ACKNOWLEDGEMENTS

My thanks go first to my project supervisors, Prof. Dr. Tharek Abdul Rahman, Dr. Razali Ngah and Prof. Peter S. Hall. Their guidance and support makes this work possible. I sincerely believe that this work would not exist without their inspiration and advices. Special thanks to Prof. Peter S. Hall and Dr. Razali Ngah, they didn't hesitate to give a fruitful advice and didn't forget to say "good job" whenever I brought an idea. The word "good job" was a great encourage to me during my research.

I wish to thank Chenghao Yuan, PhD, and Jian X. Zheng, Ph.D from Zeland software, Inc. for giving me valuable idea, guidance and much help in validating my results by Zeland software. I would also like to thank Dr. Mohd. Ramli and Dr. Sharul Kamal. Their advices and sharing experiences gave much inspiration in completing my research. Their comments on my research were very helpful for enhancing the thesis quality.

I owe special thanks to my husband, Vannebula Eka Indraguna, ST.,M.Eng. His constant encouragements, valuable suggestions, ultimately led to a more thorough were instrumental in completing this thesis. I also wish to thank Mr. Mohammed Abu Bakar for assisting me in experimental process with his patient. The warmest gratitude goes to my mother, my sisters and family, my friends and colleagues for their willingness to help with any problem that arose. Their love, lots of cares and happiness has brightened my life.

Finally, thanks to all member of wireless communication centre (WCC) that I had the pleasure working with. I can not forget the beautiful moments sharing my life with them.

ABSTRACT

A few years after the early investigation on Ultra WideBand (UWB) wireless system, considerable research efforts have been put into the design of UWB antennas and systems for communications. These UWB antennas are essential for providing wireless wideband communications based on the use of very narrow pulses on the order of nanoseconds, covering a very wide bandwidth in the frequency domain, and over very short distances at very low power densities. In this thesis, new models of T-, L- and U-slotted UWB antennas are proposed by studying their current distribution characteristics. The wideband behavior is due to the currents along the slots' edges introducing an additional resonance, which, in conjunction with the resonance of the antennas main patch. Thus, the resonances overlapping have produced an overall broadband frequency response characteristic. These antennas are considerable smaller than others listed in the references, in which their sizes are less than a wavelength, compact, and suitable for many UWB applications. The configuration of slots type for both patches and feeding strip are considered as a novelty and contribution in this thesis. The geometry of the antenna implies the current courses and makes it possible to identify active and neutral zones in the antenna, thus it will be possible to fix which elements will act on each characteristic. This thesis also investigated the ability of slotted UWB antennas to reject the interference from licensed Fixed Wireless Access (FWA), High PERformance Local Area Network (HIPERLAN) and Wireless Local Area Network (WLAN) within the same propagation environment. Inserting a half-wavelength slot structure with additional small patches gap attached have resulted frequency notched band characteristics. The small patches gap instead of switching that will be used to shortened and lengthen the slot length. The measured return loss, radiation patterns, and phase have good agreement with the simulated results. The antenna provides an omnidirectional pattern with the return loss less than -10 dB and linear in phase.

ABSTRAK

Beberapa tahun setelah penyelidikan awal pada sistem wayarles jalur ultra lebar (UWB), usaha penyelidikan telah ditumpukan pada reka bentuk antena UWB dan sistem komunikasi. Antena UWB ini sangat penting dalam penyediaan komunikasi jalur lebar berasaskan penggunaan denyut yang sangat sempit dalam kiraan nanosaat, meliputi jalur yang sangat lebar dalam domain frekuensi, dan mencakupi jarak yang sangat pendek pada ketumpatan tenaga yang sangat rendah. Dalam tesis ini, model baru antena UWB teralur-T, -L dan -U telah dicadangkan dengan mengkaji pencirian taburan arus. Perilaku jalur lebar disebabkan pada arus sepanjang tepian alur memperkenalkan satu resonan tambahan, yang mana ianya berkaitan dengan resonan antena tampal utama, sehingga pertindihan resonan menghasilkan ciri sambutan frekuensi jalur lebar menyeluruh. Antena-antena ini berukuran agak kecil bila dibandingkan dengan antena lain yang tersenarai dalam rujukan, ukurannya lebih kecil dari satu panjang gelombang, padat, dan sangat sesuai digunakan untuk pelbagai aplikasi UWB. Konfigurasi antenna jenis alur pada kedua tampal dan jalur suapan adalah asli dan boleh dianggap sebagai sumbangan dalam tesis ini. Geometri antena mempengaruhi arah arus dan dengan menentukan zon aktif dan neutral pada antenna, maka elemen yang sesuai dapat ditentukan bagi setiap karakteristik. Tesis ini juga mengkaji kemampuan antena UWB teralur untuk menolak gangguan isyarat daripada Capaian Wayarles Tetap (FWA), Rangkaian Kawasan Tempatan Berprestasi Tinggi (HIPERLAN) dan Rangkaian kawasan Tempatan Wayarles (WLAN) yang wujud dalam kawasan yang sama. Kemasukan sebuah struktur alur separuh panjang gelombang dengan penambahan sela tampal yang kecil berjaya menghasilkan ciri frekuensi jalur *notched*. Sela tampal yang kecil ini digunakan bagi mewakili suatu suis yang digunakan untuk memendekkan dan memanjangkan panjang alur. Keputusan pengujian seperti kehilangan kembali, corak sinaran dan fasa didapati menepati keputusan simulasi. Antena ini memberikan corak sinaran omni arah dengan kehilangan kembali kurang dari -10 dB dan mempunyai sambutan fasa yang lelurus.

