# DEGRADATION LIMIT STATE MODEL FOR STRUCTURAL RELIABILITY SCREENING OF AGEING FIXED OFFSHORE PLATFORMS

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# DEDICATION

To the loved ones. Thank you.

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#### ABSTRACT

Ageing fixed offshore platforms are growing in numbers worldwide. Operators choose to extend the platforms lives beyond the original design to improve economic viability and increase profitability. The structural integrity of these platforms is affected by various degradation factors throughout their service lives. However, a limited number of comprehensive studies have been conducted on the relationship between reserve strength ratio, probability of failure and return period with multiple degradation factors. This study aims to develop a comprehensive regression model of reserve strength ratio, probability of failure and return period by considering marine growth, corrosion and subsidence. Calculating reserve strength ratio, probability of failure, and return period are fairly time consuming. The presence of the proposed model is to provide a quick reference and immediate results of the remaining life of the fixed offshore platform in the occurrence of degradations, thus minimising the usage of industry resources. It is also expected that degradation effects over time will be predicted accurately. The development of the degradation limit state model adopted structural reliability assessment, which has been widely used in the oil and gas industry to determine the probability of failure and return period of offshore structures. The assessment can provide a higher confidence level that is required by regulators and stakeholders. This study includes the effects of wave height at the collapse of the platform caused by wave-in-deck. The wave-in-deck load has been calculated based on the silhouette method introduced by International Organization for Standardization. The degradation limit state models considered have 0 m, 2 m, 4 m, 6 m and 8 m subsidence. Each of them with 0 mm, 3 mm, 6 mm, 9 mm and 12 mm corrosion depth has been studied separately. The model has been developed using both single and linear multi regression method. The proposed models are then validated with a platform of similar configurations. Based on the validation results of single regression method, the lowest accuracy for reserve strength ratio was 94.9 %, while the probability of failure and return period were 56.6 % and 69.7 %, respectively. Despite that, the variations are acceptable since both probability of failure and return period values conform with the standard industry requirements. However, the results for 5 m subsidence shows very low accuracies, hence not recommended to utilise subsidence value that has not been considered in model development. For linear multi regression method, the lowest accuracy for reserve strength ratio has been 92.1 %. However, both probability of failure and return period shows very low accuracies, therefore, not recommended to be utilized by industry. It has been found that although the analysis model used for validation had a similar configuration, the overall platform surfaces were different, which in turn gave different platform responses. This eventually led to differences in the probability of failures and return periods. Careful consideration is expected prior to adopting the proposed model as it is to be used with platforms, which have similar platform configurations, structural member sizing, water depth and metocean data. The accuracy and effectiveness of the proposed model will generally assist operators in the industry in decision-making and more importantly, in outlining the action items for business risk management in which marine growth, corrosion, and subsidence are expected to occur.

#### ABSTRAK

Bilangan pelantar minyak tetap luar pesisir lebih usia semakin bertambah di seluruh dunia. Pengendali memilih untuk memanjangkan jangka hayat pelantar melebihi usia reka bentuk asal bagi meningkatkan daya maju ekonomi dan keuntungan. Integriti struktur pelantar ini dipengaruhi oleh pelbagai masalah degradasi sepanjang hayat operasi. Walau bagaimanapun, sebilangan kajian komprehensif yang terbatas telah dijalankan mengenai hubung kait antara nisbah kekuatan simpanan, kebarangkalian gagal and tempoh ulangan dengan pelbagai degradasi. Kajian ini bertujuan untuk membangunkan model regresi yang menyeluruh bagi nisbah kekuatan simpanan, kebarangkalian gagal and tempoh ulangan dengan mengambil kira hidupan marin, karatan dan enapan. Mengira nisbah kekuatan simpanan, kebarangkalian gagal dan tempoh ulangan memakan masa yang agak panjang. Kehadiran model yang diusulkan ini dapat menjadi rujukan dan memberikan keputusan yang segera terhadap baki jangka hayat pelantar minyak tetap luar pesisir sekiranya degradasi terjadi, seterusnya mengurangkan penggunaan tenaga kerja industri. Turut dijangkakan bahawa kesan degradasi dari masa ke masa akan dapat diramalkan dengan tepat. Pembangunan model degradasi had keadaan menggunakan penilaian kebolehpercayaan struktur, yang telah banyak digunakan dalam industri minyak dan gas untuk menentukan kebarangkalian gagal dan tempoh ulangan pelantar minyak tetap luar pesisir. Penilaian ini dapat memberikan aras keyakinan yang diperlukan oleh pihak berkuasa dan berkepentingan. Kajian ini juga merangkumi kesan ketinggian ombak ketika platform runtuh disebabkan oleh bebanan hempasan ombak ke dek. Bebanan hempasan ombak ke dek dikira berdasarkan kaedah siluet yang dicadangkan oleh International Organization for Standardization. Model degradasi had keadaan ini mengambil kira enapan sebanyak 0 m, 2 m, 4 m, 6 m dan 8m. Setiap model tersebut mempunyai 0 mm, 3 mm, 6 mm, 9 mm dan 12 mm tebal karatan. Model in dibangunkan mengunakan kaedah regresi tunggal dan kaedah lelurus berbilang. Model yang dicadangkan juga telah dibandingkan dengan satu pelantar minyak luar persisir yang mempunyai persamaan konfigurasi. Berdasarkan pengesahan menggunakan kaedah regresi tunggal, nilai ketepatan terendah bagi nisbah kekuatan simpanan adalah 94.9 %, manakala kebarangkalian gagal dan tempoh ulangan, nilainya masing-masing adalah 56.6 % dan 69.7 %. Walau bagaimanapun, perbezaan ini boleh diterima kerana nilai kebarangkalian gagal dan tempoh ulangan memenuhi keperluan piawaian industri. Walau bagaimanapun, keputusan enapan 5 m menunjukkan ketepatan yang sangat rendah, oleh itu tidak digalakkan untuk menggunakan nilai yang tidak diambil kira dalam pembangunan model. Bagi kaedah regresi lelurus berbilang, ketepatan terendah untuk nisbah kekuatan simpanan adalah 92.1 %. Namun begitu, nilai kebarangkalian gagal dan tempoh ulangan menunjukkan ketepatan yang sangat rendah, maka tidak disarankan untuk digunakan oleh industri. Dengan ini didapati bahawa walaupun analisis model yang digunakan untuk validasi mempunyai konfigurasi yang sama, tetapi keseluruhan permukaan pelantar adalah berbeza menyebabkan perbezaan dari segi tindakbalas pelantar. Ini akan menyebabkan perbezaan kebarangkalian gagal dan tempoh ulangan. Pertimbangan yang teliti adalah diperlukan sebelum menggunakan model yang dicadangkan ini kerana ia mestilah digunakan bersama pelantar minyak yang mempunyai persamaan dari segi konfigurasi platform, saiz anggota struktur, kedalaman air dan data meteorologi samudera. Ketepatan dan keberkesanan model degradasi yang diusulkan dalam kajian ini akan membantu pengendali di dalam industri untuk membuat keputusan. Lebih penting, dalam menggariskan item tindakan bagi pengurusan risiko perniagaan sekiranya ada hidupan marin, karatan dan enapan yang dijangka akan berlaku.

