



## ORIGINAL ARTICLE

# Entropy analysis of magnetized ferrofluid over a vertical flat surface with variable heating



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Nanofluid;  
 Entropy generation;  
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 Finite difference method

**Abstract** This research analyzes the entropy generation in a two-dimensional flow of magnetized ferrofluid with variable wall temperature in the presence of heat generation. The mathematical model is designed to consolidate cylindrical-shaped  $\text{Fe}_3\text{O}_4$ -nanoparticles in pure water. An implicit finite difference is used to obtain the desired numerical solutions. The effects of nanoparticle volume concentration, magnetic parameter, heat generation, and power index on fluid velocity, temperature, entropy generation, and Bejan number are illustrated graphically. The entropy generation increased when the Brinkmann number increased; however, it decreased when the temperature difference decreased. For the authenticity of the current research, the obtained findings are compared with the previously existing results under certain conditions, and a good coexistence is achieved.

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## 1. Introduction

Numerous industrial and technical fields are using nanotechnology because it plays a leading role in advanced technologies. Nanotechnology depends on the capacity to create, manipulate, and fabricate materials at the nanoscale, and nanomaterials are the name given to these materials. The contribution of nanomaterials in enhancing the heat transfer

mechanism is appreciable. On the other hand, the thermal conductivity of traditional heat transfer fluid is inadequate to acquire the desired heat transfer rates. Therefore, researchers are using nanoparticles to increase the thermal efficiency of heat transfer fluids. The mixture of nanoparticles and fluid is called nanofluid, introduced by Choi and Eastman [1]. Several studies have been performed on convective heat transfer fluid flow using nanomaterials over the past few decades [2–7]. Nanofluids with superparamagnetic nanoparticles are named ferrofluids. These are frequently known as functional and valuable fluids in which a magnetic field is applied to fluid flow, thereby improving the carrier fluid's thermal performance. Because of their potential use in the process of heat transmission, they have attracted a lot of study attention. Pattnaik

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et al. [8] noticed an increment in the temperature of  $\text{Fe}_3\text{O}_4$ /water ferrofluid due to the radiative heat energy emitted by the particle. In a study, Hanif et al. [9] observed that heat transfer rates of  $\text{Fe}_3\text{O}_4$ /water are higher than Cu/water in the presence of heat absorption. The flow of  $\text{Fe}_3\text{O}_4$ /water ferrofluid between two spinning surfaces has been studied by Shahzad et al. [10]. During the study, they found that heat transfer rates increase dramatically for the  $\text{Fe}_3\text{O}_4$ /water compared to the conventional fluid as the concentration of nanoparticles increases. We also refer to some investigations considering ferrofluid [11–13].

Heat transfer phenomena in the presence of a magnetic field have numerous applications in several industries, including manufacturing and engineering, such as crystal growth, paper production, polymer extrusion, artificial fibers, plastic films, etc. Due to these significant applications, magnetohydrodynamics (MHD) in heat transfer owned special attention from researchers and engineers. Several research studies have been conducted to explore the influence of a magnetic field on the heat transfer characteristics of conventional fluids. Hanif and Shafie investigated MHD Maxwell fluid in the presence of Joule heating and viscous dissipation [14,15]. Their results showed that the magnetic field causes a downturn in the velocity but increases the temperature. Pattnaik et al. [16] analyzed the MHD flow of Au/water in a permeable channel. Saqib et al. [17] utilized the Cattaneo-Friedrich concept to analyze the influence of inclined MHD Flow of Maxwell fluid. Some fruitful articles on MHD flow are present in [18–20].

In recent years, it has proven possible to create the best engineering system designs by limiting entropy formation using the second law of thermodynamics. Entropy generation is a unit of measurement for the amount of irreversibility that builds up throughout a process. Entropy generation may therefore be a metric for assessing the performance of engineering devices [21]. Numerous forms of irreversibility contribute to entropy generation, including temperature gradient, fluid frictions, and convective heat transfer qualities. Entropy analysis is famous in various sectors, including spinning reactors, heat transfer equipment, nuclear fuel rod cooling, and solar energy collectors. For instance, Khosravi et al. [22] used neural networks to analyze the entropy production of hybrid nanofluid flow in a wavy microchannel solar receiver. Marzougui et al. [23] calculated the irreversibility of convective nanofluid flow in the presence of a magnetic field in a cavity with chamfers. A depletion in viscous and thermal entropy generation occurred for an increased Hartmann number with a fixed angle of inclination of the magnetic field. Jamshed [24] noticed an exaggerated entropy in MHD Maxwell nanofluid on adding nanoparticles. Tayebi et al. [25] investigated the irreversibility of MHD nanofluid flow between two differentially heated circular cylinders. Their results showed that irreversibility due to thermo-effects is prominent for low Rayleigh numbers. Moreover, the irreversibility due to thermo-effects is no longer the main contributor to total entropy generation when Rayleigh values increase. Nakhchi and Rahmati [26] explored the effects of transverse-cut twisted tapes on the thermal properties and entropy generation of Cu/water nanofluid within a uniform-wall heat exchanger. Jamshed et al. [27] analyzed entropy generation in a second-grade fluid and noticed an incredible increment in entropy due to Reynolds and Brinkman numbers. Contemporary

works on convective heat transfer and entropy generation problems in different configurations can be found in [28–30].

The main objective of this investigation is to examine the irreversibility problem in nanofluid flow in the presence of a magnetic field. Numerous scholars have highlighted the irreversibility of MHD fluid flow. But unsteady flow problems have been frequently disregarded. Further, solving time-dependent partial differential equations (PDEs) using similarity transformations is common, but solving PDEs is rare. Therefore, the present research analyzes the irreversibility process in an unsteady nanofluid flow using the finite difference method. It is worth mentioning the thermal and mechanical properties of a nanofluid depend on the selection of base fluid, volume concentration, type, size, and shape of nanoparticles. Even though the most common particles are spherical nanoparticles, they are insubstantial in terms of significance and applications. As a consequence, the cylindrical nanoparticles have been integrated with the current study. The novelty of the research increased by considering the effects of a magnetic field and heat generation.

## 2. Problem description

A convective heat transfer in magnetized  $\text{Fe}_3\text{O}_4$ /water ferrofluid with uniform velocity  $u_0$  is considered. The surface of the geometry is taken as  $x$ -axis, and  $y$ -axis is assumed in the normal direction to the flow. A uniform-magnetic field  $B = (0, B_0, 0)$  is applied normal to the flow direction, see Fig. 1. The flow is initiated with wall temperature  $T_w(x)$  in the presence of heat generation  $Q_0$ . If  $(u(x, y, t), v(x, y, t))$  be the velocity components in  $(x, y)$  directions and  $T(x, y, t)$  is the temperature then the governing equations using boundary layer and Boussinesq approximations are given as

$$u_x + v_y = 0, \quad (1)$$

$$\rho_{nf}(u_t + uu_x + vv_y) = \mu_{nf}u_{yy} - \sigma_{nf}B_0^2u + g(\rho\beta)_{nf}(T - T_\infty), \quad (2)$$

$$(\rho C_p)_{nf}(T_t + uT_x + vT_y) = k_{nf}T_{yy} + Q_0(T - T_\infty). \quad (3)$$