TABLE OF CONTENTS

CHAPTER TITLE

PAGE

DECLARATIONS	ii
DEDICATION	iii
ACKNOWLEDGEMENTS	iv
ABSTRACT	v
ABSTRAK	vi
TABLE OF CONTENTS	vii
LIST OF TABLES	xii
LIST OF FIGURES	xiv
LIST OF ABREVIATIONS	xxi
LIST OF SYMBOLS	xxiii
LIST OF APPENDICES	XXV

1 INTRODUCTION

1

1.1	Introduction	1
1.2	Research Background	3
1.3	Problem Statements	6
1.4	Research Objective	8
1.5	Research Scope and Methodology	8
1.6	Thesis Outline	9

ULTRA WIDEBAND APPLICATIONS	11
TECHNOLOGY	

2

2.1	Introduction	11
2.2	UWB Definition	13
	2.2.1 Regulations Worldwide	17
2.3	A Brief History of UWB Antenna	19
2.4	Application of UWB Technology	24
	2.4.1 Communication Systems	24
	2.4.2 Radar Systems	26
	2.4.3 Positioning Systems	26
	2.4.4 UWB Over Wires	27
2.5	Short Pulse Generation	28
2.6	Summary	29

3 ULTRA WIDEBAND ANTENNA DESIGN 30 METHODOLOGY

3.1	Introc	luction	30
3.2	Funda	amental Antenna Parameter	32
	3.2.1	Radiation Pattern	32
	3.2.2	Field Region	35
	3.2.3	Directivity, Efficiency and Gain	36
	3.2.4	Voltage Standing Wave Ratio (VSWR)	37
		and Return Loss	
	3.2.5	Impedance Bandwidth	39
	3.2.6	Polarization	40
	3.2.7	Dispersion and Non Dispersion	41
3.3	UWB	Antenna Design Methodology	42

	3.3.1	Variou	is Geometries and Perturbations	42
	3.3.2	e Geneti	c Algorithm (GA)	45
	3.3.3	Reson	ance Overlapping	47
3.4	Recor	nfigurable	e UWB Antenna	47
	3.4.1	Reconfi	gurability Antenna Parameters	47
		3.4.1.1	Frequency Response	48
			Reconfigurability	
		3.4.1.2	Polarization Reconfigurability	48
		3.4.1.3	Radiation Pattern	49
			Reconfigurability	
	3.4.2	Design	Methodology	49
3.5	Theor	y Charac	teristic Modes for Planar	55
	Mono	pole Ant	ennas	
3.6	Summ	nary		56

4 SLOTTED AND RECONFIGURABLE UWB 57 ANTENNA DESIGN

4.1	Introd	luction	57
4.2	Slotte	d UWB Antenna Design Consideration	58
	4.2.1	Various Bevels and Notches	58
	4.2.2	Current Distribution Behavior	73
	4.2.3	Various Slots	82
	4.2.4	Feed Gap and Slotted Ground Plane	90
	4.2.5	Substrate Permittivity and Thickness	101
4.3	Recor	figurable Slotted UWB Antenna Design	103
	Consi	deration	
	4.3.1	Reconfigurable Modified T Slotted	104
		Antenna	

		4.3.2	Reconfigurable Modified L and U	109
			Slotted Antenna	
	4.4	Sum	mary	112
5	RES	SULTS	S AND DISCUSSIONS	113
	5.1	Introd	luction	113
	5.2	Final	Design of Slotted UWB Antenna Design	113
		and E	xperimental Verification	
		5.2.1	Simulated and Measured Return Loss	115
		5.2.2	Simulated and Measured VSWR	119
		5.2.3	Simulated and Measured Gain	120
		5.2.4	Various Slot Design	128
			5.2.4.1 Various T Slot Design	128
			5.2.4.2 Various L and U Slot Design	132
	5.3	Final	Design of Reconfigurable Slotted UWB	137
	5.4	Spher	ical Near Field Testing	143
		5.4.1	Radiation Pattern of T Slotted Antenna	145
			with Slotted Ground Plane	
		5.4.2	Radiation Pattern of L and U Slotted	151
			Antenna	
		5.4.3	Radiation Pattern of Reconfigurable T	156
			Slotted UWB Antenna	
		5.4.4	Radiation Pattern of Reconfigurable L	161
			and U Slotted Antenna	
	5.5	Estim	ating Error Analysis in Radiation Pattern	167
		Measu	urement	
	5.6	Key C	Contributions	171
	5.7	Summ	nary	172

х

6	CONCLUSIONS AND FUTURE WORKS	
	6.1 Conclusion	173
	6.2 Future Works	175
REFERENCES	References	177
APPENDICES	Appendix A - D	190

