. and Freund, A. The predictive capability of failure mode concept-based strength criteria for multidirectional laminates. *Composite Science Technology*, 2004, 64: 344–377.
9. Ghaboussi, J., Pecknold, D.A., Zhang, M. and Haj-Ali R.M. Autoprogressive training of neural network constitutive models. *International Journal of Numerical Mechanical Engineerin*, 1998, 42: 105–126.

10. Rybicki, E.F. and Kanninen, M.F. A finite element calculation of stress intensity factors by a modified crack closure integral. *Engineering Fracture Mechanics*, 1977, 9: 931–938.
11. Huang, H., Springer, G.S. and Christensen, R.M. Predicting failure in composite laminates using dissipated energy. *Journal of Composite Materials*, 2006, 37(23): 2073–2099.
12. Hart-Smith, L.J. Predictions of the original and truncated maximum-strain failure models for certain fibrous composite laminates. *Composite Science Technology*, 1998, 58: 1151–1178.
13. Greszczuk, L.B. Microbuckling of lamina-reinforced composites. *Composite materials: testing and design (third conference)*. ASTM STP, 546. American Society for Testing and Materials, 5–29. 1974
14. Kim, C.H. and Yeh, H.Y. Development of a new yielding criterion: the Yeh–Stratton criterion. *Engineering Fracture Mechanics*, 1994, 47: 569–582.
15. Echaabi, J. and Trochu, F. Failure mode dependent strength criteria for composite laminates. *Journal of Reinforced Plastic Composites*, 1997, 16(10): 926–945.
16. ASTM standard. West Conshohocken, PA, "Standard terminology Relating to Fatigue and Fracture," ASTM Testing Designation E1823, 03.01, 1034.2000
17. Stephens, R.I., Fatemi A. and Fuchs H.O. *Metal fatigue in engineering*, 2<sup>nd</sup> ed. New York: John Wiley & Sons, Inc. 2001
18. Harris, B. A historical review of the fatigue behavior of fiber-reinforced plastics. In: Harris, B. (Ed.) *Fatigue in composites, science and technology of the fatigue response of fiber-reinforced plastics*, 2<sup>nd</sup> ed. Boca Raton, USA: CRC Press. 3-35; 2003
19. Howe, R.J. and Owen, M.J. Accumulation of damage in a glass-reinforced plastic under tensile and fatigue loading, in *Proceedings of the Eighth International Reinforced Plastics Congress* (British Plastics Federation, London), 1972, 137–148.
20. Green, A.K. and Pratt P.L. The shear fatigue behavior of unidirectional CFRP. *Composites* 1975, 6(6): 246-248.

21. Gusenkov, A.P., Kogaev, V.P., Berezin, A.V., Strekalov, V.B., Peshekhonov, B. A. and Zvyagin, L. K. Fatigue resistance of carbon fiber-reinforced plastics related to constructional engineering factors. *Plenum Publishing Corporation*, 1981, 289-293.
22. Bevan, L.G. Axial and short beam shear fatigue properties of CFRP laminates. *Composites* 1977, 8(7): 227-232.
23. Mao, H. and Mahadevan, S. Fatigue damage modeling of composite materials. *Composite Structures* 2002, 58: 405-410.
24. Turon, A., Camanho, P.P., Costa, J. and Davila, C.G. A damage model for the simulation of delamination in advanced composites under variable-mode loading. *Mechanics of Materials* 2006, 38: 1072-1089.
25. Benzeggagh, M.L. and Kenane, M. Measurement of mixed-mode delamination fracture toughness of unidirectional glass/ epoxy composites with mixed-mode bending apparatus. *Composite Science Technology* 1996, 49: 439-449.
26. Dugdale, D.S. Yielding of steel sheets containing slits. *Journal of the Mechanics and Physics of Solids*, 1960, 8: 100-104.
27. Barenblatt, G. The mathematical theory of equilibrium cracks in brittle fracture. *Advanced Applied Mechanics*, 1962, 7: 55-129.
28. Hillerborg, A., Modér, M. and Petersson, P.E. Analysis of crack formation and crack growth in concrete by means of fracture mechanics and finite elements. *Cement Concrete Research* 1976, 6: 773-782.
29. Borst, R., Remmers, J. and Needleman, A. Mesh-independent discrete numerical representations of cohesive-zone models. *Engineering Fracture Mechanics* 2006, 73 (2): 160-177.
30. Perales, F., Dubois, F., Monerie, Y., Piar, B. and Stainier, L.. Multi-body nscd strategy as a multi-domain solver. application to code coupling dedicated to the modeling of fracture of heterogeneous media. *European Journal of Computational Mechanics*, 2010, 19: 189-417.
31. Richefeu, V., Chrysochoos, A., Huon, V., Monerie, Y., Peyroux, R. and Wattrisse, B. Toward local identification of cohesive zone models using digital image correlation. *European Journal of Mechanics A/Solids*, 2012, 34: 38-51.