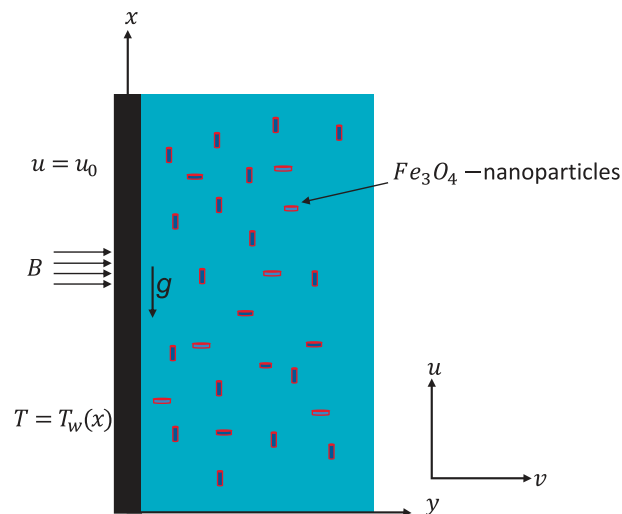


Fig. 1 Graphical representation.

The mathematical expression for nanofluid properties including density  $\rho_{nf}$ , dynamic viscosity  $\mu_{nf}$ , thermal expansion  $\beta_{nf}$ , heat capacity at constant pressure  $(C_p)_{nf}$ , thermal conductivity  $k_{nf}$  and electrical conductivity  $\sigma_{nf}$  are given Table 1 and the thermo-physical properties of base fluid and nanoparticles are depicted in Table 2.

The initial and boundary conditions are given as below:

$$\begin{aligned} t \leq 0 : \quad & u(x, y, t) = v(x, y, t) = 0, T(x, y, t) = T_\infty, \\ t > 0 : \quad & u(x > 0, 0, t) = u_0, v(x, 0, t) = 0, T(x, 0, t) = T_\infty + c\chi^n, \\ & u(0, y, t) = u(x, \infty, t) = 0, T(0, y, t) = T(x, \infty, t) = T_\infty. \end{aligned} \quad (4)$$

Using the following non-dimensional quantities:

$$x^* = \frac{xu_0}{v_f}, \quad y^* = \frac{yu_0}{v_f}, \quad t^* = \frac{tu_0^2}{v_f}, \quad u^* = \frac{u}{u_0}, \quad v^* = \frac{v}{u_0}, \quad T^* = \frac{T - T_\infty}{T_w - T_\infty}. \quad (5)$$

into Eqs. 1, 2 and 3, gives us (for the sake of simplicity \* is removed)

$$u_x + v_y = 0, \quad (6)$$

$$\phi_1 [u_t + uu_x + vv_y] = \phi_2 u_{yy} - \phi_3 Mu + \phi_4 Ri Re^{-1} T, \quad (7)$$

$$\phi_5 [T_t + uT_x + vT_y] = \phi_6 Pr^{-1} T_{yy} + QT, \quad (8)$$

where

$$\begin{aligned} \phi_1 &= (1 - \varphi) + \varphi \frac{\rho_s}{\rho_f}, & \phi_2 &= 1 + 13.5\varphi + 904.4\varphi^2, & \phi_3 &= \frac{\sigma_{nf}}{\sigma_f}, \\ \phi_4 &= (1 - \varphi) + \varphi \frac{(\rho\beta)_s}{(\rho\beta)_f}, & \phi_5 &= (1 - \varphi) + \varphi \frac{(\rho C_p)_s}{(\rho C_p)_f}, & \phi_6 &= \frac{k_{nf}}{k_f}, \\ M &= \frac{B_0^2 \sigma_{nf}}{\rho_f \mu_0^2}, & Ri &= \frac{g\beta_f(T_w - T_\infty)L}{u_0^2}, & Re &= \frac{u_0 L}{\mu_f}, \\ Pr &= \frac{\nu_f}{\alpha_f}, & \alpha_f &= \frac{k_f}{(\rho C_p)_f}, & Q &= \frac{Q_0 \nu_f}{(\rho C_p)_f \mu_0^2}. \end{aligned} \quad (9)$$

Here  $\phi_1 - \phi_6$ ,  $M$ ,  $Ri$ ,  $Re$ ,  $Pr$ ,  $\alpha$  and  $Q$  denote the nanofluid constants, magnetic parameter, Richardson number, Reynolds number, Prandtl number, thermal diffusivity, and heat gener-

ation/absorption parameter, respectively. The initial and boundary conditions are given below:

$$\begin{aligned} t \leq 0 : \quad & u(x, y, t) = v(x, y, t) = 0, T(x, y, t) = 0, \\ t > 0 : \quad & u(x > 0, 0, t) = 1, v(x, 0, t) = 0, T(x, 0, t) = x^n, \\ & u(0, y, t) = u(x, \infty, t) = 0, T(0, y, t) = T(x, \infty, t) = 0. \end{aligned} \quad (10)$$

### 3. Entropy generation analysis

The entropy generation model for nanofluid with a magnetic field can be described as

$$S_{gen} = \frac{k_{nf}}{T_\infty^2} \left( \frac{\partial T}{\partial y} \right)^2 + \frac{\mu_{nf}}{T_\infty} \left( \frac{\partial u}{\partial y} \right)^2 + \frac{\sigma_{nf} B^2}{T_\infty} u^2. \quad (11)$$

The non-dimensional entropy generation  $S_{GEN}$  is described as proportion of the volumetric entropy generation ( $S_{gen}$ ) to the characteristic entropy rate ( $S_0$ ). Mathematically

$$S_{GEN} = \frac{S_{gen}}{S_0} = \phi_6 \left( \frac{\partial T}{\partial y} \right)^2 + \phi_2 Br \Omega^{-1} \left( \frac{\partial u}{\partial y} \right)^2 + \phi_3 Br \Omega^{-1} Mu^2, \quad (12)$$

given that

$$\begin{aligned} S_0 &= \frac{k_f(T_w - T_\infty)^2 u_0^2}{T_\infty \nu_f^2} \quad (\text{Characteristic entropy generation}), \\ Br &= \frac{\mu_f u_0^2}{k_f(T_w - T_\infty)} \quad (\text{Brinkmann number}), \\ \Omega &= \frac{T_w - T_\infty}{T_\infty} \quad (\text{Temperature difference}). \end{aligned} \quad (13)$$

Let  $N_1$  and  $N_2$  represent the irreversibility due to heat transport and fluid friction, respectively, then Eq. 12 takes the form

$$S_{GEN} = N_1 + N_2, \quad (14)$$

provided that

$$N_1 = \phi_6 \left( \frac{\partial T}{\partial y} \right)^2, N_2 = \phi_2 Br \Omega^{-1} \left( \frac{\partial u}{\partial y} \right)^2 + \phi_3 Br \Omega^{-1} Mu^2. \quad (15)$$

The Bejan number ( $Be$ ) is valuable for evaluating irreversibility distribution. It is a ratio of entropy generation due to heat transfer to overall entropy generation

$$Be = \frac{N_1}{N_1 + N_2}. \quad (16)$$

The Bejan number range is [0,1],  $Be = 0$  indicates that  $N_1$  is defeated by  $N_2$  and  $Be = 1$  shows that  $N_1$  is dominated by  $N_2$ . If the entropy generated by fluid friction and heat transfer contribute equally, the  $Be$  value is 0.5.

