

PREMATURE FAILURE DETECTION OF DISTRIBUTION TRANSFORMER  
WITH UNBALANCED HARMONIC LOADS USING HOTSPOT  
TEMPERATURE ANALYSIS

ZARIS IZZATI BINTI MOHD YASSIN

UNIVERSITI TEKNOLOGI MALAYSIA

PREMATURE FAILURE DETECTION OF DISTRIBUTION TRANSFORMER  
WITH UNBALANCED HARMONIC LOADS USING HOTSPOT  
TEMPERATURE ANALYSIS

ZARIS IZZATI BINTI MOHD YASSIN

A thesis submitted in fulfilment of the  
requirements for the award of the degree of  
Doctor of Philosophy

School of Electrical Engineering  
Faculty of Engineering  
Universiti Teknologi Malaysia

FEBRUARY 2022

## ACKNOWLEDGEMENT

With the name of Allah SWT the most gracious, the most merciful and His messenger, Muhammad PBUH...

First and foremost, this humble gratitude solely belongs to Allah SWT upon His love, guidance and mercy this thesis finally be able to complete as the best it can be.

In particular, I would like to give my most appreciation to these valuable people of my life, who were there from day one until the end of this road. My dedicated supervisor, Assoc. Prof. Ts. Dr. Dalila Mat Said and co-supervisor, Assoc. Prof. Ir. Dr. Hayati Abdullah, in their lots of commitments, contributions and patiently led me the correct way in my research. The love of my life, my husband, Mr. Tuan Mohd Faiz Tuan Borhanuddin and my beautiful daughters Tuan Airina Eshal and Tuan Aisha Eilana. My beloved heroes' figures and role models, Tuan Haji Mohd Yassin Mohd Shariff and Puan Hajjah Halimah Saidin. My precious siblings, Dr. Airil Yasreen and spouse, Dr. Halinawati, Mr. Airil Hafizal and spouse, Mrs. Hawa, Mr. Airil Syazni and spouse, Mrs. Farah Yasmin, Dr. Nurain Izzati and spouse, Dr. Al Akhbar and Mr. Airil Ikmal. My prides and joys, Airil Haziq, Hasya 'Ainaa, Nurina Fatihah, Nuha Liyana, Nurina Dhiya, Hafsa Binish and Airil Hafiz. Also, not to be forgotten, my kind, warmth and supportive in-laws.

This appreciation extends to my fellow research mates in Centre of Electrical Energy (CEES) and The Doctor Strange for their tremendous support. And last but not least to all good people that have come crossed in my life either directly or indirectly. I could not thank you all enough for the presents, loves, understanding, wise words, lend me the shoulder and ear whenever I lost the grip and will. I pray that all of you will be granted with successful life in dunya akhirah, and may Allah keep us together in His highest paradise ultimately.

## ABSTRACT

Harmonics distortion is the most prominent power quality problem in an electrical power distribution network that interrupts a good quality of electric power to be drawn in the network. Additionally, the major impact of harmonics distortion is the risk of the distribution transformer failure due to the elevation of power losses and hotspot temperature (HST) in its three-phase low voltage (LV) winding cables. The major challenge is to identify the exact location and point where the premature failure could occur on the three-phase cables. This research proposes an HST mathematical expression to detect a premature failure at the three-phase LV winding along with the transformer loading. As most transformer failure cases were rooted in heat losses that require meticulous analysis, the best accuracy numerical method as Finite Element Method (FEM) is selected to analyse the HST of the thermal distribution transformer model. The HST is simulated by considering the three-phase unbalanced harmonic loads from three different group levels of THDI and under five different insulation temperature classes system. The simulation outputs are then verified with HST results from the HST mathematical model based on IEEE C57.110-2018 standard. Further analysis of the simulation results has been done to propose the HST mathematical expression, which will be assessed on the three-phase LV winding cables to detect premature failure. At the end of this research, it is found that the individual harmonic currents from the 7th until 19th order are the prominent harmonic orders that had exceeded the limit of MS 1555 (IEC 61000-3-4) standard. Other than that, based on the proposed HST mathematical expression, it is found out that if the transformer is being loaded with loading over 0.9 pu, the premature failure is expected to occur promptly in the group of THDI peak-level, prominently at 180, 200 and 220 insulation temperature classes. As for the lifetime expectancy of the distribution transformer, if the transformer is loaded with loading at 0.9 pu and above, the lifetime is approximated to drop by the minimum at 14.5% and maximum at 56% from its expectancy lifetime. Plus, it is also concluded that the possibility of the lifetime reduction to be happened at the premature failure point at average of 93.5%, 85.4% and 78% of the THDI peak-level, THDI average-level and THDI low-level correspondingly. Hence, the findings have successfully shown the proposed method's effectiveness in vividly viewing the distribution transformer's current condition. Upon the early detection of the premature failure on the three-phase cables, the execution of the proposed HST mathematical expression is also able to identify the exact location and point where the premature failure shall happen. Thus, it outright protects the distribution transformer from any unwanted breakdown, next preserves its best performance and lifetime expectancy.