# **TABLE OF CONTENTS**

# TITLE

DE	CLARATION	iii
DEI	DICATION	iv
AC	KNOWLEDGEMENT	v
ABS	STRACT	vi
ABS	STRAK	vii
TA	BLE OF CONTENTS	viii
LIS	T OF TABLES	xiii
LIS	T OF FIGURES	XV
LIS	T OF ABBREVIATIONS	xviii
LIS	xix	
LIS	T OF APPENDICES	xxii
CHAPTER 1	INTRODUCTION	1
1.1	Background	1
1.2	Problem Statement	4

1.2	I Ioolem Statement	+
1.3	Aims and Research Objectives	5
1.4	Scopes of the Study	6
1.5	Significance of the Study	7
1.6	Thesis Outline	7
CHAPTER 2	LITERATURE REVIEW	9
2.1	Introduction	9
2.2	Platform Degradation Factors	10
	2.2.1 Marine Growth	10
	2.2.2 Corrosion	13
	2.2.3 Subsidence	18
	2.2.4 Fatigue Induced Weld Crack	22

2.2.5 Damaged Member due to Ship Impact 24

	2.2.6	Scour		26
	2.2.7	Summar Factors	y of Review on Platform Degradation	28
2.3			bility Assessment for Fixed Offshore	
	Platfo			31
	2.3.1		al Reliability Assessment Approach	31
	2.3.2	1	e of Structural Reliability Assessment	33
	2.3.3	Structur	al Reliability Assessment Procedure	34
		2.3.3.1	Pushover Analysis	36
		2.3.3.2	Wave Breaking Limit	39
		2.3.3.3	Wave-in-Deck Loads	40
		2.3.3.4	Types of Failure Mechanism	43
		2.3.3.5	Reliability Based Design and Assessment Method	45
2.4	Revie	w on Stru	ctural Reliability Assessment	47
2.5	Resea	rch Gap		51
2.6	Concl	uding Rei	narks	54
CHAPTER 3	RESI	EARCH N	<b>IETHODOLOGY</b>	57
3.1	Introd	luction		57
3.2	Resea	rch Flowe	chart	57
3.3	Analy	vsis Model	Preparation	59
3.4	Conve	ersion and	Verification of Analysis Model	62
3.5	Struct	ural Relia	bility Assessment	63
	3.5.1	Pushove	r Analysis and Reserve Strength Ratio	63
		3.5.1.1	Numerical Example of Reserve Strength Ratio	65
	3.5.2	Extreme	Air Gap Analysis	67
		3.5.2.1	Numerical Example of Maximum Wave Height at Collapse and Wave Breaking Limit	69
	3.5.3	Wave-in	-Deck Load	70
		3.5.3.1	Numerical Example of Wave-in- Deck Load	71