**Table 1** Mathematical expression of nanofluid properties.

| Properties              | Nanofluid   |
|-------------------------|---|
| Density                 | $\rho_{nf} = (1 - \varphi)\rho_f + \varphi\rho_s$   |
| viscosity               | $\mu_{nf} = \mu_f(1 + 13.5\varphi + 904.4\varphi^2)$  |
| Thermal expansion       | $(\rho\beta)_{nf} = (1 - \varphi)(\rho\beta)_f + \varphi(\rho\beta)_s$  |
| Heat capacitance        | $(\rho C_p)_{nf} = (1 - \varphi)(\rho C_p)_f + \varphi(\rho C_p)_s$   |
| Thermal conductivity    | $\frac{k_{nf}}{k_f} = \frac{(k_s + (m-1)k_f) + (m-1)\varphi(k_s - k_f)}{(k_s + (m-1)k_f) - \varphi(k_s - k_f)}$   |
| Electrical conductivity | with $m = 3/\psi$ , where $\psi = 0.62$<br>$\frac{\sigma_{nf}}{\sigma_f} = 1 + \frac{3\varphi \left( \frac{\sigma_s}{\sigma_f} - 1 \right)}{\left( \frac{\sigma_s}{\sigma_f} + 2 \right) - \varphi \left( \frac{\sigma_s}{\sigma_f} - 1 \right)}$ |

**Table 2** Thermo-physical properties of water and  $Fe_3O_4$  nanoparticle.

| Materials  | $\rho$<br>kgm <sup>-3</sup> | $\sigma$<br>Sm <sup>-1</sup> | $\beta$<br>K <sup>-1</sup> | $C_p$<br>J(kgK) <sup>-1</sup> | $k$<br>W(mK) <sup>-1</sup> |
|------------|-----------------------------|------------------------------|----------------------------|-------------------------------|----------------------------|
| Pure water | 997.1                       | 0.05                         | $21 \times 10^{-5}$        | 4179                          | 0.613                      |
| $Fe_3O_4$  | 5200                        | 25000                        | $1.3 \times 10^{-5}$       | 670                           | 6                          |

**Table 3** Comparison of values of  $\frac{\partial T}{\partial y}|_{y=0}$  for various values of  $Pr$  when  $\varphi = M = Q = n = 0$  and  $Ri = Re = 1$ .

| $Pr$ | [34]   | [35]  | [36]   | [37]   | Present |
|------|--------|-------|--------|--------|---------|
| 0.1  | 0.1637 | 0.164 | 0.1629 | 0.1630 | 0.1644  |
| 1    | 0.4009 | 0.401 | 0.4012 | 0.4015 | 0.4093  |
| 10   | 0.8266 | 0.827 | 0.8262 | 0.8274 | 0.8445  |

**4. Numerical analysis**

The numerical solutions have obtained using the finite difference method. Specifically, an implicit, unconditionally stable, Crank–Nicolson method has been utilized to find accurate and convergent solutions [31–33]. If  $u_{ij}^n, v_{ij}^n$  and  $T_{ij}^n$  represent the approximation of  $u(x, y, t), v(x, y, t)$ , and  $T(x, y, t)$  at time  $n$  for any point  $(x_i, y_j)$ , then the discrete form of Eqs. 6, 7 and 8, are given as

$$v_{ij}^{n+1} = v_{ij-1}^{n+1} - v_{ij}^n + v_{ij-1}^n - a_1 \left( u_{ij-1}^{n+1} - u_{i-1,j-1}^{n+1} + u_{ij}^{n+1} - u_{i-1,j}^{n+1} + u_{ij-1}^n - u_{i-1,j-1}^n + u_{ij}^n - u_{i-1,j}^n \right), \tag{17}$$

$$- a_2 u_{i-1,j}^{n+1} - b_1 u_{ij-1}^{n+1} + (1 + d_1) u_{ij}^{n+1} - c_1 u_{ij+1}^{n+1} = a_2 u_{i-1,j}^{n+1} + b_1 u_{ij-1}^{n+1} (1 - d_1) u_{ij}^n + c_1 u_{ij+1}^n + f, \tag{18}$$

$$- a_2 T_{i-1,j}^{n+1} - b_2 T_{ij-1}^{n+1} + (1 + d_2) T_{ij}^{n+1} - c_2 T_{ij+1}^{n+1} = a_2 T_{i-1,j}^n + b_2 T_{ij-1}^n + (1 - d_2) T_{ij}^n + c_2 T_{ij+1}^n, \tag{19}$$

given that

$$\begin{aligned} a_1 &= \frac{\Delta y}{2\Delta x}, \quad a_2 = \frac{\Delta t}{2\Delta x} u_{ij}^n, \quad f = \frac{\phi_4 Ri Re^{-1} \Delta t}{2\phi_1} \left( T_{ij}^{n+1} + T_{ij}^n \right), \\ b_1 &= \frac{\phi_2 \Delta t}{2\phi_1 \Delta y^2} + \frac{\Delta t}{4\Delta y} v_{ij}^n, \quad b_2 = \frac{\phi_6 \Delta t}{2\phi_5 Pr \Delta y^2} + \frac{\Delta t}{4\Delta y} v_{ij}^n, \\ c_1 &= \frac{\phi_2 \Delta t}{2\phi_1 \Delta y^2} - \frac{\Delta t}{4\Delta y} v_{ij}^n, \quad c_2 = \frac{\phi_6 \Delta t}{2\phi_5 Pr \Delta y^2} + \frac{\Delta t}{4\Delta y} v_{ij}^n, \\ d_1 &= \frac{\Delta t}{2\Delta x} u_{ij}^n + \frac{\phi_2 \Delta t}{\phi_1 \Delta y^2} + \frac{\phi_3 M \Delta t}{2\phi_1}, \quad d_2 = \frac{\Delta t}{2\Delta x} u_{ij}^n + \frac{\phi_6 \Delta t}{\phi_5 Pr \Delta y^2} + \frac{Q \Delta t}{2\phi_5}. \end{aligned} \tag{20}$$

At each  $i$ , the discrete Eqs.18 and 19 give us tri-diagonal systems, further solved by Thomas algorithm in MATLAB Software. The integration area has been taken as a rectangular with limits  $x_{max} = 1$  and  $y_{max} = 15$  such that it takes a location far away from the thermal and momentum boundary layers, here  $y_{max}$  refers to  $y = \infty$ . The mesh sizes are taken as  $\Delta x = \Delta y = 0.05$  and the time level is considered  $\Delta t = 0.01$ . Numerical iterations have been repeated several times to obtain convergent solutions. For a convergent solution, the tolerance rate has been taken as  $1e^{-5}$ . Moreover, Table 3 ensures validation of the present numerical solution with the existing study for steady case with zero velocity conditions at the wall.

