MASS RATIO EFFECT ON THE VORTEX INDUCED VIBRATION OF CYLINDERS IN TANDEM ARRANGEMENT

MOHAMMAD MOBASSHER BIN TOFA

UNIVERSITI TEKNOLOGI MALAYSIA

MASS RATIO EFFECT ON THE VORTEX INDUCED VIBRATION OF CYLINDERS IN TANDEM ARRANGMENT

MOHAMMAD MOBASSHER BIN TOFA

A thesis submitted in fulfilment of the requirements for the award of the degree of Doctor of Philosophy (Mechanical Engineering)

> Faculty of Mechanical Engineering Universiti Teknologi Malaysia

> > DECEMBER 2016

Dedicated to my mother who is no more in this world

ACKNOWLEDGEMENT

I thank all mighty for everything.

I would like to state my earnest gratitude to my supervisor **Prof. Adi Maimun** for his encouragement, appropriate and precious guidance. Throughout my research, he has inspired me to be innovative and creative. I thank him for that. He supported me financially by allowing me to work as research assistant for a number of research projects beside my PhD project. Those projects also helped me to widen my engineering knowledge.

I would like to thank my co-supervisor **Dr Yasser Ahmed** for helping me in CFD modeling (specially meshing) required for this study.

I am thankful to **Technip Malaysia** for providing test set up that I used for some experiment.

I would like to thank my research colleagues such as Mr. Saeed Jamei, Mr. Atif, Mr.Ang, Mr.Takey, Mr Siewo etc for various help. I like to thank Mr. Ismail from MTC for helping me conducting VIV tests.

Last, but not the least, I would like to extend my deepest gratitude to my kind father, sister and brother for their encouragement during my study.

ABSTRACT

Vortex-Induced Vibration (VIV) is often regarded as the most complex fluidstructure interaction problem that is yet to be fully understood. This research investigated the impact of mass ratio on the mechanism of VIV of closely spaced cylinders. The mass ratio is a vital parameter which affects the VIV of a circular cylinder. There are few studies that discussed mass ratio effect on VIV of single cylinder and no significant research has been conducted to study the effect of mass ratio on VIV of closely spaced cylinders. In the study, numerical simulations were carried out to understand the nature of VIV of two cylinders with equal-diameter for different mass ratios in tandem configuration. VIV characteristics of two mass ratios were compared. Cylinder with mass ratio 2 represents lighter cylinder whereas mass ratio 8 represents a heavier cylinder. Only the upper or super upper response branch normally found between reduced velocities 5 to 8 was studied. The cylinders were exposed to uniform flows in subcritical flow regime and shear stress transport detached eddy turbulence model was employed for simulating the turbulent flow around these cylinders. The center to center spacing between cylinders was four times of cylinder diameter. A series of tests were conducted to validate the present numerical study. Vital VIV parameters with detailed discussions of flow patterns to scrutinize the influence of upstream cylinder's mass ratio on the VIV of the rear cylinder at resonance zone were presented. It was found that oscillation frequency of the upstream cylinder plays a significant role in the nature of VIV of downstream cylinder. For a relatively heavier upstream cylinder, VIV amplitude of downstream cylinder escalates at the lower limit of resonance zone. Noticeable VIV increment of rear cylinder can be found when natural frequency of the upstream cylinder is at least 14% lower than that of the downstream cylinder. The study of the mass ratio effect on VIV of closely spaced cylinders is significant in terms of designing aquatic clean energy converter widely known as VIVACE converter and assessing the collision risk and fatigue of cylindrical-shaped risers located close to each other.

ABSTRAK

Vortex-Induced Vibration (VIV) sering dianggap sebagai masalah interaksi struktur cecair yang paling kompleks yang masih belum dapat difahami sepenuhnya. Kajian ini mengkaji tentang kesan nisbah jisim kepada mekanisme VIV yang bertindak kepada silinder rapat. Nisbah jisim merupakan parameter penting yang memberi kesan kepada VIV silinder bulat. Terdapat beberapa kajian yang membincangkan kesan nisbah jisim pada VIV silinder tunggal dan tidak ada kajian penting telah dijalankan untuk mengkaji kesan nisbah jisim pada VIV silinder bulat. Dalam kajian itu, simulasi berangka telah dijalankan untuk memahami sifat VIV daripada dua silinder dengan sama-diameter dengan nisbah jisim yang berbeza dalam susunan seiring. Ciri-ciri VIV daripada dua nisbah jisim telah dibandingkan. Silinder dengan nisbah jisim 2 mewakili silinder yang lebih ringan manakala nisbah jisim 8 mewakili silinder yang lebih berat. Hanya upper atau super upper response branch yang biasanya ditemui antara pengurangan halaju 5-8 adalah dikaji. Silinder yang bertindak dengan aliran seragam dalam regim aliran subgenting dan model gelora shear stress transport detached eddy telah digunakan untuk simulasi aliran bergelora sekitar silinder ini. Jarak antara pusat dua silinder adalah empat kali daripada diameter silinder. Satu siri ujian telah dijalankan untuk mengesahkan kajian berangka ini. Parameter penting dalam penyelidikan VIV telah dibentangkan dan perbincangan terperinci dari segi corak aliran untuk meneliti pengaruh nisbah jisim silinder di hulu ke atas VIV silinder di hilir pada zon resonans. Penyelidikan ini mendapati bahawa kekerapan ayunan untuk silinder hulu memainkan peranan penting dalam kegiatan-VIV pada silinder hiliran. Bagi silinder hulu yang lebih berat, amplitud VIV silinder di hilir bertambah pada had bawah zon resonans. Untuk kenaikan VIV yang ketara di silinder belakang, frekuensi semulajadi silinder hulu adalah sekurang-kurangnya 14% lebih rendah daripada silinder di hilir. Kajian mengenai kesan nisbah jisim pada VIV silinder rapat adalah penting dari segi mereka bentuk akuatik bersih penukar tenaga yang dikenali sebagai VIVACE dan penilai risiko pelanggaran dan lesu penaik berbentuk silinder yang terletak berhampiran antara satu sama lain.