	3.5.4	Probabilit	y of Failure and Return Period	71
		3.5.4.1	Numerical Example of Probability of Failure and Return Period	73
3.6	Develo Ageing Assess	g Fixed	Degradation Limit State Model for Offshore Platform Reliability	75
	3.6.1	Fundamer Model	ntal Basis of Degradation Limit State	75
	3.6.2	Degradati	on Limit State Model Procedures	79
	3.6.3	Proposed State Mod	Comprehensive Degradation Limit lel	84
		3.6.3.1	Single Regression	84
		3.6.3.2	Linear Multi Regression	91
3.7		tion Proce State Mode	esses for the Proposed Degradation	95
3.8	Summ	ary		96
CHAPTER 4	RESU	LTS AND	DISCUSSIONS	99
4.1	Introdu	uction		99
4.2	Test S	tructure Sp	pecification	99
4.3	Dynan	nic and Sta	tic Analysis	101
4.4	Pusho	ver Analys	is	104
	4.4.1	Wave Hei	ight at Collapse	105
	4.4.2	Reserve S	Strength Ratio	106
	4.4.3	Base Shea	ar at Collapse	110
	4.4.4	Mode of I	Failure	114
4.5			f Comprehensive Degradation Limit g Structural Reliability Assessment	116
	4.5.1	Reserve S	strength Ratio	117
		4.5.1.1	Single Regression Model	117
		4.5.1.2	Linear Multi Regression	120
	4.5.2	Probabilit	y of Failure	120
		4.5.2.1	Single Regression Model	120
		4.5.2.2	Linear Multi Regression	123
	4.5.3	Return Pe	riod	123

		4.5.3.1	Single Regression Model	123
		4.5.3.2	Linear Multi Regression	126
4.6	Valida Mode		Proposed Degradation Limit State	126
	4.6.1	Compari	ison of Reserve Strength Ratio	129
		4.6.1.1	Single Regression Model	129
		4.6.1.2	Linear Multi Regression	132
	4.6.2	Compari	ison of Probability of Failure	132
		4.6.2.1	Single Regression Model	132
		4.6.2.2	Linear Multi Regression	135
	4.6.3	Compari	ison of Return Period	135
		4.6.3.1	Single Regression Model	135
		4.6.3.2	Linear Multi Regression	138
	4.6.4	Overall	Discussion	138
4.7	Value	Delivery	and Classification of Benefits	143
4.8	Summ	nary		144
CHAPTER 5	CON	CLUSIO	NS AND RECOMMENDATIONS	147
<b>CHAPTER 5</b> 5.1		CLUSION uction	NS AND RECOMMENDATIONS	<b>147</b> 147
	Introd			
5.1	Introd Overa	uction ll Conclus Researcl Degrada		147 148
5.1	Introd Overa	luction Il Conclus Research Degrada Fixed O Research Compred of Reser and Ret	sion n Objective 1: To Investigate the Primary tion Factors for Comprehensive Ageing ffshore Platforms Model Development n Objective 2: To Develop a hensive Degradation Limit State Model ve Strength Ratio, Probability of Failure urn Period for Ageing Fixed Offshore	147 148 148
5.1	Introd Overa 5.2.1	uction Il Conclus Research Degrada Fixed O Research Comprel of Reser and Ret Platform Research Degrada	sion n Objective 1: To Investigate the Primary tion Factors for Comprehensive Ageing ffshore Platforms Model Development n Objective 2: To Develop a hensive Degradation Limit State Model ve Strength Ratio, Probability of Failure urn Period for Ageing Fixed Offshore IS n Objective 3: To Validate the Proposed tion Limit State Model by Conducting a	147 148 148 149
5.1 5.2	Introd Overa 5.2.1 5.2.2 5.2.2	uction Il Conclus Research Degrada Fixed O Research Comprel of Reser and Ret Platform Research Degrada	sion n Objective 1: To Investigate the Primary tion Factors for Comprehensive Ageing ffshore Platforms Model Development n Objective 2: To Develop a hensive Degradation Limit State Model ve Strength Ratio, Probability of Failure urn Period for Ageing Fixed Offshore as n Objective 3: To Validate the Proposed	147 148 148 149 150
5.1	Introd Overa 5.2.1 5.2.2 5.2.2	uction Il Conclus Research Degrada Fixed O Research Compreh of Reser and Ret Platform Research Degrada Compreh ibutions	sion n Objective 1: To Investigate the Primary tion Factors for Comprehensive Ageing ffshore Platforms Model Development n Objective 2: To Develop a hensive Degradation Limit State Model ve Strength Ratio, Probability of Failure urn Period for Ageing Fixed Offshore IS n Objective 3: To Validate the Proposed tion Limit State Model by Conducting a	147 148 148 149 150 151
5.1 5.2	Introd Overa 5.2.1 5.2.2 5.2.3	uction Il Conclus Research Degrada Fixed O Research Compreh of Reser and Ret Platform Research Degrada Compreh ibutions Academ	sion n Objective 1: To Investigate the Primary tion Factors for Comprehensive Ageing ffshore Platforms Model Development n Objective 2: To Develop a hensive Degradation Limit State Model ve Strength Ratio, Probability of Failure urn Period for Ageing Fixed Offshore as n Objective 3: To Validate the Proposed tion Limit State Model by Conducting a hensive Parametric Study	147 148