32. Chandra, N., Li, H., Shet, C. and Ghonem, H. Some issues in the application of cohesive zone models for metal-ceramic interfaces. *International Journal of Solids and Structures* 2002, 39: 2827-2855.
33. Tvergaard, V., and Hutchinson, J. The relation between crack growth resistance and fracture process parameters in elastic-plastic solids. *Journal of the Mechanics and Physics of Solids* 1992, 40: 1377-1397.
34. Alfano, G. On the influence of shape of the interface law on the application of cohesive-zone models. *Composites Science and Technology*, 2006, 66: 723-730.
35. Kubair, D., and Geubelle, P. Comparative analysis of extrinsic and intrinsic cohesive models of dynamic fracture. *International Journal of Solids and Structures* 2003, 40 (15): 3853-3868.
36. Chaboche, J., Feyel, F. and Monerie, Y. Interface debonding models: a viscoplastic regularization with a limited rate dependency. *International Journal of Solids and Structures* 2001, 38: 3127-3160.
37. Tomar, V., Zhai, J., and Zhou, M. Bounds for element size in a variable stiffness cohesive finite element model. *International Journal for Numerical Methods in Engineering*, 2004, 61 (11): 1894-1920.
38. Jiang, L.Y. A cohesive law for carbon nanotube/polymer interface accounting for chemical covalent bonds. *Mathematics and Mechanics of Solids*, 2010, 15 (7): 718-732.
39. Andena, L., Rink, M., and Williams, J.G. Cohesive zone modeling of fracture in polybutene. *Engineering Fracture Mechanics*, 2006, 73 (16): 2476-2485.
40. Hong, S., and Kim, K. Extraction of cohesive-zone laws from elastic far-fields of a cohesive crack tip: a field projection method. *Journal of the Mechanics and Physics of Solids*, 2003, 51: 1267-1286.
41. Arias, I., Knap, J., Chalivendra, V.B., Hong, S., Ortiz, M., and Rosakis, A.J. Numerical modeling and experimental validation of dynamic fracture events along weak planes. *Computer Methods in Applied Mechanics and Engineering*, 2007, 196 (37-40 SPEC. ISS.): 3833-3840.

42. Tan, H., Liu, C., Huang, Y., and Geubelle, P. The cohesive law for particle/matrix interfaces in high explosives. *Journal of the Mechanics and Physics of Solids*, 2005, 53 (8): 1892-1917.
43. Fedele, R., Raka, B., Hild, F., and Roux, S. Identification of adhesive properties in glare assemblies using digital image correlation. *Journal of the Mechanics and Physics of Solids*, 2009, 57 (7): 1003-1016.
44. Valoroso, N., and Fedele, R. Characterization of a cohesive-zone model describing damage and de-cohesion at bonded interfaces. sensitivity analysis and mode-I parameter identification. *International Journal of Solids and Structures*, 2010, 47 (13): 1666-1677.
45. Shen, B., and Paulino, G. Direct extraction of cohesive fracture properties from digital image correlation: a hybrid inverse technique. *Experimental Mechanics*, 2011, 51 (2): 143-163.
46. Zhu, Y., Liechti, K., and Ravi-Chandar, K. Direct extraction of rate-dependent traction-separation laws for polyurea/steel interfaces. *International Journal of Solids and Structures*, 2009, 46 (1): 31-51.
47. Fuchs, P., and Major, Z. Experimental determination of cohesive zone models for epoxy composites. *Experimental Mechanics*, 2011, 51 (5): 779-786.
48. Da'vila, C.G. and Camanho P.P. Analysis of the effects of residual strains and defects on skin/stiffener debonding using decohesion elements. *NASA TM-2004-211737*, Hampton VA, 2004:1-9.
49. Camanho, P.P., Da'vila, C.G., and Moura, M.F. Numerical simulation of mixed-mode progressive delamination in composite materials. *Journal of Composite Materials*, 2003, 37 (16): 1415-1438.
50. Reeder, J.R. An Evaluation of Mixed-Mode Delamination Failure Criteria. *NASA-TM 104210*, 1992: Hampton, VA.
51. Campilho, R.G., Moura, M.F. and Domingues, J.S. *International Journal of Solids and Structures*, 2007, 45: 1497.

52. Shi, Y., Swait, T., and Soutis, C. Modeling damage evolution in composite laminates subjected to low velocity impact, *Composite Structures*, 2012, 39: 1016.