TABLE OF CONTENTS

CHAPTER			TITL	LE	PAGE
	DEC	LARATI	ION		ii
	DED	ICATIO	N		iii
	ACK	NOWLE	EDGEMENT		iv
	ABS'	TRACT			v
	ABS'	TRAK			vi
	ТАВ	LE OF C	CONTENTS		vii
	LIST	OF TAI	BLES		х
	LIST	OF FIG	URES		xi
	LIST	C OF ABI	BREVIATIONS		xviii
	LIST	OF SYN	MBOLS		xix
1	INTI	RODCTI	ON		1
	1.1	Backgr	ound		1
	1.2	Probler	n statement		3
	1.3	Objecti	ves of the study		3
	1.4	Scope of	of the study		4
	1.5	Signific	cance of the study		4
	1.6	Organiz	zation of the thesis		5
2	LITI	ERATUR	E REVIEW		7
	2.1	Introdu	ction		7
	2.2	VIV M	echanism		9
		2.2.1	Basic parameters		10
		2.2.2	VIV of Single Cyli	inder	16

	2.2.3	VIV suppression	18
	2.2.4	Flow induced vibration of a pair of cylinders	21
2.3	Usage	of CFD to study VIV	25
	2.3.1 T	rurbulace Model	27
	2.3.2 N	Aesh motion	28
2.4	Mass F	Ratio effect	29
2.5	VIV fo	r hydrokinetic energy harnessing	31
2.6	Motiva	tion of the research	33
2.7	Chapte	er summary	33

3	RES	EARCH	METHODOLOGY	35
	3.1	Introdu	ction	35
	3.2	Experir	nental Set Up	36
		3.2.1	One DOF system	37
		3.2.1	Two degree of freedom system	39
	3.3	Numeri	cal Simulation	43
		3.3.1	Introduction	43
		3.3.2	Numerical models	43
		3.3.3	Mesh ,bounary conditions and time step	46
	3.4	Research	ı Flow	50
4	VAI	IDATIO	N OF NUMERICAL STUDY	52
	4.1	General	1	52
	4.2	Single l	Rigid cylinder	52
	4.3	VIV of	Single cylinder (1DOF system)	54
	4.4	VIV of	a pair of cylinders (2 DOF system)	55
	4.5	Summa	ry	58
5	MAS	SS RATI	O EFFECT FOR SINGLE CYLINDER	60
	5.1	Introdu	ction	60
	5.2	Results	and Discussion	61
		50114	less ratio affact on VIV of single cylinder (1 DOF	
		5.2.1 M	lass ratio effect on viv of single cylinder (1 DOF	

		5.2.2 Mass ratio effect on VIV of single cylinder (2 DOF	7
		system)	69
	5.3	Effect of degree of freedom for low and high mass ratio	77
	5.4	Main findings and conclusion	79
6	VIV	OF CYLINDERS IN TANDEM ARRANGEMENT FO	R
	DIFF	TERENT MASS RATIOS	80
	6.1	Introduction	80
	6.2	Results and discussion	81
		6.2.1 Mass ratio effect on viv of two cylinders in tande	m (1
		DOF system)	81
		6.2.2 Mass ratio effect on viv of two cylinders in tande	m (2
		DOF system)	86
	6.3	Factors determine the VIV of downstream cylinder	92
	6.4	Main findings and Conclusion	100
7	VIV	OF CYLINDERS IN TANDEM ARRANGEMENT WI	ТН
	VAR	YING THE MASS RATIO	102
	7.1	Introduction	102
	7.2	Results and Discussion	104
	7.3	Effect of upstream cylinder's osicillation frequency	109
	7.4	Application for designing VIVACE convertor	124
	7.5	Main findings and Conclusion	126
8	CON	CLUSION AND FUTURE WORK	128
	8.1	Conclusion	128
	8.2	Recommendation	130
	8.2	Recommendation	130
REFEREN	8.2 NCES	Recommendation	130 132

ix

LIST OF TABLES

TITLE

TABLE NO.

3.1	Experimental parameters (Cylinder Particulars)	39
3.2	Experimental parameters (Cylinder Particulars) for 2DOF	41
4.1	Comparison of Experimental and numerical results	53
5.1	Key parameters of cylinder for VIV simulation	60
6.1	Key parameters of cylinder for VIV simulation of a pair	
	of cylinders	81
7.1	Key parameters of cylinder for VIV simulation of a pair of	
	cylinders for varying mass ratio	103
7.2	Flow velocity and corresponding reduced velocity for case	
	1	103
7.3	Flow velocity and corresponding reduced velocity for case	
	2	103
7.4	Parameters for VIVACE converter using synergy of a pair	
	of cylinders	124

PAGE

LIST OF FIGURES

FIGURE NO	. TITLE	PAGE
1.1	Vortex induced vibration of cylinder	01
2.1	Example of Velocity profiles for flow over a curved surface	09
2.2	Vortex patterns behind fixed cylinder	11
2.3	Strouhal number as a function of Re	12
2.4	Cylinder and coordinate system	14
2.5	Add-on devices for suppression of vortex-induced vibration	
	of cylinders	20
2.6	Two circular cylinders of equal diameter in cross-flow: (a)	
	tandem; (b) staggered; and (c) side-by-side	22
2.7	Sketch of interference region	23
2.8	Regimes of flow interference for tandem cylinders for	
	different separations	25
2.9	The peak amplitude and the range of ;U*(Ur) for	
	synchronization is controlled primarily by m^* (when $m^*\zeta$ is	
	constant)	30
2.10	Schematic of a single-cylinder VIVACE (left) and the 1st	
	generation of lab prototype	32
3.1	Research flow chart	36
3.2	1DOF system (left) 2DOF system (right)	36
3.3	Schematic diagram for 1DOF VIV	38
3.4	Experimental set up to measure VIV(1DOF)	38
3.5	Free decay test results	39

3.5 Free decay test results
3.6 Cylinders in tandem arrangement where "d" is the spacing between them
40

3.7	Experimental System for 2DOf VIV response Set up for	
	2DOf VIV response (a) Conventional parallel linkage system	
	(b) spring bar system	40
3.8	Details of set up for 2DOF VIV response of model riser(a),	
	Risers at towing tank(b)	41
3.9	Marker at cylinder top for qualisys video motion analysis	42
3.10	Boundary conditions used for simulations	47
3.11	Mesh dependency test	48
3.12	General view of Mesh for single cylinder	48
3.13	General view of Mesh for two cylinder in tandem	
	arrangement	49
3.14	Mass ratio effect on VIV of circular cylinder at Ur=6 for both	
	1DOF and 2 DOF	50
4.1	Fixed cylinder lift force $PSD(Re=10^4)$	53
4.2	Wide variety of results (rigid cylinder CL_{rms}) found by	
	different researchers, experimental uncertainty $> \pm 10\%$,	
	Norberg CL _{rms} values varies between 0.41-0.5 for Re>= 10^4 –	
	Re<10 ⁵ (Norberg, 2003)	54
4.3	Response curve (A/D vs Ur) plotted for cylinder with (m $\!\!\!\!\!\!\!\!\!\!\!\!\!$	
	\approx 1) for 1DOF to validate present numerical work to compare	
	numerical and experimental work	55
4.4	Response curve (A/D vs Ur) plotted for upstream cylinder	
	with (m ⁺ \approx 2) for 2DOF system to validate present numerical	
	work	56
4.5	Response curve (A/D vs Ur) plotted for downstream	
	cylinder with (m ⁺ \approx 2) for 2DOF system to validate present	
	numerical work	57
4.6	Ratio of cross line VIV amplitude between downstream	
	cylinder and upstream cylinder plotted as a function of Ur or	
	$(m^+ \approx 2)$ for 2DOF system	58
4.7	Ratio of in line VIV amplitude between downstream cylinder	
	and upstream cylinder plotted as a function of Ur for	
	$(m^+ \approx 2)$ for 2DOF system	58