# REFERENCES155LIST OF PUBLICATIONS175

## LIST OF TABLES

TABLE NO.	TITLE	PAGE
Table 2.1	Corrosion model for different zone (Zve et al., 2015)	15
Table 2.2	Summary of review on platform degradation factors	28
Table 2.3	Drag coefficient for wave/current on platform deck (ISO, 2007)	43
Table 2.4	Platform exposure category (ISO, 2007)	46
Table 2.5	Development led to this study	51
Table 3.1	Relationship between subsidence depth and structural reliability analysis output	79
Table 3.2	Selected subsidence depth and corrosion depth	80
Table 3.3	Marine growth thickness	80
Table 3.4	Summary of selected single regression model	90
Table 3.5	Relationship between reserve strength ratio, probability of failure and return period $(y)$ and subsidence depth $(x1)$ and corrosion depth $(x2)$	92
Table 3.6	Regression analysis results for reserve strength ratio	93
Table 3.7	Regression analysis results for probability of failure	93
Table 3.8	Regression analysis results for return period	94
Table 4.1	Analysis model specification	100
Table 4.2	Metocean data (Courtesy of Shell)	100
Table 4.3	Governing water depth	102
Table 4.4	Reserve strength ratio comparison	107
Table 4.5	Base shear at collapse comparison	111
Table 4.6	Proposed degradation limit state model for reserve strength ratio	118
Table 4.7	Proposed comprehensive degradation limit state model for probability of failure	120
Table 4.8	Proposed comprehensive degradation limit state model for probability of failure	121

Table 4.9	Proposed comprehensive degradation limit state model for probability of failure	123			
Table 4.10	Proposed comprehensive degradation limit state model for return period				
Table 4.11	Proposed comprehensive degradation limit state model for probability of failure				
Table 4.12	Test structure for validation	127			
Table 4.13	Metocean data (Courtesy of Shell)	128			
Table 4.14	Validation cases	129			
Table 4.15	Validation cases with different subsidence depth	129			
Table 4.16	Reserve strength ratio comparison	132			
Table 4.17	Probability of failure comparison	135			
Table 4.18	Return period comparison	138			
Table 4.19	Summary of reserve strength ratio comparison using single regression method	139			
Table 4.20	Summary of probability of failure comparison using single regression method				
Table 4.21	Summary of return period comparison using single regression method	140			
Table 4.22	Summary of reserve strength ratio comparison using linear multi regression method	141			
Table 4.23	Summary of probability of failure comparison using linear multi regression method	142			
Table 4.24	Summary of return period comparison using linear multi regression method	142			
Table 4.25	Level, types of benefit and reliability acceptance	143			

# LIST OF FIGURES

FIGURE NO	. TITLE	PAGE
Figure 1.1	PETRONAS platform age distribution (Ng et al., 2019)	1
Figure 1.2	Bowtie of existing jacket structure with degradation	3
Figure 2.1	Goodwyn Alpha Platform jacket covered by marine growth (McLean et al., 2019)	11
Figure 2.2	Corroded leg and bracing (El-Reedy, 2012)	14
Figure 2.3	Proposed corrosion model (Jeffrey and Melchers, 2007)	15
Figure 2.4	Probability density versus corrosion damage depth with time for approximate data (Paik and Kim, 2012)	16
Figure 2.5	Offshore platforms with and without subsidence	19
Figure 2.6	Evidence of platform subsidence (Nagel, 2001)	19
Figure 2.7	Subsidence influence diagram (Nagel, 2001)	21
Figure 2.8	Actual weld crack at K-joint of jacket structure (Dong et al., 2012)	23
Figure 2.9	Causes of damage jacket in North Sea (Sharp et al., 1995)	25
Figure 2.10	Big Orange XVIII vessel and Ekofisk 2/4 collision (Sharp et al., 1995)	25
Figure 2.11	Laboratory setup showing local and global scour (MSL Engineering Limited, 2000)	27
Figure 2.12	Reliability verification approaches (Arangio, 2012)	31
Figure 2.13	Fundamental of reliability assessment for offshore structures (Moses and Stahl, 1979)	33
Figure 2.14	Structural reliability assessment procedure (Tromans and van de Graaf, 1992)	35
Figure 2.15	The incremental of 100-year environmental load (DNV GL, 2014)	37
Figure 2.16	Global load versus global displacement and plastic utilisation plot (DNV GL, 2014)	38
Figure 2.17	Global load versus global displacement and plastic utilisation plot (Kajuputra et al., 2016)	39