LIST OF TABLES

TABLE NO.TITLE		PAGE	
2.1	FCC limits for indoor and handheld systems	15	
2.2	UWB limits for the Singapore UFZ	19	
3.1	Proposed antenna design parameters and specifications	31	
3.2	Summarizing on existing UWB notched-band antenna	52	
4.1	The effect of notches to the simulated -10dB bandwidths	62	
	of the proposed antenna		
4.2	The effect of bevels to the simulated -10dB bandwidths	64	
	of the proposed antenna		
4.3	The effect of bevels coupling notches to the simulated -	68	
	10dB bandwidths of the proposed antenna		
4.4	Trapezoidal and pentagonal fractional bandwidth with	70	
	respect to the simulated return loss of -10dB		
4.5	The effect of smooth bevels and upper edge transition to	72	
	the simulated -10dB bandwidths of the proposed antenna		
4.6	Slot size of the slotted rectangular antenna in Figure 4.15	84	
4.7	Slot size of the slotted pentagonal antenna in Figure 4.16	85	
4.8	Simulated -10dB bandwidths of the T slotted antenna for	91	
	different feed gaps of the ground plane		
4.9	Simulated -10dB bandwidths of the L and U slotted	94	
	antenna for different feed gaps of the ground plane		
5.1	The simulated maximum gain and directivity of T slotted	121	
	antenna with slotted ground plane		
5.2	The simulated radiation properties of T slotted antenna	126	
	with slotted ground plane		

5.3	The simulated maximum gain and directivity of L and U	127
	slotted antenna	
5.4	The simulated radiation properties of L and U slotted	128
	antenna	
5.5	Near field error analysis for spherical measurement	168

LIST OF FIGURES

FIGU	RE NO. TITLE	PAGE
2.1	UWB spectral power density mask (FCC and ETSI)	14
2.2	Ultra wideband communications spread transmitting energy	16
	across a wide spectrum of frequency	
2.3	Proposed spectral mask of ECC	17
2.4	Proposed spectral mask in Asia	18
3.1	Dipole model for simulation and simulated 3D radiation	33
	pattern	
3.2	Representation plots of the normalized radiation pattern of	34
	a microwave antenna in (a) polar form and (b) rectangular	
	form.	
3.3	Field regions of antenna	35
3.4	Some wave polarization states where the wave is approaching	40
3.5	Various bevel techniques at the antenna's edge	42
3.6	Antenna design procedures	53
3.7	Antenna measurement procedures	54
4.1	Various type of polygonal monopole antennas (a) various	58
	steps notches at the bottom and (b) various bevel at the	
	bottom	
4.2	(a) Simulated return loss curves and (b) input impedance	61
	for various notches	
4.3	(a) Simulated return loss curves (b) input impedance for	63
	various bevels	
4.4	Various type polygonal monopole antennas (a) combination	65
	of notch and bevel, (b) trapezoidal and pentagonal bevels	
	and (c)smooth bevels at the bottom	

4.5	(a) Simulated return loss curves (b) input impedance for	67
	various pair bevel and notches	
4.6	(a) Simulated return loss curves (b) input impedance for	69
	trapezoidal and various pentagonal	
4.7	(a) Simulated return loss curves (b) input impedance for	71
	various transitions with smooth bevel	
4.8	Simulated comparison return loss curves for each best type	72
	of antenna	
4.9	Simulated current distribution for three model antennas	74
	with affect to the impedance bandwidth (a) rectangular (b)	
	rectangular with two notches (c) pentagonal	
4.10	Simulated return loss for three model antennas with affect	76
	to the impedance bandwidth	
4.11	Neutral zones for various frequencies of pentagonal	77
	antenna (a) 5 GHz (b) 8GHz (c) 10.5 GHz	
4.12	(a) The simulated radiation pattern for various diamond	79
	slots of pentagonal antenna at 5.25 GHz (b) the simulated	
	return loss for various diamond slots	
4.13	Neutral zones for various frequencies of rectangular with	80
	two notches antenna (a) 4.5 GHz (b) 5 GHz (c) 8 GHz	
4.14	(a) The simulated radiation pattern for various rectangular	81
	slots of rectangular antenna with two notches at 5.25 GHz	
	(b) The simulated return loss for various rectangular slots	
4.15	Various slots design of rectangular with two notches antennas	83
4.16	Various slots design of pentagonal antennas	83
4.17	The simulated return loss of various slot designs for	86
	pentagonal antennas	
4.18	The simulated return loss of various slot designs for	87
	rectangular with two notches antennas	
4.19	The simulated radiation pattern of various slot designs (a)	89
	rectangular with two notches (b) pentagonal	