5.1	Comparison between lighter and heavier cylinder's non-	
	dimensional VIV amplitudes (Ay/D) at different reduced	
	velocities (Ur)	62
5.2	Ratio between VIV amplitude of low mass ratio cylinder and	
	VIV amplitude of high mass ratio cylinder as a function of	
	Ur	63
5.3	Non-dimensional frequency f_{osc}/f_n plotted as a function of Ur	
	for cylinder with low and high mass ratio	63
5.4	Non-dimensional VIV amplitude against non-dimensional	
	time for cylinder with mass ratio ≈ 2 (stable zone)	64
5.5	Non-dimensional VIV amplitude against non-dimensional	
	time for cylinder with mass ratio ≈ 8 (stable zone)	64
5.6	Comparison between lighter and heavier cylinder's non-	
	dimensional Drag force (C _D) at different reduced velocities	
	(Ur) (1DOF)	65
5.6	Comparison between lighter and heavier cylinder's non-	
	dimensional Lift force (CL) at different reduced velocities	
	(Ur) (1DOF)	66
5.8	Velocity curl for cylinder with mass ratio 2 for a complete	
	cycle of motion at reduced velocity 5(1DOF)	67
5.9	Velocity curl for cylinder with mass ratio 8 for a complete	
	cycle of motion at reduced velocity 5(1DOF)	68
5.10	Comparison between lighter and heavier cylinder's non-	
	dimensional VIV amplitudes (A_y/D) at different reduced	
	velocities (Ur) (2DOF)	69
5.11	Comparison between lighter and heavier cylinder's non-	
	dimensional inline VIV amplitudes (A_x/D) at different	
	reduced velocities (Ur) (2DOF)	70
5.12	Non-dimensional frequency f_{osc}/f_n plotted as a function of Ur	
	for cylinder with low and high mass ratio (2DOF)	70
5.13	Comparison between lighter and heavier cylinder's non-	
	dimensional Lift force (CL) at different reduced velocities	
	(Ur) (2DOF)	71

5.14	Comparison between lighter and heavier cylinder's non-	
	dimensional Drag force (C _D) at different reduced velocities	
	(Ur) (2DOF)	72
5.15	VIV amplitude against time for cylinder with mass ratio \approx	
	2(stable zone) at Ur=6 (2DOF)	72
5.16	VIV amplitude against time for cylinder with mass ratio \approx	
	8(stable zone) at Ur=6 (2DOF)	73
5.17	Velocity curl for cylinder with mass ratio 2 for a complete	
	cycle of motion for 2DOF system	74
5.18	Velocity curl for cylinder with mass ratio 8 for a complete	
	cycle of motion for 2DOF system	75
5.19	Motion trajectory for cylinder with low mass ratio for 2DOF	76
5.20	Motion trajectory for cylinder with high mass ratio for 2DOF	76
5.21	Comparison of A_y/D for cylinder with mass ratio 2 for	
	1DOF and 2DOF system	77
5.22	Comparison of A_y/D for cylinder with mass ratio 8 for	
	1DOF and 2DOF system	78
5.23	Ratio between VIV amplitude of cylinder for 2DOF and VIV	
	amplitude of cylinder for 1DOF as a function of Ur	78
6.1	Cylinders in tandem arrangement where d is the spacing	
	between them	80
6.2	Response curve (A/D vs Ur) of two 1-DOF cylinders with	
	low mass ratio (m ⁺ \approx 2) in tandem compared with an isolated	
	cylinder	82
6.3	Comparison between non-dimensional frequency of two 1-	
	DOF cylinders with low mass ratio $(m^+ \approx 2)$ in tandem	83
6.4	Comparison between response curves (A/D vs Ur) of two 1-	
	DOF cylinders with high mass ratio $(m^+ \approx 8)$ in tandem	83
6.5	Comparison between non-dimensional frequency of two 1-	
	DOF cylinders with high mass ratio $(m^+ \approx 8)$ in tandem	84
6.6	Ratio of VIV amplitude of downstream cylinder and	
	upstream cylinder plotted as a function of Ur for cylinder	
	with different mass ratio	84

6.7	Ratio of lift coefficient of downstream cylinder and upstream	
	cylinder plotted as a function of Ur for two different mass	
	ratio	85
6.8	Ratio of drag coefficient of downstream cylinder and	
	upstream cylinder plotted as a function of Ur for two	
	different mass ratio	85
6.9	Comparison of nondimensional transverse amplitude of two	
	2-DOF cylinders with low mass ratio (m ⁺ \approx 2) in tandem	87
6.10	Comparison of nondimensional frequency of two 2-DOF	
	cylinders with low mass ratio $(m^+ \approx 2)$ in tandem	88
6.11	Comparison of nondimensional inline response amplitude	
	of two 2-DOF cylinders with low mass ratio $(m^+ \approx 2)$ in	
	tandem	88
6.12	Comparison of nondimensional transverse amplitude of two	
	2-DOF cylinders with low mass ratio ($m^+ \approx 8$) in tandem	89
6.13	Comparison of non-dimensional frequency of two 2-DOF	
	cylinders with low mass ratio $(m^+ \approx 8)$ in tandem	89
6.14	Comparison of nondimensional inline response amplitude	
	of two 2-DOF cylinders with low mass ratio $(m^+ \approx 8)$ in	
	tandem	90
6.15	Ratio of cross flow VIV amplitude of downstream cylinder	
	and upstream cylinder plotted as a function of Ur for	
	cylinder with different mass ratio(2DOF)	91
6.16	Ratio of in line VIV amplitude of downstream cylinder and	
	upstream cylinder plotted as a function of Ur for cylinder	
	with different mass ratio(2DOF)	91
6.17	Ratio of lift coefficient of downstream cylinder and upstream	
	cylinder plotted as a function of Ur for cylinder with	
	different mass ratio(2DOF)	91
6.18	Ratio of Drag coefficient of downstream cylinder and	
	upstream cylinder plotted as a function of Ur for cylinder	
	with different mass ratio (2DOF)	92