Figure 2.18	Region of applicability of alternative wave theories and wave breaking limit (ISO, 2007)	40
Figure 2.19	Silhouette area definition (ISO, 2007)	42
Figure 2.20	Failure mechanism in pushover analysis (Ayob et al., 2014)	44
Figure 2.21	Probability of failure of a structure (Mat Soom et al., 2016)	46
Figure 3.1	Research flowchart	58
Figure 3.2	Analysis model preparation procedure in Step A	60
Figure 3.3	Analysis model preparation procedure in Step $B - 1^{st}$ part	61
Figure 3.4	Isometric analysis model	61
Figure 3.5	Conversion and verification procedures in Step $B - 2^{nd}$ part	62
Figure 3.6	Reserve strength ratio and plastic utilisation for the case without wave-in-deck load	66
Figure 3.7	Base shear at collapse and plastic utilisation for the case with wave-in-deck load	67
Figure 3.8	Wave crest height	68
Figure 3.9	Regression model (Paulson, 2007)	76
Figure 3.10	Relationship between reserve strength ratio and platform subsidence	77
Figure 3.11	Relationship between probability of failure and platform subsidence	78
Figure 3.12	Relationship between return period and platform subsidence	78
Figure 3.13	Overall procedures of degradation limit state model	82
Figure 3.14	Relationship between (a) reserve strength ratio, (b) probability of failure and (c) return period and subsidence depth	85
Figure 3.15	Reserve strength ratio for 0mm corrosion (RSR_SR_CORR0)	88
Figure 3.16	Probability of failure for 0mm corrosion (POF_SR_CORR0)	88
Figure 3.17	Return period for 0mm corrosion (RP_SR_CORR0)	89
Figure 3.18	Validation procedure of the proposed degradation limit state model	95
Figure 4.1	Environmental load direction	101
Figure 4.2	Relationship between inertia load and subsidence	103
Figure 4.3	Relationship between 100-year base shear and subsidence	103

Figure 4.4	Wave crest height at collapse	105
Figure 4.5	Reserve strength ratio with wave-in-deck load	107
Figure 4.6	Reserve strength ratio without wave-in-deck load	110
Figure 4.7	Base shear at collapse with wave-in-deck load	111
Figure 4.8	Base shear at collapse without wave-in-deck load	114
Figure 4.9	Failure mode for various subsidence (a) 0 m, (b) 2 m, (c) 4 m, (d) 6 m and (e) 8 m	115
Figure 4.10	Proposed comprehensive degradation limit state models for reserve strength ratio	119
Figure 4.11	Proposed comprehensive degradation limit state models for probability of failure	122
Figure 4.12	Proposed comprehensive degradation limit state models for return period	125
Figure 4.13	Isometric analysis model for PC4-78	127
Figure 4.14	Reserve strength ratio at 4 m, 5 m and 6 m subsidence along with 3 mm corrosion depth	130
Figure 4.15	Reserve strength ratio at 5 m and 6 m subsidence along with 6 mm corrosion depth	131
Figure 4.16	Probability of failure at 4 m and 6 m subsidence along with 3 mm corrosion depth	133
Figure 4.17	Probability of failure at 6 m subsidence along with 6 mm corrosion depth	134
Figure 4.18	Return period at 4 m and 6 m subsidence along with 3 mm corrosion depth	136
Figure 4.19	Return period at 6 m subsidence along with 6 mm corrosion depth	137

# LIST OF ABBREVIATIONS

ALARP	-	As Low As Reasonably Practical
API	-	American Petroleum Institute
AWS	-	American Welding Society
BOS	-	Bottom of Steel
CAPEX	-	Capital Expenditure
COV	-	Coefficient of Variance
EEMUA	-	Engineering Equipment Material Users Association
GUSA	-	Global Ultimate Strength Assessment
HAT	-	Highest Astronomical Height
HSE	-	Health & Safety Executive
HSSE	-	Health, Safety, Security and Environment
ISO	-	International Organization for Standardization
LAT	-	Lowest Astronomical Height
MSL	-	Mean Sea Level
NCS	-	Norwegian Continental Shelf
NORSOK	-	The Norwegian Shelf's Competitive Position Standard
OPEX	-	Operational Expenditure
РМО	-	Peninsular Malaysia Operation
RBDA	-	Reliability Based Design and Assessment
ROV	-	Remotely Operated Vehicle
SACS	-	Structural Analysis Computer Software
SBO	-	Sabah Operation
SKO	-	Sarawak Operation
SRA	-	Structural Reliability Assessment
TOS	-	Top of Steel
UKCS	-	United Kingdom Continental Shelf
USFOS	-	Ultimate Strength of Offshore Structure

# LIST OF SYMBOLS

A	-	environment constant
$A_w$	-	projected area of the wave-in-deck
$C_d$	-	drag coefficient
$C_m$	-	inertia coefficient
$D_L$	-	gravity load
$E_{collapse}$	-	base shear at the collapse of platform / ultimate capacity
$E_{RP}$	-	base shear corresponding to return period
$E_{topsides}$	-	wave-in-deck load
$E_0$	-	environment constant
<i>E</i> <sub>100</sub>	-	base shear of 100-year return period
$f(x_i)$	-	approximate value to the model function
H <sub>max</sub>	-	maximum wave height
h <sub>RSR</sub>	-	maximum wave height at collapse of the platform
$h_{100}$	-	100-year wave height
L	-	load
Ī	-	mean load
$L_D$	-	design load
n	-	total number of dependent variables
$P_E$	-	probability density function
$P_f$	-	probability of failure / failure probability
$P_R$	-	probability density resistance
POF	-	probability of failure
p	-	total number of coefficients
R	-	resistance
$R^2$	-	coefficient of determination
$R_{adj}^2$	-	adjusted coefficient of determination
R	-	mean resistance
$R_i$	-	characteristic resistance
R <sub>mean</sub>	-	mean member capacity or mean member resistance