4.20	Simulated return loss curves of T slotted antenna for	91
	different feed gaps	
4.21	Simulated input impedance curves of T slotted antenna for	93
	different feed gaps (a) real part and (b) imaginary part	
4.22	Simulated return loss curves of L and U slotted antenna for	94
	different feed gaps	
4.23	Simulated input impedance curves of L and U slotted	95
	antenna for different feed gaps (a) real part (b) imaginary	
	part	
4.24	Geometry of staircase slotted ground plane	96
4.25	The effect of various length slotted ground plane to the	97
	antenna performance (a) T slotted antenna (b) L and U	
	slotted antenna	
4.26	The effect of various width slotted ground plane to the	98
	antenna performance (a) T slotted antenna (b) L and U	
	slotted antenna	
4.27	The effect of various number slotted ground plane to the	100
	antenna performance (a) T slotted antenna (b) L and U	
	slotted antenna	
4.28	Simulated return loss curves of T slotted antenna for	101
	different substrate permittivity	
4.29	Simulated return loss curves of L and U slotted antenna for	102
	different substrate permittivity and thickness	
4.30	The simulated return loss of T slotted antenna with	103
	different length of patch radiator	
4.31	The reconfigurable modified T slotted antenna	105
4.32	Switching configuration for T slotted antenna: (a) notched	107
	at FWA, (b) UWB bandwidth (w/o notched), (c) notched at	
	HIPERLAN, and (d) notched at WLAN	
4.33	The simulated VSWR for reconfigurable modified T slotted	108
	antenna	

4.34	Switching configuration for L and U slotted antenna: (a)	110
	UWB bandwidth (w/o notched), (b) notched at FWA, (c)	
	notched at HIPERLAN, and (d) notched at WLAN	
4.35	The simulated VSWR for reconfigurable modified L and U	111
	slotted antenna	
5.1	The geometry and prototypes of final design for slotted	114
	UWB antennas: (a) geometry, (b) prototypes	
5.2	Measurement setup for return loss	115
5.3	The measured and simulated return loss for T slotted	117
	antenna: (a) with slotted ground plane and (b) without	
	slotted ground plane	
5.4	The measured and simulated return loss for L and U slotted	118
	antenna	
5.5	The measured and simulated VSWR for both antennas	120
5.6	The simulated maximum gain and directivity of T slotted	121
	antenna with slotted ground plane	
5.7	The measured relative gain for T slotted antenna with	122
	slotted ground plane with respect to the peak plot in the H-	
	plane: (a) 4 GHz, (b) 5.8 GHz, and (c) 10.6 GHz	
5.8	The measured relative gain for L and U slotted antenna	124
	with respect to the peak plot in the H-plane: (a) 4 GHz, (b)	
	5.8 GHz, and (c) 10.6 GHz	
5.9	The simulated antenna and radiation efficiency of T slotted	125
	antenna with slotted ground plane	
5.10	The simulated maximum gain and directivity of L and U	126
	slotted antenna	
5.11	The simulated antenna and radiation efficiency of L and U	127
	slotted antenna	
5.12	The simulated current distribution for T slotted with slotted	129
	ground plane antenna: (a) 3 GHz, (b) 5.5 GHz, and (c) 9	
	GHz	
5.13	The simulated return loss of various T slots design for T	130
	slotted with slotted ground plane antenna	

5.14	The simulated return loss of various width of T slots design	130
5.15	The simulated current distribution on the antenna by	131
	varying its height of T slot on the patch radiator for	
	different frequency: (a) both length 3 mm, (b) both length 5	
	mm, and (c) length 4 and 3mm	
5.16	The simulated return loss of various heights for upper T	132
	slot	
5.17	The simulated current distribution of 3, 6, and 9 GHz for L	133
	and U slotted antenna	
5.18	The simulated return loss of various L and U slots design	134
	for L and U slotted antenna	
5.19	The simulated return loss of various width of L and U slots	135
	design	
5.20	The simulated current distribution on the antenna by	136
	varying its length of L and U slot on the patch radiator for	
	different frequency: (a) vary L, (b) vary U, and (c) vary	
	both L and U	
5.21	The simulated return loss of L and U slotted antenna with	137
	different length slot	
5.22	Three prototypes of T slotted antennas with notched band at	138
	FWA (left), notched at HIPERLAN (middle) and notched	
	at WLAN (right): (a) geometry of reconfigurable T slotted	
	antenna and (b) photograph of prototype	
5.23	The measured VSWR for the three prototypes of modified	139
	T slotted antenna	
5.24	The measured phase for modified T slotted antenna	140
5.25	Three prototypes of modified L and U slotted antenna for	141
	band notched at FWA (left), at HIPERLAN (middle) and at	
	WLAN (right): (a) geometry and (b) photograph	
5.26	The measured VSWR for L and U slotted antenna	142
5.27	The measured phase of L and U slotted antenna with	143
	HIPERLAN notched band	