6.19	Velocity curl for cylinders in tandem arrangement with	
	mass ratio 2 at Ur =5 for a cycle of motion for 1DOF system	94
6.20	Flow streamlines for cylinders in tandem arrangement with	
	mass ratio 2 at Ur =5 for complete cycle of motion for 1DOF	
	system	95
6.21	Velocity curl for cylinders in tandem arrangement with	
	mass ratio 2 at Ur =6 for a cycle of motion for 2DOF system	96
6.22	Flow streamlines for cylinders in tandem arrangement with	
	mass ratio 2 at Ur =6 for complete cycle of motion for 2DOF	
	system	97
6.23	Velocity curl for cylinders in tandem arrangement with	
	mass ratio 2 at Ur =8 for a cycle of motion for 1DOF system	98
6.24	Flow streamlines for cylinders in tandem arrangement with	
	mass ratio 2 at Ur =8 for complete cycle of motion for 1DOF	
	system	99
7.1	Cylinders in tandem arrangement where d is the spacing	
	between them	102
7.2	Non dimensional VIV amplitude (A/D) plotted as a function	
	of downstream cylinder's reduced velocities (Ur) for two	
	different cases to identify the upstream cylinder's mass ratio	
	effect on the VIV of downstream cylinder	105
7.3	Non dimensional VIV amplitude (A/D) plotted as a function	
	of Reynolds number (Re) for two different cases to identify	
	the upstream cylinder's mass ratio effect on the VIV of	
	downstream cylinder	106
7.4	VIV amplitude against time for case 1(stable zone) at Re \approx 5	
	$x10^4$	106
7.5	Time series of lift force (downstream cylinder) for case	
	1(stable zone) at Re $\approx 5 \times 10^4$	107
7.6	VIV amplitude against time for case 2(stable zone) at Re \approx 5	
	$x10^{4}$	107
7.7	Time series of lift force (downstream cylinder) for case 2	
	(stable zone) at Re $\approx 5 \times 10^4$	108

7.8	Maximum downstream VIV increment plotted as a function	
	of ratio between upstream and downstream mass ratio	108
7.9	Maximum downstream VIV increment plotted as a function	
	of ratio between upstream and downstream natural frequency	109
7.10	Velocity curl for cylinders in tandem arrangement for case 1	
	at Re $=5 \times 10^4$ for complete cycle of motion for 1DOF system ,	
	time difference between each frame is .05 sec	112
7.11	Flow streamlines for cylinders in tandem arrangement for	
	case 1 at Re $=5 \times 10^4$ for complete cycle of motion for 1DOF	
	system, time difference between each frame is .05 sec	115
7.12	Velocity curl for cylinders in tandem arrangement for case 2	
	at Re $=5 \times 10^4$ for complete cycle of motion for 1DOF system,	
	time difference between each frame is .05 sec	118
7.13	Flow streamlines for cylinders in tandem arrangement for	
	case 2 at $\text{Re} = 5 \times 10^4$ for complete cycle of motion for 1DOF	
	system, time difference between each frame is .05 sec	121
7.14	Obtained VIVACE energy (J) against Reynolds number for	
	case1 and case 2	125
7.15	VIVACE energy increment (%) against Reynolds number	126
A.1.1	Conceptual sketches of new design concept to reduce VIV.	141
A.1.2	Conceptual sketches of new design with weathervane	
	capability concept to reduce VIV	142
A.1.3	Conceptual sketches of new design by using aerofoil and	
	ground effect(Top View)	142
A.1.4	Conceptual sketches of new design with weathervane	
	capability concept to reduce VIV	143
A.2.1	Relationship between drag and VIV amplitude at lock-in	
	(1DOF)	144
A.2.2	Relationship between drag and VIV amplitude at lock-in	
	(2DOF)	144

LIST OF ABBREVIATIONS

- 1 DOF One Degree Of Freedom
- 2 DOF Two Degree Of Freedom
- ALE Arbitrary Lagrangian Eulerian
- CFD Computational Fluid Dynamics
- CEL CFX Expression Language
- DAAS Data Acquisition System and Analysis System
- FIM Flow induced motion
- FFT Fast Fourier transform
- FSI Fluid Structure Interaction
- DES Detached Eddy Simulation
- DNV Det Norske Veritas
- LES Large Eddy Simulation
- PSD Power spectral density
- RANS Reynolds Averaged Navier-Stokes
- RMS Root mean square
- WIV Wake induced vibration
- VIV Vortex induced vibration
- VIVACE Vortex Induced Vibration for Aquatic Clean Energy
- UTM Universiti Teknologi Malaysia

LIST OF SYMBOLS

A_x	-	Inline amplitude in X direction
A _y or A	-	Cross line amplitude in Y direction
C _D	-	Drag Coefficient
C _L	-	Lift Coefficient
C_m	-	Added mass coefficient
D	-	Diameter of the cylinder
f or f_{osc}	-	Oscillation frequency
$\mathbf{f}_{\mathbf{n}}$	-	Natural frequency
$\mathbf{f}_{\mathbf{s}}$	-	Vortex shedding frequency
F_L	-	lift force acted on the cylinder
F_x	-	Inline force in X direction
F_y	-	cross line force in Y direction
L	-	Length of the cylinder
L/D	-	Inline amplitude in X direction
m	-	Cylinder mass
m _a	-	Added mass

m ⁺ or m [*]	-	Mass ratio
R _e	-	Reynolds number
U	-	Free stream mean velocity
Ur	-	Reduced velocity
Κ	-	Spring constant
E _{mech}	-	Converted energy by VIVACE
ω_z	-	Circular natural frequency of the cylinder
ρ	-	Water density
ω	-	Cylinder circular natural frequency
Φ	-	Phase difference
ζ	-	Damping factor
ν	-	Kinematic viscosity
μ	-	Dynamic viscosity
$\rho \overline{u_i u_j}$	-	Reynolds stresses.

LIST OF APPENDICES

APPENDIX	TITLE	PAGE
А	Conceptual designs to suppress VIV	141
В	Additional Graphs	144

CHAPTER 1

INTRODCTION

1.1 Background

Vortex-Induced Vibration widely known as VIV is a complicated hydrodynamic phenomenon. VIV is often regarded as the most complex fluidstructure interaction problem that happens when fluid flows over a certain structure. During the interaction of flow and the structure, at the boundary layer region due to viscous drag, energy dissipates and the flow lacks adequate kinetic energy. The lack of energy causes flow separation at boundary layer and vortices are formed at the wake region of the body as shown in figure.1.1. These vortices disperse periodically



Figure 1.1: Vortex induced vibration of cylinder (Blevins, 1990)

from each side of the body and produce the time dependent non-uniform pressures that are distributed around the object.