$\bar{R}_{mean}$	-	mean distribution of structural strength	
RP	-	return period	
RSR	-	reserve strength ratio	
RSS	-	residual sum of squares	
S	-	strength	
S <sub>ult</sub>	-	ultimate strength	
$S_x$	-	strength in X-direction	
$S_y$	-	strength in Y-direction	
T <sub>ass</sub>	-	associated period	
TSS	-	total sum of squares	
U <sub>c</sub>	-	current speed in-line with the wave from metocean data	
$U_w$	-	fluid velocity corresponding to crest height	
x	-	subsidence depth	
<i>x</i> <sub>1</sub>	-	independent variable representing subsidence depth	
<i>x</i> <sub>2</sub>	-	independent variable representing corrosion depth	
у	-	dependent variable representing either reserve strength ratio	
		or probability of failure or return period	
$\overline{\mathcal{Y}}$	-	mean value of either reserve strength ratio or probability of	
		failure or return period	
α	-	constant from metocean data	
$\alpha_1$	-	intercept	
α <sub>2</sub>	-	coefficient of linear term	
α <sub>3</sub>	-	coefficient of quadratic term	
$lpha_4$	-	coefficient of cubic term	
$\alpha_5$	-	coefficient of quartic term	
$\alpha_{cb}$	-	current blockage factor	
$\alpha_L$	-	constant of linearity	
$\alpha_{wk}$	-	wave kinematic factor from metocean data	
$\beta_0$	-	intercept	
$\beta_1$	-	coefficient for subsidence depth	
$\beta_2$	-	coefficient for corrosion depth	
$\gamma_D$	-	gravity load factor	
$\gamma_E$	-	environmental load factor from metocean data	

δ	-	displacement
$\phi_i$	-	resistance factor
$ ho_w$	-	density of seawater
$\sigma_R$	-	standard deviation of the distribution of structural strength

## LIST OF APPENDICES

APPENDIX		TITLE	PAGE	
Appendix A	Analysis Results		169	
Appendix B	Research Output		173	

#### **CHAPTER 1**

#### **INTRODUCTION**

## 1.1 Background

Anglo-Saxon Petroleum Company, owned by Royal Dutch Shell, discovered the first commercial oil well in Malaysia in 1910. It was located at onshore field in Miri, Sarawak (Seong and Hong, 1995; Sorkhabi, 2010). The discovery marked the starting point of petroleum industry in Malaysia. Over the years, exploration was extended to offshore location which brought West Lutong oilfield in Sarawak as the first offshore oilfield which started operating in 1968 (Abdul Rahim and Liwan, 2012). In 2000, there were more than 300 offshore platforms in Malaysia operated by PETRONAS Peninsular Malaysia Operation (PMO), Sarawak Operation (SKO) and Sabah Operation (SBO) (Wan Abdullah Zawawi et al., 2012). According to Ng et al. (2019), more than 50 % of platforms in Malaysia operate for more than 25 years as shown in Figure 1.1. The oldest platform owned by PETRONAS is already in operation for 50 years (Ng et al., 2019).

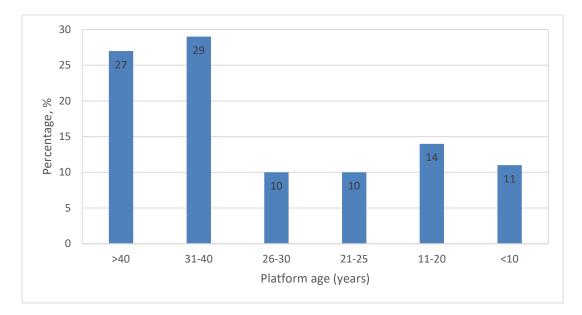


Figure 1.1 PETRONAS platform age distribution (Ng et al., 2019)

Ageing platforms are either decommissioned or go through a series of structural integrity assessment for life extension. Structural integrity assessment is crucial to ensure offshore platforms are able to operate safely and avoid structural failure. There are two factors that may affect the structural integrity of offshore platforms. They are excessive load and insufficient strength (Ayob et al., 2014; Kajuputra et al., 2016). The excessive load may come from environmental load, operational load, and accidental load. Whereas insufficient strength may cause by error in design, fabrication, installation, operation, and degradation. Degradation is critical in ensuring the integrity of platforms as the operators opt to extend their platform service life beyond the original design life (Shanker, 2018).