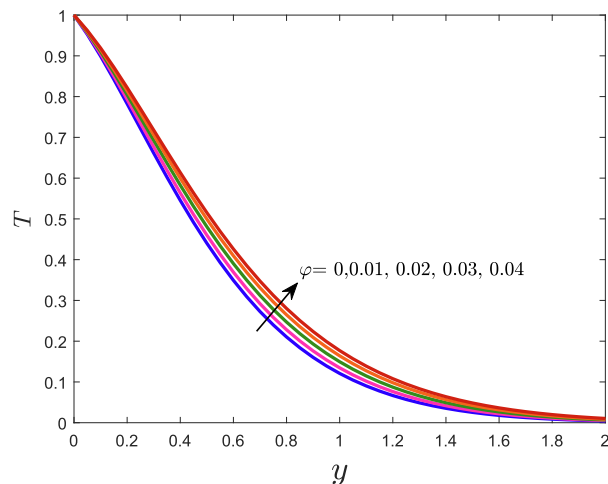
**5. Graphical results and discussion**

The effect of cylindrical-shaped  $Fe_3O_4$  nanoparticles on mixed convection heat transfer and entropy generation in an electrically conducting ferrofluid over a vertical surface in the

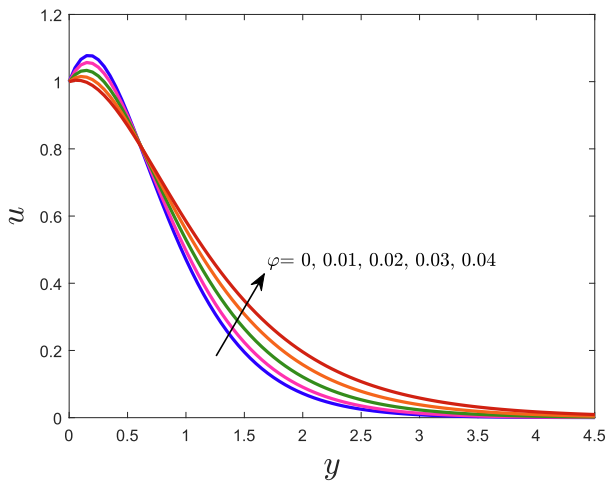
presence of heat generation is studied. The thermal conductivity of cylindrical-shaped nanoparticles is estimated using Hamilton and Crosser [38].

The effects of involved parameters on fluid flow and heat transfer features of ferrofluid are presented graphically. The numerical values assigned to the fixed parameters are:  $Pr = 6.2, \varphi = 0.01, M = 3, Ri = 1, Re = 0.1, Q = 1$ , and  $n = 0.5$ . The range of parameters are:  $0 \leq \varphi \leq 0.04, 0 \leq M \leq 7, 0 \leq Q \leq 1.5$  and  $0 \leq n \leq 1$ . The results are logical and closer to physical expectations.

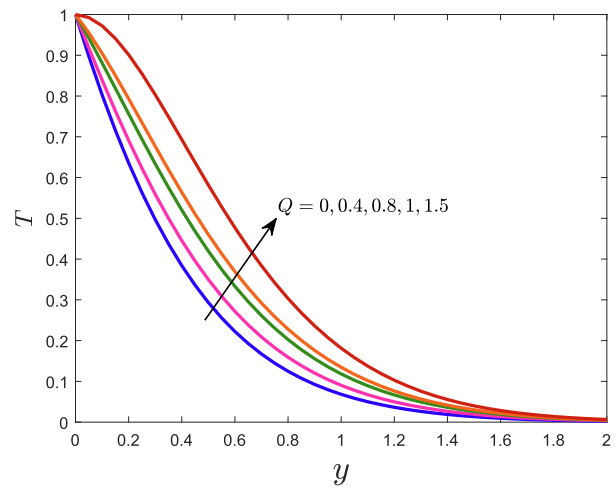
The variation in the temperature and velocity profiles of ferrofluid due to the volumetric concentration of cylindrical-shaped  $Fe_3O_4$  nanoparticles are depicted in Figs. 2 and 3, respectively. A significant increment in temperature is observed on suspending tiny nanoparticles in the base fluid, see Fig. 2. This relation is close to physical expectation since the suspension of nanoparticles increases the temperature due to increased thermal conductivity. On the other hand, the velocity of ferrofluid showed a dual nature under the variation of volumetric concentration of  $Fe_3O_4$  nanoparticles, displayed in Fig. 3. The flow profile decrease with an increment in nanoparticle volume fraction when  $y \lesssim 1$  and increases by adding more particles when  $y \gtrsim 1$ . The effects of the magnetic field on the temperature and velocity profiles of ferrofluid are plotted in Figs. 4 and 5, respectively. The result ensures a significant increment in the temperature for higher values of  $M$ . An opposite behavior is noticed on the velocity profile. This behavior was evident because the magnetic field generates resistive Lorentz force and an increment in the value of  $M$  also intensifies the resistive forces. Due to this fact, the velocity profile



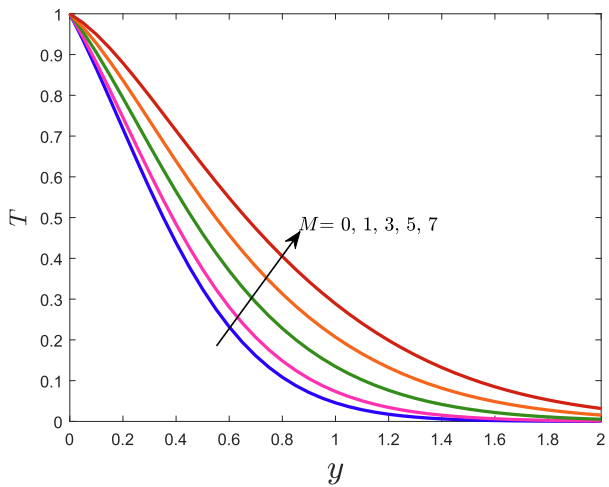
**Fig. 2** Influence of  $\varphi$  on temperature profile.



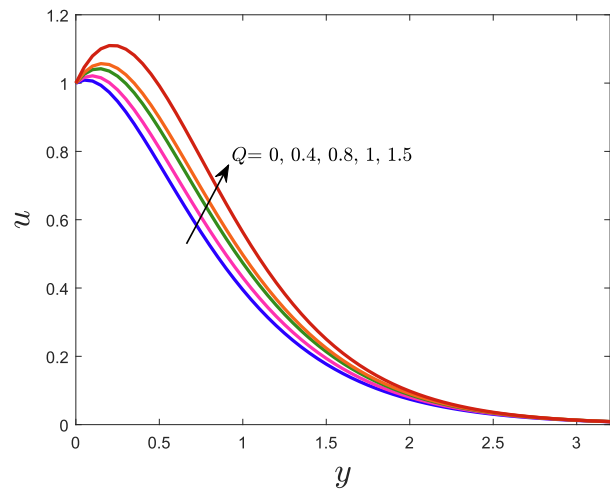
**Fig. 3** Influence of  $\phi$  on velocity profile.