Lift forces that is dependent on time, are originated around the body by these non-uniform pressures. As a result, the structure oscillates in both inline and cross flow direction depending upon the degree of freedom. Vortices shed are unsteady flow by nature that depends on the mass and profile of the body, it also relies on the velocity of the free stream flow. Accurate calculation of the separation point is the key, surface roughness and Reynolds number play a significant role in terms of governing the nature of separation. When the shedding frequency is close to the natural frequency of the object, higher VIV amplitudes can be found. These higher VIV amplitudes can occur for a range of reduced velocities which is defined as lockin zone. Vikestad (1998) showed this synchronization mainly occurs due to the variation of hydrodynamic mass. Vortex-induced vibration can be defined as hydroelastic phenomenon if cylinders are subjected to water flows, where non-dimensional parameter mass ratio normally remains between 1 to 10. Mass ratio is nothing but the ratio between oscillating structure's mass and mass fluid that is displaced by the structure.

Most of the research works about VIV of a circular cylinder or other blunt objects discuss cases where the body was only freed to oscillate in cross flow direction. In other words, single degree of freedom cases dominate VIV related research works. However, there are very few recent researches that studied two degree of freedom cases and it was found that the nature of VIV for two degree of freedom cases where cylinder was designed to vibrate both cross flow and stream wise direction can be significantly different. Though there are numbers of research papers about VIV simulation of a circular cylinder, most of them were related to 2D flow and lower Reynolds number, numerical simulation of vortex induced vibration at high Reynolds number can be very challenging. Suitable mesh, appropriate turbulence model, strong computational resources are tricky issues to be dealt with before considering 3D simulation. The study of vortex dynamics and characteristics of fluid flow around a circular cylinder is important to understand the nature of flow around relatively large and complex structures. A circular cylinder is considered one of the fundamental shapes of structures that are used in many engineering designs and often a group of circular cylinders are used for designing complex structures. When two bodies are placed near to each other, thought-provoking fluid phenomena can be observed, so the VIV study of cylinders near to each other became an interesting and important subject of basic research in fluid mechanics. Vortex induced vibration can be observed in many engineering objects , such as offshore structures, production risers, bridges, aircraft control surfaces, thermo wells, engines, heat exchangers etc. The goal of this research work is to examine the nature of VIV of a pair of circular cylinders positioned in tandem; we specially focused on the effect of upstream (front) cylinder's mass ratio on the behavior of VIV of downstream (rear) cylinder.

1.2 Problem statement

There are comparatively very little available experimental or numerical research works that study VIV of a pair of cylinders. The initial hypothesis about VIV of closely spaced cylinders may be behind this lack of references for an oscillating pair of cylinders. Initially, it was assumed that when two closely spaced cylinder's experience VIV, the VIV of each cylinder resembles that of isolated cylinder. However, recent researches indicate that assumption was far from the reality. Recent literature also discussed the role of mass ratio on single cylinder's VIV and its significance, but the influence of mass ratio on the VIV of cylinders positioned near to each other has not been studied to the best of our knowledge. The study of cylinders in tandem arrangement is also important for designing VIVACE device. So far, no conclusive studies were done to study mass ratio effect for VIVACE device.

1.3 Objectives of the study

The goal of this research work is to examine the nature of VIV of a pair of circular cylinders positioned in tandem and develop new knowledge in terms of finding factors that govern rear cylinder's VIV. So, this research work has following objectives:

- To assess the mass ratio effect on the VIV of a circular cylinder at high Reynolds number.
- To determine the mass ratio effect on the VIV of two cylinders in the tandem arrangement.
- To identify the fluid dynamic effects of upstream cylinder's mass ratio on downstream cylinder in details by analyzing flow patterns.

1.4 Scope of the study

This research work contains subjects related to hydrodynamic nature of Vortex-induced vibration (VIV) of single cylinder and cylinders positioned near to each other. Procedures / guidelines / formulas to analyze VIV of single cylinder are established through literature study. The vortex induced vibration of closely spaced cylinders in tandem configuration was studied based on that analysis. Intensive numerical simulations were conducted for this study. Numerical simulations were validated by comparing obtained results with available experimental results. The influence of the mass ratio of the upstream cylinder over rear (downstream) cylinder's VIV was studied in details for 4D spacing. Only upper or super upper response branch (resonance zone) which is generally found between reduced velocity 5 to reduced velocity 7 was studied for all cases.

1.5 Significance of the study

As mentioned earlier, VIV is one of the most complicated fluid-structure interaction problems. There are many parameters that affect the nature of VIV of circular cylinders; mass ratio is one of those factors. Hydrodynamic engineers faced enormous challenge while designing riser systems that are used for extracting oil and gas from sea bed due to its destructive nature in terms of causing severe fatigue damage within small period of time. Vortex Induced Vibration can also be used to generate clean energy. Aquatic Clean Energy Converter or better known as VIVACE uses VIV to generate clean renewable energy from ocean currents (Soo, 2013). In most cases numbers of closely spaced circular cylinders are used to design VIVACE. Therefore, determination of mass ratio effect on vortex dynamics of closely spaced circular cylinders is important especially for designing riser system and VIVACE device.

1.6 Organization of the thesis

This thesis is divided into eight chapters. The current chapter gives the outline of the thesis. The objectives along with the scope of the research work are presented in chapter one. Significances of this study are also mentioned in this current part of the thesis.

Chapter two reports a thorough review of the already conducted research works that are related to the present study. For more vibrant presentation, the literature review was divided into several groups' i.e. basic definition of VIV, VIV mechanism of single and pair of cylinders, Usage of CFD to study VIV, the effect of mass ratio and motivation of the study.

In chapter three research methodologies have been described. Experimental and numerical research methods are presented. The experimental methodology describes the facilities, test set-up of experiment and procedure of test. It also describes the mathematical model used for numerical simulation.

Chapter four presents the validation of numerical simulation by comparing experimental results that are obtained through towing tank tests conducted by the author and from other researcher's work.

Chapter five explains the mass ratio effects on single cylinder for both 1DOF and 2DOF systems.

Natures of vortex induced vibration of cylinders in the tandem arrangement for different mass ratio are described in chapter six. Here both cylinders are allowed to vibrate for both 1DOF and 2DOF systems for different mass ratios. Both cylinders have same mass ratio.