5.28	The radiation pattern measurement setup inside the	144
5.00		1.4.5
5.29	Coordinate system for typical spherical near-field rotator	145
	system	
5.30	The measured and simulated E and H planes at 4 GHz: (a)	147
	measured and simulated E-planes and (b) measured and	
	simulated H-planes	
5.31	The measured and simulated E and H planes at 5.8 GHz:	148
	(a) measured and simulated E-planes and (b) measured and	
	simulated H-planes	
5.32	The measured and simulated E and H planes at 10.6 GHz:	149
	(a) measured and simulated E-planes and (b) measured and	
	simulated H-planes	
5.33	The measured 3D radiation pattern: (a) 4 GHz and (b) 5.8	150
	GHz	
5.34	The measured 3D radiation pattern at 10.6 GHz: (a) side	151
	view and (b) top view	
5.35	The measured and simulated E and H planes at 4 GHz: (a)	152
	measured and simulated E-planes and (b) measured and	
	simulated H-planes	
5.36	The measured and simulated E and H planes at 5.8 GHz:	153
	(a) measured and simulated E-plane and (b) measured and	
	simulated H-planes	
5.37	The measured and simulated E and H planes at 10.6 GHz:	154
	(a) measured and simulated E-planes and (b) measured and	
	simulated H-planes	
5.38	The measured 3D radiation pattern: (a) 4 GHz (b) 5.8 GHz	155
5.39	The measured 3D radiation pattern at 10.6 GHz	156
5.40	The measured and simulated E and H-planes for T slotted	157
	antenna notched at FWA: (a) 4 GHz and (b) 5.8 GHz	
5.41	The measured and simulated E and H planes for T slotted	158
	antenna notched at HIPERLAN: (a) 4 GHz and (b) 5.8 GHz	

5.42	The measured and simulated E and H planes for T slotted	159
	antenna notched at WLAN: (a) 4 GHz and (b) 5.8 GHz	
5.43	The measured 3D radiation patterns for T slotted notched	160
	band antenna: (a) band notched at FWA and (b) band	
	notched at HIPERLAN	
5.44	The measured 3D radiation patterns for T slotted notched	161
	band at WLAN	
5.45	The measured and simulated E and H planes for L and U	162
	slotted notched antenna at FWA (a) 4 GHz and (b) 5.8 GHz	
5.46	The measured and simulated E and H planes for L and U	163
	slotted antenna notched at HIPERLAN: (a) 4GHz and (b)	
	5.8 GHz	
5.47	The measured and simulated E and H planes for L and U	164
	slotted antenna notched at WLAN: (a) 4 GHz and (b)	
	5.8 GHz	
5.48	The measured 3D radiation patterns for L and U slotted	165
	antenna notched band at FWA: (a) 4 GHz and (b) 5.8 GHz	
5.49	The measured 3D radiation patterns for L and U slotted	166
	antenna notched band at HIPERLAN: (a) 4 GHz and (b)	
	5.8 GHz	
5.50	The measured 3D radiation patterns for L and U slotted	167
	antenna notched band at WLAN: (a) 4 GHz and (b) 5.8	
	GHz	
5.51	An Example of results of random errors for L and U slotted	169
	antenna at 5.8 GHz	

LIST OF ABBREVIATIONS

AUT	Antenna Under Test
CEPT	Conference of European Posts and Telecommunications
CATV	Cable Television
DS-UWB	Direct Sequence Ultra Wideband
DAA	Detect and Avoid
DC	Direct Current
ETSI :	European Telecommunications Standard Institute
ECC :	Electronic Communications Committee
ETRI	Electronics and Telecommunications Research Institute
FCC	Federal Communication Committee
FWA	Fixed Wireless Access
FDTD	Finite Difference Time Domain
FR4	Flame Resistant 4
GPS	Global Positioning System
HIPERLAN	High Performance Local Area Network
H-cut	Horizontal cut
IEEE	Institute of Electrical and Electronics Engineers
IDA	Infocomm Development Authority
IR	Impulse Radio
MIC	Ministry of Internal Affairs and Communications
MB	Multi Band
MCMC	Malaysian Communications and Multimedia Commissions
OFDM	Orthogonal Frequency Division Multiplexing
PDA	Personal Digital Assistance
PCB	Printed Circuit Board
RCS	Radar Cross Section

RF	Radio Frequency
SMA	SubMiniature version A
SRR	Split Ring Resonator
SB	Single Band
TEM	Transverse Electric Magnetic
TDMA	Time Division Multiple Access
UFZ	UWB Friendly Zone
UWB	Ultra Wideband
VSWR	Voltage Standing Wave Ratio
V-cut	Vertical cut
WPAN	Wireless Personal Area Network
WLAN	Wireless Local Area Network

LIST OF SYMBOLS

BW	Bandwidth
$f_{\rm H}$	High frequency
f_L	Low frequency
$\mathbf{f}_{\mathbf{C}}$	Centre frequency
dBm	Mili decibel
MHz	Megahertz
GHz	Gigahertz
P _{RX}	Antenna received power
P _{TX}	Antenna transmitted power
G _{TX}	Transmit antenna gain
G _{RX}	Receive antenna gain
А	Aperture
c	Speed of light
θ	Theta angle
φ	Phi angle
e _r	Reflection efficiency
P _{rad}	Radiated power
P _{in}	Input power
χn -	Eigenvalue
J _n	Characteristic modes
Ws	Slot width
ls	Slot length
r	Radius
λ	Wavelength
S ₁₁	Return loss
R _e	Real part

Im	-	Imaginary part
ε _r		Relative permittivity
E-plane		Electric plane
H-plane		Magnetic plane

LIST OF APPENDICES

APPENDIX

TITLE

PAGE

А	List of author's publication	190
В	Comparison between proposed UWB antennas with	192
	existing UWB antenna in terms of size and other	
	important specifications	
С	EM numerical modeling technique	193
D	Spectrum Plan	206

CHAPTER 1

INTRODUCTION

1.1 Introduction

Ultra Wideband (UWB) is currently receiving special attention and is quite a hot topic in industry and academia. UWB short-range wireless communication is different from a traditional carrier wave system. UWB waveforms are short time duration and have some rather unique properties. The benefits of UWB technology are derived from its unique characteristics that are the reasons why it presents a more eloquent solution to wireless broadband than other technologies. The unique characteristics are listed below [1].