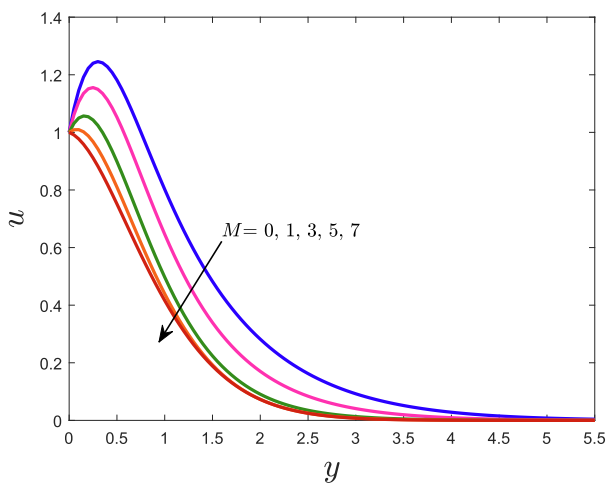
**Fig. 6** Influence of  $Q$  on temperature profile.



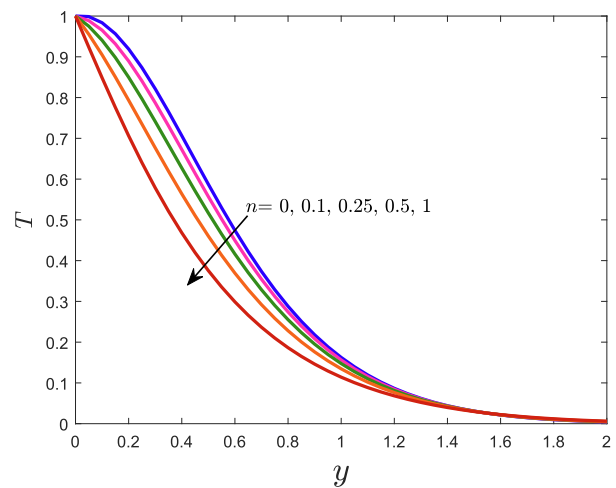
**Fig. 4** Influence of  $M$  on temperature profile.



**Fig. 7** Influence of  $Q$  on velocity profile.



**Fig. 5** Influence of  $M$  on velocity profile.



**Fig. 8** Influence of  $n$  on temperature profile.



dropped off against the magnetic field. Figs. 6 and 7 reveal the nature of temperature and velocity of ferrofluid under the effects of heat generation parameter, respectively. Fig. 6 shows that maximum temperature is attained by increasing the value of the heat generation parameter  $Q$ . Physically, when heat is generated, the temperature rise is evident. In Fig. 7, the trend of velocity curves confirmed an increment in the buoyancy force occurs due to heat generation; as a result, the velocity

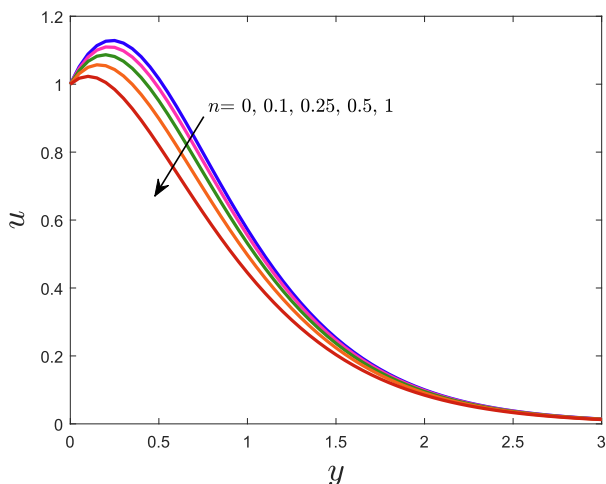


Fig. 9 Influence of  $n$  on velocity profile.

profile escalates significantly. The effects of the power index on the thermal and momentum boundary layer are plotted in Figs. 8 and 9, respectively. It is evident from the illustrated results that an increment in the power index parameter decreases the thermal and momentum boundary layer.

Figs. 10–17 are illustrated to analyze the variations in entropy generation and Bejan lines for different parameters. Fig. 10 exhibits the change in the entropy generation rate caused by the addition of nanoparticles to the base fluid. The entropy generation  $S_{GEN}$  is observed to grow with  $\phi$ . The changes in Bejan number  $Be$  for different volume fractions of nanoparticles are shown in Fig. 11. For all cases analyzed,  $Be$  reduces as  $\phi$  increases, indicating that adding nanoparticles to the base fluid increases the friction irreversibility rate. It is noted that a rise in Lorentz force tends to encourage the enhancement rate of entropy generation, as shown in Fig. 12. Furthermore,  $Be$  falls as the magnetic number rises, see Fig. 13. It reveals that lowering the magnetic number reduces the rate of irreversible heat transfer relative to friction. Fig. 14 shows that the entropy rate increases when the Brinkman number  $Br$  increases. Generally, thermal conductivity reduces when the Brinkman number grows, which increases entropy generation. On the other hand, the Bejan number decreases when  $Br$  increases, displayed in Fig. 15. The influence of temperature difference parameter  $\Omega$  on entropy generation and Bejan number are depicted in Figs. 16 and 17, respectively. The entropy generation rate reduced when  $\Omega$  increased. At the same time, the Bejan number increased with the rise in  $\Omega$ .

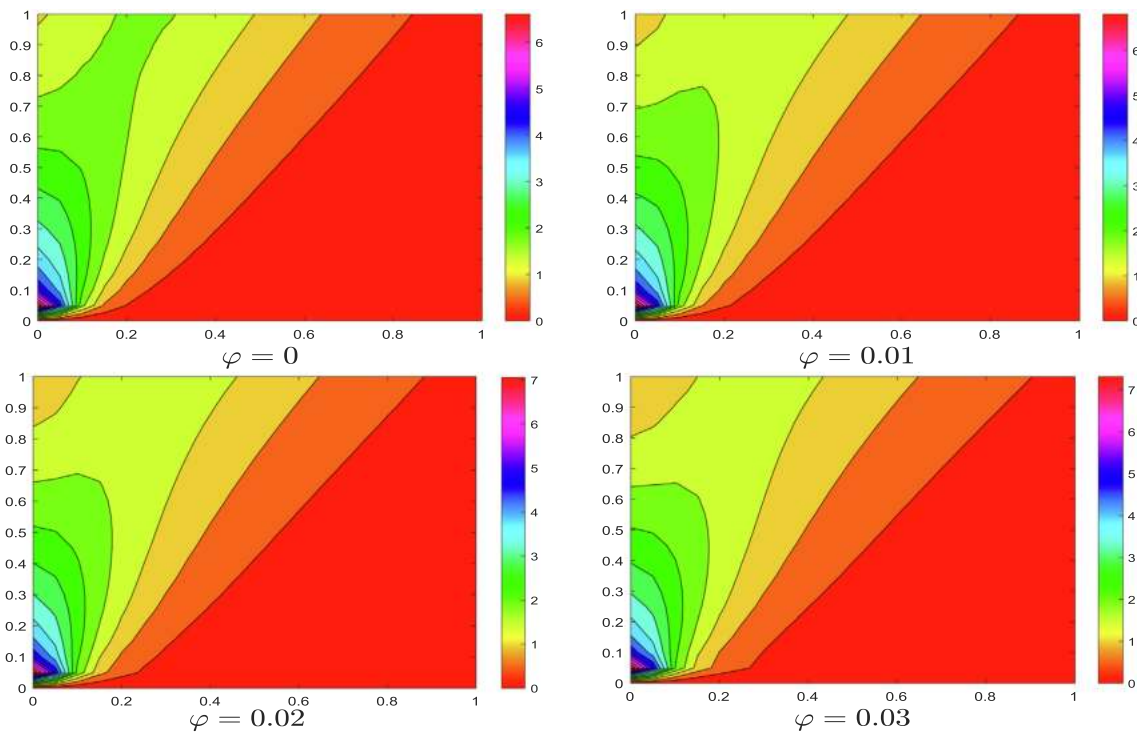


Fig. 10 Entropy generation for various values of  $\phi$ .