In chapter seven, the vortex induced vibration of cylinders in tandem arrangement with varying mass ratio. Here both cylinders are allowed to vibrate for both 1DOF and 2DOF systems. Upstream cylinders mass ratio have been altered but downstream cylinders mass ratio remain same. This chapter basically describes the most important contribution of this research.

Finally, Chapter eight presents the major conclusions obtained from this research work. In addition, recommendations for future studies have been presented.

REFERENCES

- Allen,D.W., and Henning, D. L.(2001). US20016223672B1. Retrieved February, 2016,https://docs.google.com/viewer?url=patentimages.storage.googleapis.co m/pdfs/ US20016223672B1.pdf
- Allen, D.W., and Henning, D. L. (2003). Vortex-Induced Vibration Current Tank Tests of Two Equal-Diameter Cylinders in Tandem. J. Fluids Struct, 17, 767-781.
- Allen,D.W., and Henning, D. L. (2004). US20046685394B1. Retrieved February, 2016,https://docs.google.com/viewer?url=patentimages.storage.googleapis.co m/pdfs/ US20046685394B1.pdf
- Alonso, G., Valero, E., and Meseguer, J. (2009). An analysis on the dependence on cross section geometry of galloping instability of two dimensional bodies having either biconvex or rhomboidal cross sections. *European Journal of Mechanics B/Fluids*, 28, 328-334.
- Anagnostopoulos, P., and Bearman, P. W., (1992). Response characteristics of a vortex- excited cylinder at low Reynolds numbers. *Journal of Fluids and Structures*, 6, 39–50.
- Assi, G. R. S., Meneghini, J. R., Aranha, J. A. P., Bearman, P. W., and Casaprima, E. (2006). Experimental investigation of flow-induced vibration interference between two circular cylinders. *Journal of Fluids and Structures*, 22, 819-827
- Assi, G. R. S., Bearman, P. W., and Meneghini, J. R.(2010). On the wake-induced vibration of tandem circular cylinders: the vortex interaction excitation mechanism. *Journal of Fluid Mechanics*, 661, 365–401.
- Assi, G. R. S., Bearman, P. W., Carmo, B. S., Meneghini, J. R., Sherwin, S. J. and Willden, R. H. J. (2013). The role of wake stiffness on the wake-induced vibration of the downstream cylinder of a tandem pair, *Journal of Fluid Mechanics*, 718, p. 210-245.

- Assi, G. R. S. (2014). Wake-Induced Vibration of Tandem and Staggered Cylinders with Two Degrees of Freedom. *Journal of Fluids and Structures*, 50, 340-357.
- Bernitsas, M. M. and Raghavan, K. (2011). Enhancement of vortex induced forces & motion through surface roughness control. US Patent. *8,042,232*.U.S.
 Provisional Patent Application: United States Patent and Trademark Office.
- Blevins, R. D. (1990). *Flow-Induced Vibrations*, 2nd Edition. Van Nostrand Reinhold, ISBN 0-442-20651-B.
- Bokaian, A. and Geoola, F. (1985). Hydrodynamic Forces on a Pair of Cylinders. *Offshore Technology Conf*, 6-9 May, Houston, Texas, 1985, Paper no (OTC-5007-MS).
- Borazjani, I., and Sotiropoulos, F. (2009). Vortex induced vibrations of two cylinders in tandem arrangement in the proximity-wake interference region. *Journal of Fluid Mechanics*, 621, 321-364.
- Carmo, B. S., Sherwin, S. J., Bearman, P. W. and Willden, R. H. J. (2011) .Flowinduced vibration of a circular cylinder subjected to wake interference at low Reynolds number. *Journal of Fluids and Structures*, 27, 503-522.
- Carmo, B. S., Assi, G. R. S., Meneghini, J.R. and Julio, R. (2013). Computational simulation of the flow-induced vibration of a circular cylinder subjected to wake interference. *Journal of Fluids and Structures*, 41, 99-108.
- CFX theory, Ansys 2014. Retrieved April, 2015 http://148.204.81.206/Ansys/150/ANSYS%20CFX-Solver%20Theory%20Guide.pdf
- Chang,C..and Bernitsas,M. M. (2011). Hydrokinetic energy harnessing using the VIVACE converter with passive turbulence control. *Proceedings of the 30th OMAE 2011* Conf., Paper #50290, Rotterdam, The Netherlands, June 19-24, 2011.
- Chaplin, J. R., Bearman, P. W., Cheng, Y., Fontaine. E. and Graham, J. M. R. (2005). Blind Prediction of Laboratory Measurements of Vortex-Induced Vibrations of a Tension Riser. *Journal of Fluids and Structures*, 21, 25-40.
- Dong,S.and Karniadakis,G. E.(2005). DNS of Flow past a Stationary and Oscillating Cylinder at Re D 1000. *J Fluids and Struct.* 20: 519–531.

- D. N. V. (2009). Offshore standard DNV-RP-F203: riser interference. Det Norske Veritas, Norway
- Dulhunty,P.W. (2004). US20040035601A1. Retrieved February, 2016 https://docs.google.com/viewer?url=patentimages.storage.googleapis.com /pdfs/US20040035601.pdf
- Dye, R.C.F.(1978). Photographic evidence of the mechanisms of vortex-exited vibration. *Journal of Photography Science*. 26, 203–208.
- Fielding,S.M.(2005). Laminar boundary layer theory. Lecture notes Durham University. Retrieved February, 2016 http://community.dur.ac.uk/suzanne.fielding/teaching.html.
- Gardner, T.N. (1982). Deepwater Drilling in High Current Environment. 14th Annual; Offshore Conference. Houston, Tex., paper 4316
- Govardhan, R., and Williamson, C. H. K. (2000). Modes of Vortex Formation and Frequency Response of a Freely Vibrating Cylinder. *Journal of Fluids Mechanics*. 420, 85-130.
- Griffin, O. M. (1981). OTEC cold water pipe design for problems caused by vortexexcited oscillations. *Ocean Engineering*. 8, 129–209.
- Hagatun,K.,Steinkjer,O. and Lie, H. (2010).Hybrid riser solution for harsh environments. *Proceedings of Deep Offshore Technology International*, DOT-10, Amsterdam, Netherlands.
- Hanko, Z. G. (1967). Vortex Induced Vibration at Low-Head Weirs. Proceedings of the American Society of Civil Engineers. Journal of the Hydraulics Division, 93, 255-270.
- Holmes, S.,Oakley, O. H. and Constantinides, H. (2006). Simulation of Riser VIV
 Using Fully Three Dimensional CFD Simulations. OMAE 2006-92124. 25th
 International Conference on Offshore Mechanics and Artic Engineering.
 Hamburg, Germany.
- Huang, S. and Herfjord, K. (2013). Experimental Investigation of the Forces and Motion Responses of Two Interfering VIV Circular Cylinders at Various Tandem and Staggered Positions. *Applied Ocean Research*. 43, 264-273.
- Huera-Huarte, F.J. and Bearman, P. W. (2011). Vortex and Wake- Induced Vibrations of a Tandem Arrangement of Two Flexible Circular Cylinders with Near Wake Interference. *Journal of Fluids and Structures*. 27(2), 193-211.