The structural integrity of ageing platform affected by various degradation factor throughout its service life. For example, they are corrosion, marine growth, weld crack, scour, subsidence, and damaged structural member due to boat impact (Ng et al., 2019; McLean et al., 2019; Dehghani and Aslani, 2019). Degraded offshore structure will reduce the structural integrity over time (Gholami et al., 2018). Hence, it is crucial to consider degradation in the structural integrity assessment to ensure the result represents actual condition at site. This study considers degradation, which are marine growth, corrosion, and subsidence in structural reliability assessment (SRA).

Structural reliability assessment (SRA) is not new to oil and gas industries as it has been applied to offshore structure since 1960s (Cornell, 1995). According to Szalewski (2019), structural reliability assessment can provide confidence level required by regulators and stakeholders. It is achieved by maintaining the target safety level beyond the original design life. One of structural reliability assessment component is pushover analysis (Tromans and van de Graaf, 1992; Ayob et al., 2014; Mat Soom et al., 2018), which has been performed to generate the reserve strength ratio. Subsequently, reserve strength ratio is utilised to determine annual probability of failure and return period of platform. Both probability of failure and return period of platform are important for the operator to justify the risk to their assets.

Bow-tie diagram is widely adopted in risk analysis. In order to present the background of problem of existing ageing structure, bow-tie diagram has been utilised

as shown in Figure 1.2. It comprises of fault trees and event trees, which are connected to hazardous event or top event (Lu et al., 2015; Vileiniskis and Remenyte-Prescott, 2017). The fault tree is divided into hazard and threat, while event tree is consequences of hazardous event. Bow-tie diagram is one of Health, Safety, Security and Environment (HSSE) tool support for as Low as Reasonably Practicable (ALARP) (Valeur, 2014).

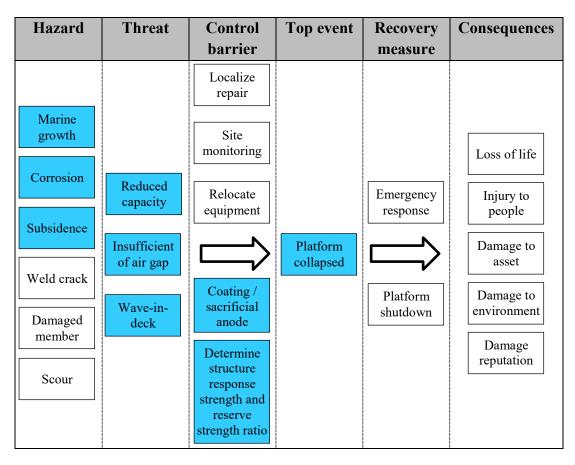


Figure 1.2 Bowtie of existing jacket structure with degradation

Based on Figure 1.2, the problem is triggered by platform degradation such as corrosion, subsidence, marine growth, weld crack, damaged member, and scour (Ng et al., 2019; McLean et al., 2019; Dehghani and Aslani, 2019). This will lead to reduction of platform carrying capacity and insufficient of air gap with a possibility of wave-in-deck. Depending on the type of degradation, control barrier that may be introduced are localized repair, site monitoring, relocation of equipment, coating, or sacrificial anode. Operator may also choose to determine the structure response and reserve strength ratio to ensure the strength of structure is sufficient. Ineffective or

failure of control barrier may cause hazardous event or top event which is platform collapse.

As a recovery measure, emergency response will be activated, and platform will be shut down as soon as possible to contain leak from live piping or wells. Consequences of platform collapse can be loss of life, injury to people, damage to assets and damage to environment (Azman et al., 2019). This study focused on three degradation issues which are marine growth, corrosion and subsidence and associated threat, control barrier and top event as shaded in blue in Figure 1.2.

## **1.2 Problem Statement**

Ageing platforms are growing in numbers worldwide. To improve economic viability and increase profitability, operators choose to extend the platform life beyond the original design life (Aeran et al., 2017; Animah and Shafiee, 2018). Life extension also reduces both capital expenditure (CAPEX) and operational expenditure (OPEX) of an offshore platform (Shafiee and Animah, 2017). Structural reliability assessment has been widely adopted in oil and gas industry and has been utilised by operator to quantify whether ageing platform life can be extended, as studied by Mat Soom et al. (2016) and Copello et al. (2017).

However, structural reliability assessment is complex and time-consuming. The conventional procedure explained by Tromans and van de Graaf (1992) and Mat Soom et al. (2019) comprises of data collection, structural modelling, and preparation, hindcast study, pushover analysis and calculation of probability of failure and return period. It is estimated that engineer requires two (2) months to complete per cycle of structural reliability assessment for specific magnitude of degradation per platform with industrial manhours of approximately 280 manhours (total manhours from principle and senior engineer). Thus, by utilising the proposed model, an engineer is able to save time as the reserve strength ratio, probability of failure and return period have been calculated depending on degradation level. This study will help industry to determine the results even before the actual degradation occur hence will save a

significant time and minimise the use of resources as the resources may contribute to better field economics.

Based on the review performed on structural reliability assessment, majority of the author did not clearly specify whether degradation has been included as part of their structural reliability assessment. Even if the author considered degradation, only single factor was highlighted as part of their study. However, there are chances that several degradation factors may occur at the same time. It is also an industry requirement to consider degradation such as marine growth and corrosion depth as during design and assessment of fixed offshore platform. Furthermore, the author concentrated on specific value of degradation, whereas this study considered multiple degradation magnitude so that industry will be able to choose a correct model once survey data is available.