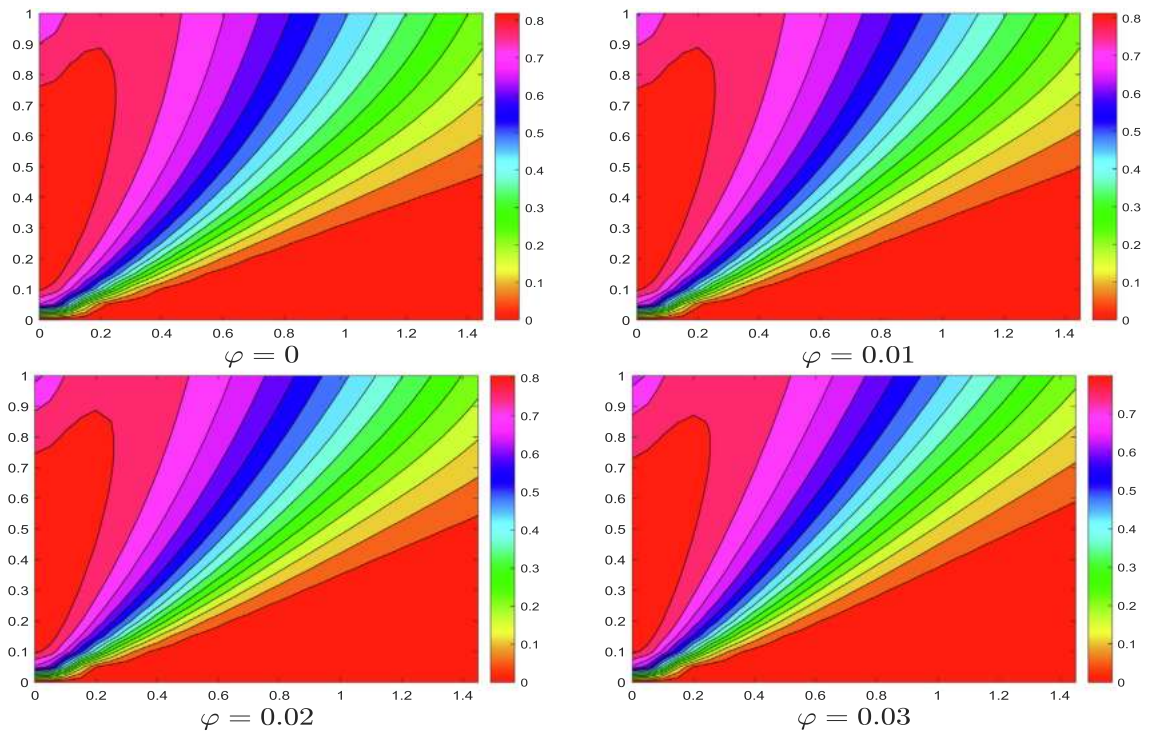


Fig. 11 Bejan lines for various values of  $\varphi$ .

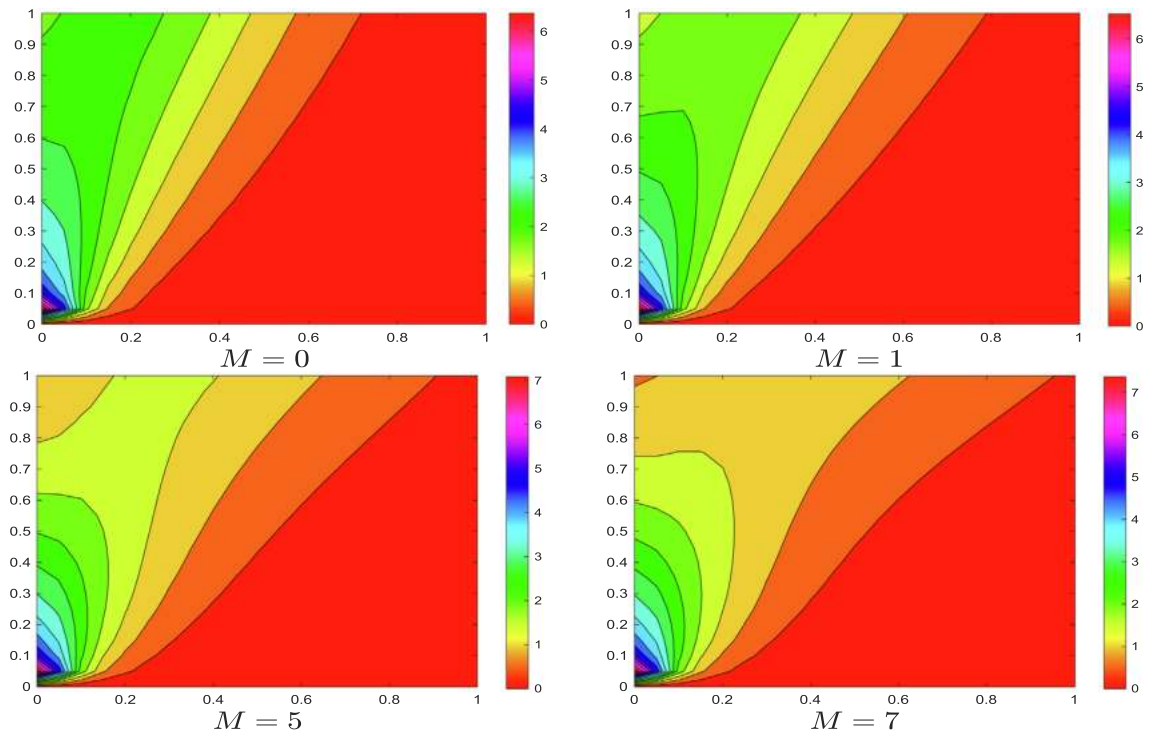


Fig. 12 Entropy generation for various values of  $M$ .