- Huera-Huarte, F. J. and Gharib, M. (2011). Vortex-and Wake-Induced Vibrations of a Tandem Arrangement of Two Flexible Circular Cylinders with Far Wake Interference. *Journal of Fluids and Structures*. 27(5), 824-828.
- Hwang, J. Y., Yang, K. S. and Sun, S. H. (2003). Reduction of flow-induced forces on a circular cylinder using a detached splitter plate. *Phys Fluids*. 15(8):2433-2436.
- Igarashi, T. (1986). Characteristics of the flow around four circular cylinders Arranged in line. *Bulletin of JSME*. 29, 751–757.
- Karniadakis, G. E. (1999). Dynamics and flow structures in the turbulent wake of rigid and flexible cylinders subject to vortex-induced vibrations. *Journal of Fluid Mechanics*. 400, 91–124.
- Khalak, and Williamson, C. K. H. (1997). Investigation of relative effects of mass and damping in vortex-induced vibration of a circular cylinder. *Journal of Wind Engineering and Industrial Aerodynamics*. 69–71, 341–350.
- Khalak, and Williamson, C. H. K. (1999). Motions, forces and mode transitions in vortex-induced vibrations at low mass-damping. *J.Fluids Structures*. 13, 813-851.
- King, R., and Johns, D. (1976). Wake Interaction Experiments With Two Flexible Circular Cylinders in Flowing Water. J. Sound Vibration. 45, 259-283.
- King, R. (1977). A review of vortex shedding research and its application. *Ocean Engineering*, 4, 141–171.
- Kwon,S.H., Cho,J.W.,Park,J.S., Choi,H.S.(2002). The effects of drag reduction by ribbons attached to cylindrical pipes. *Ocean Eng.* 29: 1945-1958.
- Larsen, C. M. and Bech, A. (1986).Stress analysis of marine risers under lock-in conditions. *Proceedings from the 5th OMAE conference*, Tokyo, Japan.358-364.
- Larsen, C. M., Koushan, K., and Passano, E.(2002). Frequency and time domain analysis of vortex induced vibrations for free span pipelines.. Proceedings of the 21st International Conference on Offshore Mechanics and Artic Engineering. Oslo, Norway, June 23-28, OMAE2002-28064.
- Lee, J. H. and Bernitsas, M. M. (2011). High-damping, high-Reynolds VIV tests for energy harnessing using the VIVACE converter. *Ocean Engineering*. 38, 1697-1712.

- Leontini, J. S., Thompson, M. C., and Hourigan, K. (2006). The beginning of branching behaviour of vortex-induced vibration during two-dimensional flow. *Journal of Fluids and Structures*. 22, 857–864.
- Lie, H. (2007). US20070215028A1. Retrieved February, 2016, from https://docs.google.com/viewer?url=patentimages.storage.googleapis.com /pdfs/US20070215028.pdf
- Lienhard, JH. (1966). Synopsis Of Lift Drag And Vortex Frequency Data For Rigid Cylinder. Bulletin 300, Washington State University, Retrieved on 22nd May, 2016, http://www.uh.edu/engines/vortexcylinders.pdf
- Ljungkrona, L., Norberg, C., Sunden, B., (1991). Free-stream turbulence and tube spacing effects on surface pressure fluctuations for two tubes in an in-line arrangement. *Journal of Fluids and Structures*. 5 (6), 701 727
- Lucor, D., Mukundan, H. and Triantafyllou, M. S. (2006). Riser Modal Identification in CFD and Full-scale Experiments. *Journal of Fluids and Structures*. 22, 905-917.
- Marcoux, S. and Blevins, R.D. (2012). Wake Induced Riser Interference under VIV at 10⁵ Reynolds. *Proc 22nd Int Offshore and Polar Eng Conf.* Rhodes, June 17-22, Greece, Vol 3.
- Menter, F. R. (1993). Two-equation eddy-viscosity turbulence models for engineering applications. *AIAA-Journal*. 32(8), 269-289.
- Menter, F. R., Kuntz, M. and Bender, R. (2003). A scale-adaptive simulation model for turbulent flow predictions. *AIAA Paper*. 2003-0767.
- Miliou,A., Spencer J., Sherwin and Michael, J. R.(2002). Three-dimensional wakes of curved pipes. Proceedings of the 21st International Conference on Offshore Mechanics and Artic Engineering. Oslo, Norway, June 23-28, paper no. OMAE2002-28308.
- Moe,G. and Wu, Z. J. (1990). The lift force on a cylinder vibrating in a current. *ASME Journal of Offshore Mechanics and Arctic Engineering*. 112, 297– 303.
- Moe,G. and Holden, K. (1994). Motion of spring supported cylinders in subcritical and critical water flows. *Proceedings of the Fourth International Offshore and Polar Engineering Conference 3*. Osaka, Japan, 468–475.

- Morison, J.R., O'Brien, M.P., Johnson, J.W., Schaaf, S.A. (1950). The force exerted by surface waves on piles. *Petroleum Transactions*. AIME 189, 149–154
- Ng,D.J.T., Teng, Y.Z., Ross,A.M., Armanadaka, Ahmed, Z., Kader, A. S.A., Malik, A.M.A., Ismail,N.H., Gani, M. P. A. (2014). Tandem Riser VIV Suppression Fairing Model Test. *Proceedings of the 33rd International Conference on Offshore Mechanics and Artic Engineering*. San Francisco, USA, June 8-13, OMAE2014-23412.
- Ng,D.J.T., Teng, Y.Z., Ross, A.M., Armanadaka, Ahmed, Z., Kader, A. S.A., Malik, A.M. A., Ismail,N.H., Gani, M. P. A. (2014). Riser VIV Suppression Device Test. Offshore Technology Conference. OTC-24874-MS, OTC Asia 2014.
- Norberg, C. (2003). Fluctuating Lift on a Circular Cylinder: Review and New Measurements. *J Fluids and Struct*. 17, 57–96.
- Nguyen, N. (2000). US20006102664. Retrieved February, 2016, https://docs.google.com/viewer?url=patentimages.storage.googleapis.com /pdfs/ US20006102664.pdf
- Oakley,O.H. and Spencer,D. (2004).Deepstar High Reynolds Number Cylinder Test Program. *Proceedings Deep Offshore Technology Conference*, DOT'04, New Orleans.
- Park, H. R., Bernitsas, M. M. and Kumar, A. R.(2011). Selective Roughness in the Boundary Layer to Suppress Flow Induced Motions of Circular Cylinder at 30,000<Re<120,000. *Proceedings of the 30th OMAE 2011 Conf.* Paper no. 50302, Rotterdam, The Netherlands, June 19-24.
- Pasto,S.(2008). Vortex-induced vibration of a circular cylinder in laminar and turbulent flows. *Journal of Fluids and Structures*, 24, 977–993.
- Prasanth,T. K. and Mittal, S. (2009). Flow induced oscillation of two circular cylinders in tandem arrangement at low Re. *Journal of Fluids and Structures*. 25, 1029-1049.
- Raghavan, K. and Bernitsas, M. M. (2008).Enhancement of high damping VIV through roughness distribution for energy harnessing at 8×10³<Re<1.5×10⁵. 27th International Conference on Offshore Mechanics and Arctic Engineering. June 9-13,871-882.
- Roshko,A.(1961). Experiments on the Flow Around a Circular Cylinder at Very High Reynolds Number. *J Fluid Mech.* 10, 345–356.