It is also noted that limited study has been conducted on the relationship between reserve strength ratio, probability of failure and return period, and degradation faced by fixed offshore structures. This study considered constant marine growth, corrosion, and subsidence to determine the impact of degradation to structural reliability assessment by developing a comprehensive degradation limit state model. Corrosion was applied in the splash zone area by reducing the structural member thickness. Subsidence effects, which include reduction of air gap and wave-in-deck were considered in the proposed model as the effects of wave-in-deck load are excluded during reserve strength ratio determination.

#### **1.3** Aims and Research Objectives

The aim of the study is to develop a comprehensive regression limit state model of reserve strength ratio, probability of failure and return period by considering degradation in the structural reliability assessment of ageing fixed offshore platforms. The proposed model is expected to provide an immediate result in order to determine whether there is a need to perform a comprehensive structural reassessment. To achieve these aims, three objectives are set as follows:

- To investigate the primary degradation factors for comprehensive ageing fixed offshore platforms model development.
- To develop a comprehensive degradation limit state model of reserve strength ratio, probability of failure and return period for ageing fixed offshore platforms.
- iii) To validate the proposed degradation limit state model by conducting a comprehensive parametric study.

#### 1.4 Scopes of the Study

This study focused on 4-legged fixed offshore jacket structures. Three degradation factors were considered in structural reliability assessment. They are marine growth, corrosion, and subsidence. Marine growth is considered constant throughout the analysis. The thickness was based water fixed offshore platform located at East Malaysian water. The value was adopted by industry, which was based on the actual survey. Corrosion was considered up to 12 mm at the splash zone area, while subsidence is considered up to 8 m. Both corrosion and subsidence values were chosen based on the predicted value at platform location. Reliability Based Design and Assessment as explained by Mat Soom et al. (2016) was utilised to calculate the probability of failure and return period of the platform. The target probability of failure and return period of the platform. The target probability of failure and return period of the platform. The target probability of failure and return period of the platform.

Existing analysis model were used and verified using Structural Analysis Computer Software (SACS). The software is widely used in the industry especially for the fixed jacket offshore structure. It is capable to perform linear static analysis and built-in with several code checks such as International Organization for Standardization (ISO), American Petroleum Institute (API) and Norwegian Shelf's Competitive Position Standard (NORSOK). Ultimate Strength for Offshore Structures (USFOS) computer programme was utilised to determine the reserve strength ratio. The software is widely used by the industry for nonlinear structural analysis. The regression analysis was performed to identify and develop the most comprehensive model for reserve strength ratio, probability of failure and return period of ageing fixed offshore structure. Details of the method were elaborated further in *Chapter 3*.

#### **1.5** Significance of the Study

A comprehensive regression model of probability of failure considering degradation, which are marine growth, corrosion, and subsidence in structural reliability assessment were introduced in this study. The proposed model is efficient and economical in terms of time and the use of resources as engineers do not need to run a full cycle of structural reliability assessment, which is time consuming. What engineers need to do are to find the degradation value to estimate the reserve strength ratio, probability of failure and return period, and compare the results with industry standard which is ISO (2007).

By systematically considers marine growth, corrosion, and subsidence in structural reliability assessment, it is expected that degradation effect will be predicted accurately. Outcomes from this study shall also allow the operator to decide and to outline the action for their business risk management in case where marine growth, corrosion and subsidence is expected to occur. This is important as it involves quality, safety, and cost, especially when the collapse of the platform potentially involves the loss of life, damage to assets and damage to environment.

#### **1.6** Thesis Outline

Chapter 1 describes the introduction of this thesis, which includes general background of oil and gas scenes in Malaysia, brief description of degradation issue and an introduction of structural reliability assessment. This chapter also include

detailed problem statement, aims and objectives, scopes, and significance of the study and lastly thesis outline.

**Chapter 2** contains the review of literature of this study. It includes platform degradation factors such as marine growth, corrosion, subsidence, weld crack, damaged member and scour and theories behind the study. This chapter explains the approach, principle and procedure of structural reliability assessment. This chapter also provides review on structural reliability assessment, which has been adopted in oil and gas industry and its development.

**Chapter 3** explains research methodology in detail including research flowchart and structural model preparation. This chapter also explains the methodology of structural reliability assessment. The development of degradation limit state model is taking into account marine growth, corrosion, and subsidence. These were elaborated in detail, together with numerical example of proposed method. This chapter also provides validation process of the proposed degradation limit state model.

**Chapter 4** discusses the structural reliability assessment results from pushover analysis, extreme air gap analysis and regression analysis of the proposed degradation limit state model. This chapter also includes validation of the proposed degradation limit state model by comparing the reserve strength ratio, probability of failure and return period.

**Chapter 5** concludes the objective of the study. Apart from that, it also contains the contribution of current study and recommendation for future. List of publications, innovations and intellectual properties are also part of this chapter.

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