Firstly, an inherent capability for integration in low cost, low power Integrated Circuit (IC) processes. UWB system based on impulse radio features low cost and low complexities which arise from the essentially base-band nature of the signal transmission. UWB does not modulate and demodulate a complex carrier waveform, so it does not require components such as mixers, filters, amplifiers and local oscillators.

Secondly, UWB has an ultra-wide frequency bandwidth; it can achieve huge capacity as high as hundreds of Mbps or even several Gbps with distances from 1 to 10 meters [2]. Thus, the UWB is a promising technology for Wireless Personal Area Network (WPAN). In recent years, more interests have been put into WPAN technology worldwide. The future WPAN aims to provide reliable wireless connections between computers, portable devices and consumer electronics within a

short range. Furthermore, fast data storage and exchange between these devices will also be accomplished. This requires a data rate which is much higher than what can be achieved by existing wireless technologies.

Thirdly, UWB system is extremely fine time and range solution even through lossy, opaque media. And fourthly, UWB system has immunity from multipaths.

Fifthly, non-interfering operation with existing services. In spreading signals over very wide bandwidths, the UWB concept is especially attractive since it facilitates optimal sharing of a given bandwidth between different systems and applications. UWB systems are highly frequency adaptive, enabling them to be positioned anywhere within the RF spectrum. This feature avoids interference to existing services, while fully utilizing the available spectrum. UWB systems operate at extremely low power transmission levels. Therefore, UWB short-range radio technology complements other longer-range radio technologies such as Wireless Fidelity (WiFi), Worldwide Interoperability for Microwave Access (WiMAX), and cellular wide area communications.

Lastly, UWB has low probability of detection and interception. UWB provides high secure and high reliable communication solutions. Due to the low energy density, the UWB signal is noise-like, which makes unintended detection quite difficult. Furthermore, the "noise-like" signal has a particular shape; in contrast, real noise has no shape. For this reason, it is almost impossible for real noise to obliterate the pulse because interference would have to spread uniformly across the entire spectrum to obscure the pulse. Interference in only part of the spectrum reduces the amount of received signal, but the pulse still can be recovered to restore the signal. Hence UWB is perhaps the most secure means of wireless transmission ever previously available [3].

As with any technology, there are always applications that may be better served by other approaches. For example, for extremely high data rate (10's of Gigabits/second and higher), point-to-point or point-to-multipoint applications, it is difficult today for UWB systems to compete with high capacity optical fiber or optical wireless communications systems. The high cost associated with optical fiber installation and the inability of an optical wireless signal to penetrate a wall dramatically limits the applicability of optically-based systems for in-home or inbuilding applications. In addition, optical wireless systems have extremely precise pointing requirements, obviating their use in mobile environments.

1.2 Research Background

The UWB technology has experienced many significant developments in recent years. However, there are still challengers in making this technology live up to its full potential. One particular challenge is the UWB antenna design. UWB technology has had a substantial effect on antenna design. The UWB antennas have to be able to transmit pulses as accurately and efficiently as possible. The spectrum allocated certainly requires transmitters and receivers with wideband antennas.

Through literature survey, there are two vital design considerations in UWB radio systems. One is radiated power density spectrum shaping must comply with certain emission limit mask for coexistence with other electronic systems [4]. Another is that the design source pulses and transmitting/receiving antennas should be optimal for performance of overall systems [5]. Emission limits will be crucial considerations for the design of source pulses and antennas in UWB systems.

The main challenge in UWB antenna design is achieving the extremely wide impedance bandwidth while still maintaining high radiation efficiency. By definition, an UWB antenna must be operable over the entire 3.1 GHz - 10.6 GHz frequency range [4]. Therefore, the UWB antenna must achieve almost a decade of impedance bandwidth, spanning 7.5 GHz. The high radiation efficiency is also required especially for UWB applications to ensure the transmit power spectral density requirement achieved. Conductor and dielectric losses should be minimized in order to maximize radiation efficiency. High radiation efficiency is imperative for an UWB antenna because the transmit power spectral density is excessively low. Therefore, any excessive losses incurred by the antenna could potentially compromise the functionality of the system. Next, the performance of UWB antenna is required to have a constant group delay. Group delay is given by the derivative of the unwrapped phase of an antenna. If the phase is linear throughout the frequency range, the group delay will be constant for that frequency range. This is an important characteristic because it helps to indicate how well a UWB pulse will be transmitted and to what degree it may be distorted or dispersed. The antennas required to have a non-dispersive characteristic in time and frequency, providing a narrow, pulse duration to enhance a high data throughput. It is also a parameter that is not typically considered for narrowband resonance.

In addition, a nearly omni-directional radiation pattern is desirable in that it enables freedom in the receiver and transmitter location. This implies maximizing the half power beam-width and minimizing directivity. It is also highly desirable that the antenna feature low profile and compatibility for integration with Printed Circuit Board (PCB) [6].