- Saltara, F., Agostini Neto, A. D. and Lopez, J. I. Z.(2011). 3D CFD Simulation of Vortex-induced Vibration of Cylinder. *International Journal of Offshore and Polar Engineering*. 21, 192–197.
- Sarpkaya, T. (1978). Fluid forces on oscillating cylinders. *Journal of Waterway Port Coastal and Ocean Division ASCE*, 104, 275–290.
- Sarpkaya,T.(1995).Hydrodynamic Damping Flow-Induced Oscillations and Biharmonic Response. ASME Journal of Offshore Mechanics and Arctic Engineering. 117, 232–238.
- Sarpkaya, T. (2004). A critical review of the intrinsic nature of vortex-induced vibrations. *J Fluid Mech.* 19, 389–447
- Scruton and Walshe (1963).*US3076533* Retrieved February, 2016 https://docs.google.com/viewer?url=patentimages.storage.googleapis.com/pdf s/US3076533.pdf
- Shur,M., Philipe,R., Spalart, Kyle.,D,Strelets.M.,Travin.A.(2005). Three Dimensionality in Reynolds-Averaged Navier-Stokes Solutions Around Two-Dimensional Geometries. *AIAA Journal*. 43, 1230–1242.
- Soni, P. K. (2008). Hydrodynamic Coefficients for Vortex-Induced Vibrations of Flexible Beams. PhD thesis, Department of marine technology, NTNU, Trondheim, Norway.
- Soo,K.E.(2013). PhD thesis, Synergy of multiple cylinders in flow induced motion for hydrokinetic energy harnessing. Retrieved February, 2015, https://deepblue.lib.umich.edu/handle/2027.42/100015.
- Stappenbelt, B. (2007). Low mass ratio vortex-induced motion. Proceedings of the 16th Australasian Fluid Mechanics Conference. December 2-7, Brisbane, Australia, 1491-1497.
- Stansby, P.K., Pinchbeck, J.N., Henderson, T.(1986). Spoilers for the suppression of vortex induced oscillations (Technical Note). *Applied Ocean Research*. 8(3), 169-173.
- Sumner, D. (2010). Two circular cylinders in cross-flow: A review. *Journal of Fluids and Structures*. 26, 849-899.
- Szwalek, J. and Larsen, C. M. (2009). Reynolds Number Effects on Hydrodynamic Coefficients of Pure In-Line and Pure Cross-Flow Vortex Induced Vibrations.

Proceedings of 28th Conference Offshore Mechanics and Arctic Engineering. May 31 – June 5, Honolulu USA, 439-452.

- Toebes,G. H.and Eagleson,P.S.(1961). Hydroelastic Vibrations of Flat Plates Related to Trailing Edge Geometry. ASME Journal of Basic Engineering. 83, 671-678.
- Triantafyllou, M. S., Triantafyllou, G. S., Tein, D. and Ambrose., B. D. (1999). Pragmatic Riser VIV Analysis. Offshore Technology Conference. Paper OTC 10931, Houston, USA.
- Trim,A. D., Braaten, H., Lie, H. and Tognarelli, M. A. (2005). Experimental Investigation of Vortex-induced Vibration of Long Marine Risers. *Journal of Fluids and Structures*. 21, 335-361.
- Willden and Graham. (2004). Multi-modal Vortex-Induced Vibrations of a Vertical Riser Pipe Subject to a Uniform Current Profile. *European Journal of Mechanics B/Fluids*. 23, 209-218.
- Williamson, C. & Jauvtis, N., (2004). A High-Amplitude 2T Mode of Vortex-Induced Vibration for a Light Body in XY Motion. European Journal of Mechanics B/Fluids 23, 107-114.
- Wong and Kokkalis. (1982). A comparative study of three aerodynamic devices for suppressing vortex-induced oscillation. J Wind Eng Indust Aerodyn. 10, 21-29.
- Vandiver, J.K. and Li, L. (2003). SHEAR7 V4.2f program theoretical manual. Department of Ocean Engineering MIT, Massachusetts, USA.
- Vikestad, K. (1998). Multi-Frequency Response of a Cylinder Subjected Vortex-Shedding and Supported Motions. D.Sc. Thesis, Department of Marine Structures, Norwegian University of Science and Technology, Trondheim, Norway.
- Yen, K. M., Ross, A.M., Armanadaka, Ahmed, Z., Ismail,N.H., Malik, A.M. A., Gani, M. P.A., Teng, Y.Z. (2013). Riser VIV suppression device test for application to a south Asia TLP. *Proceedings of the 32nd International Conference on Offshore Mechanics and Artic Engineering*. Nantes, France, June 8-13, OMAE2013-11087.

- Zdravkovich (1988). Review of Interference-Induced Oscillations in Flow Past Two Parallel Circular Cylinders in Various Arrangements. *Journal of Wind Engineering and Industrial Aerodynamics*. 28(1), 183-199.
- Zhang, H. J, Zhou Y., So, R. M. C., Mignolet, M. P., Wang, Z. J. (2003). A note on the fluid damping of an elastic cylinder in a cross flow. *J Fluids Structure*. 17: 479-483.
- Zhao, M. (2013). Flow Induced Vibration of Two Rigidly Coupled Circular Cylinders in Tandem and Side-by-Side Arrangements at a Low Reynolds Number of 150. *Physics of Fluids*. 25(12),123601.