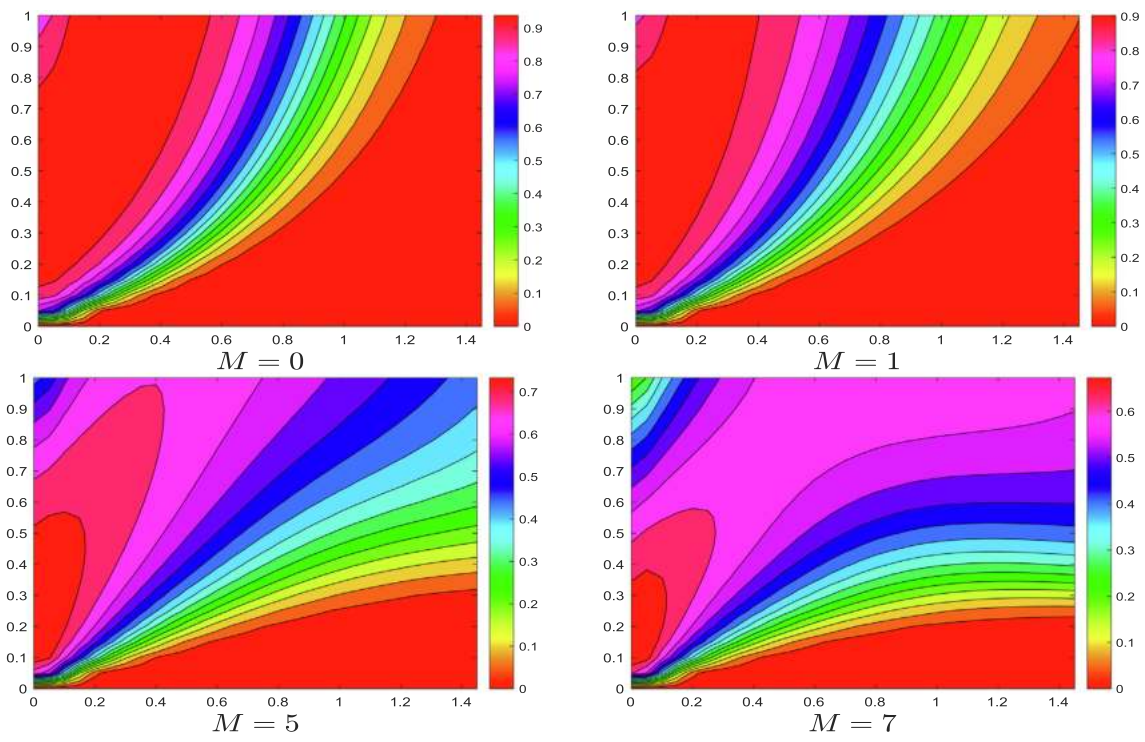


Fig. 13 Bejan lines for various values of  $M$ .

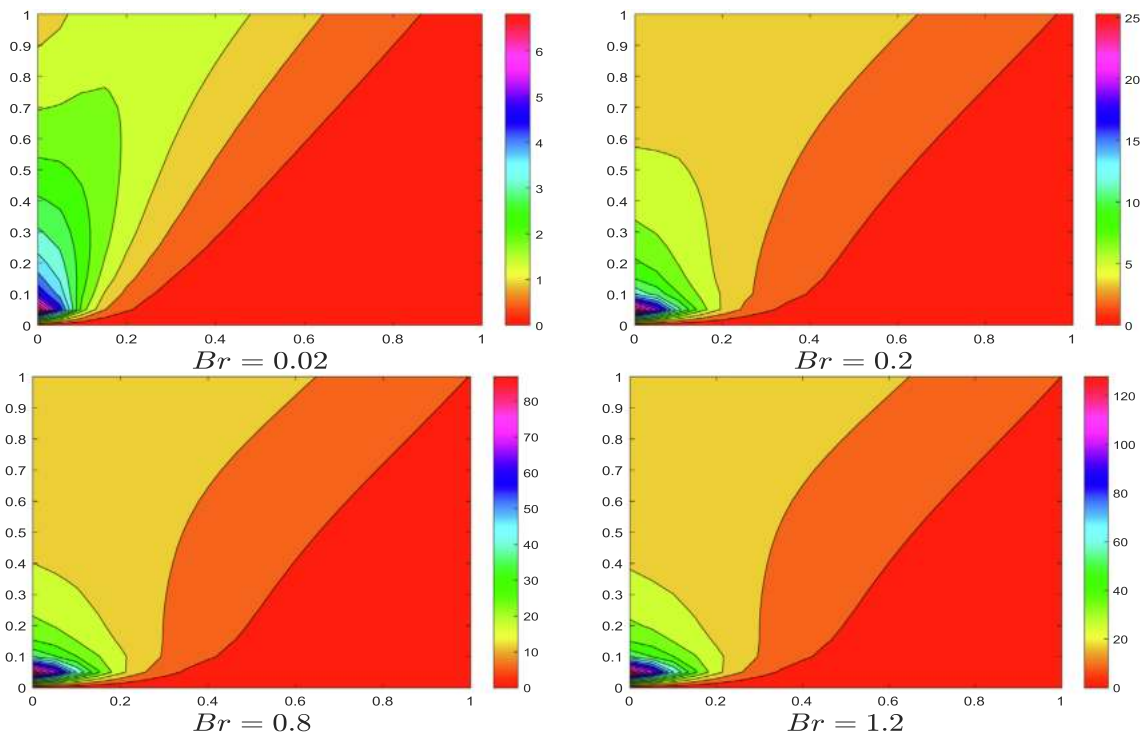


Fig. 14 Entropy generation for various values of  $Br$ .



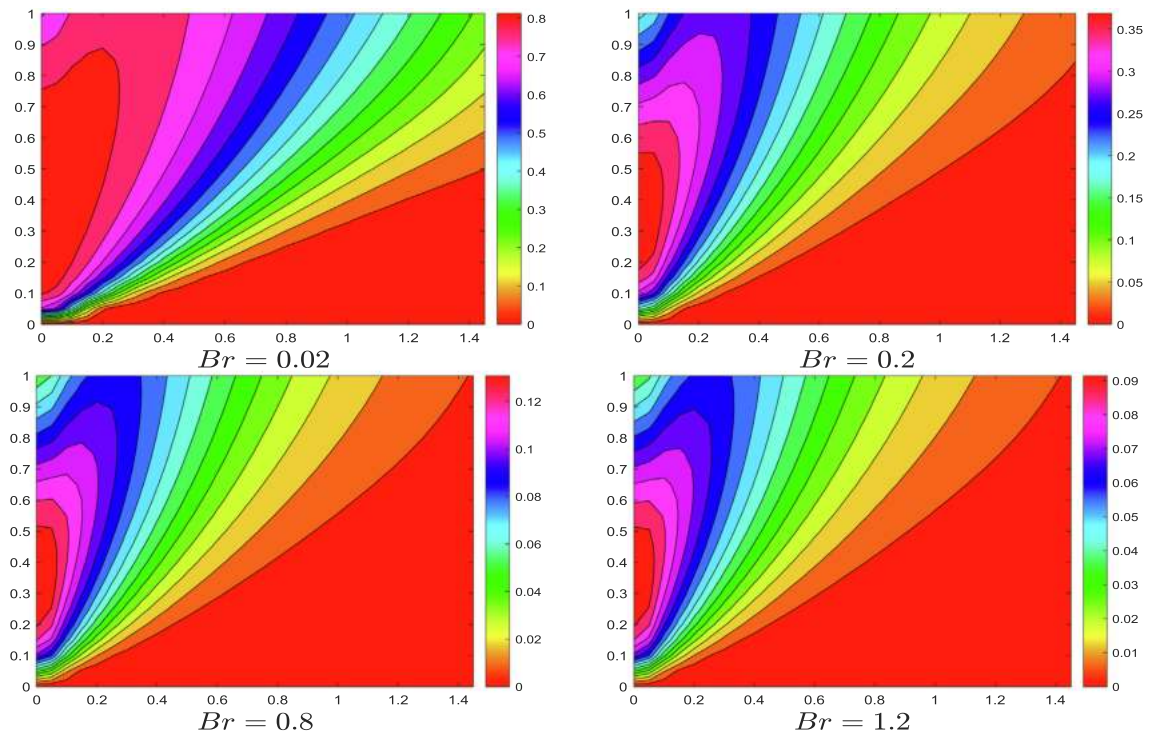


Fig. 15 Bejan lines for various values of  $Br$ .