A good design of UWB antenna should be optimal for the performance of overall system. For example, the antenna should be designed such that the overall device (antenna and Radio Frequency (RF) front end) complies with the mandatory power emission mask given by the Federal Communication Committee (FCC) or other regulatory bodies [6]. But not the least important, a UWB antenna is required to achieve good time domain characteristics. Minimum pulse distortion in the received waveform, is a primary concern of a suitable UWB antenna because the signal is the carrier of useful information. For the narrow band case, it is approximated that an antenna has same performance over the entire bandwidth and the basic parameters, such as gain and return loss, have little variation across the operational band.

Today the state of the art of UWB antennas focuses in the microstrip, slot and planar monopole antennas with different matching techniques to improve the bandwidth ratio without loss of its radiation pattern properties [7]. The expected antennas are small size, omni directional patterns, and simple structure that produce low distortion but can provide large bandwidth [8]. In the past, one serious limitation of microstrip antennas was the narrow bandwidth characteristic, being 15% to 50% that of commonly used antenna elements such as dipoles, and slots [9]. This limitation was successfully removed achieving a matching impedance bandwidth of up 90%. To increase the matching impedance bandwidth ratio it was necessary to increase the size, height, volume or feeding and matching techniques [10]. Variety of matching techniques have been proposed in the literature reviews, such as the use of slot [11][12], bevel or taper at the bottom of patch [13], notch and partial ground plane [12]. There is a growing demand for small and low cost UWB antennas that can provide satisfactory performances in both frequency domain and time domain.

The planar monopole antennas are promising antennas for UWB applications due to their simple structure, low profile, easy to fabricate and UWB characteristics with nearly omni-directional radiation patterns [6][14][15]. Planar monopole antennas feature broad impedance bandwidth but somewhat suffer high crosspolarization radiation levels. The large lateral size or asymmetric geometry of the planar radiator causes the cross-polarized radiation. Fortunately, the purity of the polarization issue is not critical, particularly for the antennas used for portable devices [16]. There are several UWB planar antenna designs, including planar halfdisk antenna [17], planar horn antenna [18], and metal plate antenna [19], have been reported.

Even though UWB is recommended by the FCC of United States (U.S) to operate with maximum in-band effective incident radiated power of -41.3 dBm/MHz within the band from 3.1 GHz to 10.6 GHz, there were tremendous complaints logged against UWB deployment so far [20]. Evaluation of interference between Multiband Orthogonal Frequency Division Multiplexing (MB-OFDM) UWB and Wireless Local Area Network (WLAN) systems using a Gigahertz Transverse Electromagnetic (GTEM) cell has been proposed in [21]. As a result, when the frequencies of the MB-OFDM UWB corresponded to out-of-band radiation for 11a (Band #3), MB-OFDM UWM did not interfere with the WLAN system. In the other hand, when frequencies of the MB-OFDM UWB corresponded to in-band radiation for 11a (Band #4), although the interference power of MB-OFDM UWB was less than receiver noise, the MB-OFDM UWB systems interfered with the WLAN. Evaluation of interference between Direct Sequence spread spectrum UWB (DS-UWB) and WLAN systems using a GTEM cell has already been presented a year before in [22]. Even if the UWB signal is smaller than the receiver noise of WLAN, the throughput characteristics deteriorate than those in case of the non-interference [22]. Therefore, recently the consideration of UWB antennas is not only focused on an extremely wide frequency bandwidth, but on the ability of rejecting the interference from WLAN 11.a (5725 - 5825 MHz) and High Performance Local Area Network (HIPERLAN) (5150 - 5350 MHz) within the same propagation environment [23].

To avoid the interference between the UWB, WLAN and HIPERLAN systems, a band-notch filter in UWB systems is necessary. However, the use of a filter will increase the complexity of the UWB systems [24]. One of the solutions proposed, as far as antennas are concerned, was to design frequency notched antenna. Therefore, several techniques used to introduce a notched band for rejecting the WLAN and HIPERLAN interference have been investigated, which include such as inserting a half-wavelength slot structure [23][25]-[29], slitting on the edges [30]-[31], utilizing fractal feeding structure [32], and parasitic quarter-wave patch [33] or parasitic open-circuit stub [34]. With the notched band characteristic, the antenna allows to reconfigurable its frequency that only responsive to other frequencies beyond the rejection bands within UWB bandwidth.

1.3 Problem Statements

One of the critical issues in this UWB antenna design is the size of the antenna for portable devices, because the size affects the gain and bandwidth greatly [35]. Therefore, to miniaturize the antennas capable of providing ultra wide bandwidth for impedance matching and acceptable gain will be a challenging task [5]. Planar monopole is used to reduce the size of the proposed antennas. Some novelty UWB planar monopole antennas are investigated in detail in order to understand their operations; find out the mechanism that leads to UWB

characteristics and to obtain some quantitative guidelines for designing of this type of antennas.