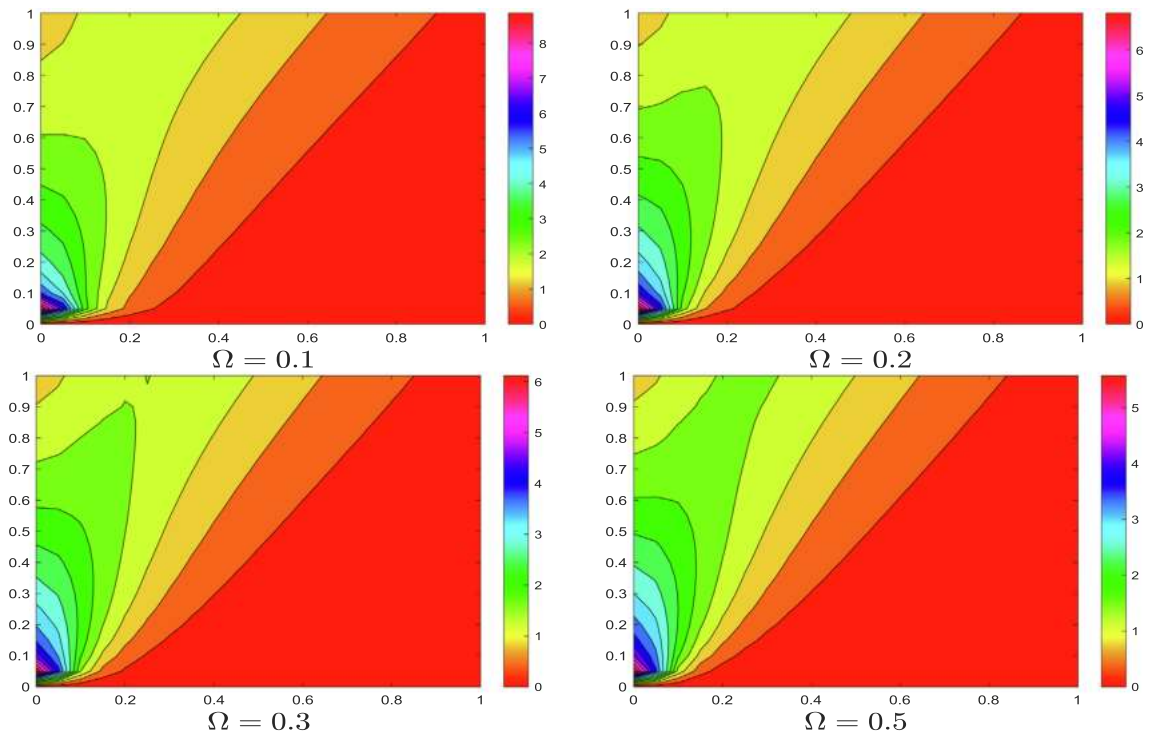


Fig. 16 Entropy generation for various values of  $\Omega$ .

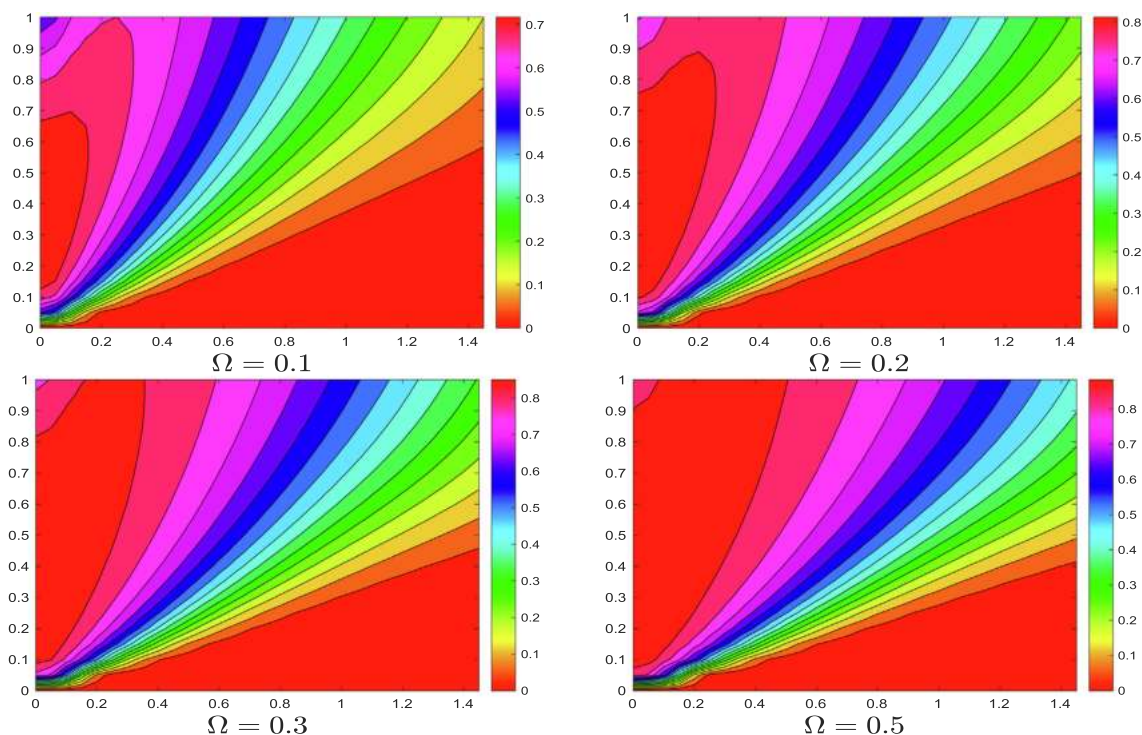


Fig. 17 Bejan lines for various values of  $\Omega$ .

## 6. Conclusions

Entropy generation in a two-dimensional ferrofluid flow over a flat surface with variable wall temperature is analyzed. Additionally, the impacts of the magnetic field together with heat generation/absorption are also investigated. An implicit finite difference is utilized to obtain the numerical solutions. The results showed that:

- The temperature profile is lifted up by adding nano-sized  $\text{Fe}_3\text{O}_4$  particles. Physically the suspension of nanoparticles improves the thermal conductivity of the regular base fluid (water), consequently, the temperature.
- The  $\text{Fe}_3\text{O}_4$  nanoparticles diminished the velocity profile when  $y \lesssim 1$ .
- The temperature distribution and the velocity profile attained maximum values when heat is generated.
- The entropy generation increases with the Brinkman number; however, the entropy generation decreases as the temperature difference grows.
- The friction irreversibility rate increased when the nanoparticle volume fraction and magnetic parameter increased.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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