In order to obtain the ultra wide bandwidth and omni directional radiation pattern, four matching techniques are applied to the proposed UWB antennas, such as the use of slots, the use of bevels and notches at the bottom of patch, the truncation ground plane, and the slotted ground plane. All these techniques are applied to the small UWB antenna without degrading the required UWB antenna's performance. The size of slots, bevels and notches are critically affect to the impedance bandwidth. The distance between truncation ground plane to the bottom of the patch is as matching point, where it determines the resonance frequency. To ensure the broad bandwidth can be obtained, the proper designs on those parameters are required.

The theory characteristic modes are used to design and optimize the proposed UWB antennas as well as some new designs are studied. From the study of the behavior of characteristic modes, important information about the resonant frequency and the bandwidth of an antenna can be obtained. The current behaviors of the antenna are investigated in order to obtain several new slotted UWB antennas. High radiation efficiency and linear phase are also required.

A licensed Fixed Wireless Access (FWA) for point to multipoint radio systems assigned by Malaysian Communications and Multimedia Commissions (MCMC) for 3.4 to 3.7 GHz is considered giving a potential interference to UWB application. This is due to the allocation frequency for this FWA within the UWB range. Thus, the proposed notched antenna is not only designed to reject interference from WLAN, HIPERLAN but also from FWA. In order to meet the goal, the previous designed UWB slotted antenna is chosen as a basic type of reconfigurable slotted UWB antennas. This is due to the slot antennas are good candidate to meet the needs for UWB communication and antenna size reduction due to their compact and broadband. To design this reconfigurable UWB slotted antenna with three notched bands characteristics by using a simple structure of antenna is very challenging task. In this thesis, this antenna is known as reconfigurable UWB slotted antenna. The reconfigurability characteristic means the ability of UWB slotted antenna to reject certain frequencies by using some small gaps, instead of switches, without any degrading the radiation pattern. The controllable slot length by the gaps is intended to reject the required frequencies.

Finally, two types of UWB antennas have been designed and resulted in this thesis. The first is slotted antenna type for general UWB applications. The second is reconfigurable UWB slotted antenna. This second type of antenna is used to reject the interference from existing wireless communication systems within the UWB range such as FWA, HIPERLAN, and WLAN bands. However this is still the newest issue, the existing publications mostly on UWB antenna with notched bands on HIPERLAN/WLAN bands. This thesis is working with an additional notched on FWA band in order to give contribution in UWB antenna development.

1.4 Research Objective

The main objective of this research is to propose small novel types of antennas for UWB applications. The proposed antennas operate over UWB bandwidth (3.1 - 10.6 GHz) and have capability to reconfigurable their frequency to a narrower bandwidth while rejecting from interference from existing FWA, HIPERLAN, and WLAN bands with band notched characteristics.

1.5 Research Scope and Methodology

The research scope is focused on slotted UWB antennas designs which provide an ultra wide bandwidth. Truncation ground plane and notches/bevels techniques are added to improve the impedance matching. The reconfigurability antennas characteristics are achieved by varying the length of slots with on/off the small gaps, instead of switches. In order to achieve the objective, a number of activities have been identified, as outline below:

- i. Investigate characteristics of UWB antenna by means of simulation and numerical analysis.
- ii. Simulate the UWB antenna design model using antenna simulation software before the actual prototype built.
- iii. Integrate some small gaps into the proposed antenna to evaluate the reconfigurable characteristics performance.
- iv. Develop a new design prototype of reconfigurable UWB antenna.
- v. Antenna performance evaluation and optimization.

1.6 Thesis Outline

The thesis is divided into six chapters. Following is an introductory chapter that defines the importance of this research, objective, and scope. The introduction of UWB technology, the challenges in UWB antenna design, the UWB notched band characteristics and the current issues are also highlighted. The review of UWB applications technology is given in Chapter 2. This chapter begins by the UWB history and definition of UWB signal with some international standardization on it. A wide variety of wideband antennas are presented as well. Some applications applied for this UWB technology such as communication system, radar system and positioning system are discussed. With UWB techniques, it becomes feasible to fuse these unique capabilities into a single system. The review of UWB antenna with notched band characteristics with capability to reject interference generated between other communication systems is presented. Finally, overview of short pulse generation is discussed.

The literature review examined a comprehensive background of other related research works and the fundamental antenna parameters that should be considered in designing UWB antenna, and potential technologies for physical construction given in Chapter 3. Design methodology applied in this proposed UWB antenna and reconfigurable UWB antenna is discussed in detail. The key differences and considerations for UWB antenna design are also discussed in depth as several antennas are presented with these considerations in mind. Several bandwidth enhancement techniques such as various geometry perturbation and Genetic Algorithm will be highlighted in order to obtain optimization in size and performance.

Chapter 4 elaborates on the design methodology mentioned in the previous sections. Some new novelty slotted UWB antennas and reconfigurable UWB antennas are presented and design requirements, general strategy for the design are discussed in detail. By properly design the slots and gaps have provided band notched characteristics at 3.4 to 3.7 GHz and 5.150 to 5.850 GHz. The novelty is in term of the type of slots used and it is considered as a contribution in this thesis.

Chapter 5 presents the results and discussion. Simulated and measured results are compared. The experimental verification process is explained with numerical analysis given. The key contributions in this thesis are highlighted. Finally, some recommendations on further work as well as a concluding statement are given in Chapter 6.