## ABSTRAK

Gangguan harmonik ialah masalah utama di dalam rangkaian elektrik kuasa, yang mana ianya mengganggu kualiti kuasa yang terbaik untuk mengalir di dalam rangkaian tersebut. Tambahan lagi, kesan utama gangguan harmonik ini ialah risiko kegagalan pada alat pengubah agihan yang berpunca daripada peningkatan dalam kehilangan kuasa dan suhu titik panas (*HST*) di atas kabel voltan rendah (*LV*) tiga fasanya. Cabaran utama adalah untuk mengenal pasti lokasi dan titik tepat di mana berkemungkinan terjadi kegagalan pramatang pada kabel tiga fasa. Kajian ini mencadangkan ekspresi matematik *HST* untuk mengesan kemunculan kegagalan pramatang pada kabel *LV* tiga fasa di sepanjang muatan alat pengubah agihan. Sebagaimana kebanyakan kes - kes kegagalan pengubah berpunca daripada kehilangan haba yang memerlukan analisis yang teliti, keadah numerikal yang tepat seperti *Finite Element Method (FEM)* dipilih untuk menganalisa suhu titik panas (*HST*) pada model termal pengubah agihan. *HST* disimulasi dengan mengambilkira keadaan muatan harmonik tidak seimbang tiga fasa yang diperoleh daripada tiga kumpulan aras gangguan arus harmonik (*THDI*) dan pada lima sistem kelas penambat suhu yang berbeza. Hasil keputusan daripada simulasi tersebut kemudiannya diverifikasi dengan hasil keputusan *HST* yang diperoleh daripada model matematik *HST* berdasarkan kepada piawaian di dalam IEEE C57.110-2018. Tambahan analisis kepada keputusan simulasi tersebut dilakukan bagi mengemukakan ekspresi matematik *HST* di mana akan ditaksir pada kabel *LV* tiga fasa untuk mengesan kegagalan pramatang pada alat pengubah agihan. Di akhir kajian ini, telah didapati arus harmonik individu yang bermula dari jujukan susunan 7<sup>th</sup> sehingga 19<sup>th</sup> adalah merupakan jujukan yang paling ketara dalam melepasi batas piawai MS 1555 (IEC 61000-3-4). Selain daripada itu, berdasarkan kepada ekspresi matematik *HST* yang dikemukakan, sekiranya muatan pengubah melebihi 0.9 p.u, kegagalan pramatang dianggar akan berlaku pada kumpulan aras *THDI* tertinggi (*THDI peak-level*), terutamanya dalam sistem kelas penambat suhu 180, 200 dan 220. Bagi jangkaan hayat pengubah agihan pula, sekiranya muatan pengubah pada 0.9 p.u dan ke atas, jangkaan hayat dianggarkan akan menurun secara minimumnya sebanyak 14.5% dan maksimumnya sebanyak 56%. Tambahan, ianya juga boleh disimpulkan bahawa kemungkinan pengurangan jangka hayat pengubah terjadi pada ketika kegagalan pramatang berlaku adalah secara puratanya pada 93.5%, 85.4% dan 78% di dalam gangguan arus harmonik yang paling tinggi (*THDI peak-level*), aras sederhana (*THDI average-level*) dan aras rendah (*THDI low-level*) masing - masing. Maka berdasarkan kepada penemuan - penemuan tersebut, ianya telah menunjukkan keberkesanan metodologi yang dicadangkan untuk memaparkan secara jelas keadaan semasa alat pengubah agihan tiga fasa. Di atas pengesanan awal kegagalan pramatang pada kabel tiga fasa, pelaksanaan ekspresi matematik *HST* yang dikemukakan ini juga dapat mengenal pasti lokasi dan titik tepat di mana kegagalan pramatang bakal berlaku. Maka ia serta merta dapat melindungi alat pengubah agihan tersebut daripada kerosakkan yang tidak diingini, seterusnya dapat memelihara prestasi terbaik dan jangkaan hayatnya

## TABLE OF CONTENTS

	TITLE	PAGE
	<b>DECLARATION</b>	<b>iii</b>
	<b>DEDICATION</b>	<b>iv</b>
	<b>ACKNOWLEDGEMENT</b>	<b>v</b>
	<b>ABSTRACT</b>	<b>vi</b>
	<b>ABSTRAK</b>	<b>vii</b>
	<b>TABLE OF CONTENTS</b>	<b>viii</b>
	<b>LIST OF TABLES</b>	<b>xiii</b>
	<b>LIST OF FIGURES</b>	<b>xiv</b>
	<b>LIST OF ABBREVIATIONS</b>	<b>xviii</b>
	<b>LIST OF SYMBOLS</b>	<b>xix</b>
	<b>LIST OF APPENDICES</b>	<b>xxi</b>
<b>CHAPTER 1</b>	<b>INTRODUCTION</b>	<b>1</b>
	1.1 Research background	1
	1.2 Problem statement	5
	1.3 Research objectives	7
	1.4 Research scopes	7
	1.5 Research contributions	9
	1.6 Thesis outlines	10
<b>CHAPTER 2</b>	<b>LITERATURE REVIEW</b>	<b>11</b>
	2.1 Introduction	11
	2.2 The Importance Aspects of Unbalanced Harmonic Loads in Distribution Transformer Analysis	11
	2.3 Failure Determination in the Distribution transformer upon the Unbalanced Harmonic Loads	13
	2.4 Contribution of Harmonic Loads Behavior towards Temperature Rise and HST in the Distribution Transformer.	18

2.5	Existing Premature Failure Approach in the Distribution Transformer	20
2.5.1	Transformer Simulation Model Approach	20
2.5.1.1	Transient Analysis Using FEM	20
2.5.1.2	Analytical Solution Analysis	23
2.5.2	Power Quality and Load Parameter Measurement Approach	24
2.5.3	Laboratory Testing with Statistical Distribution Approach	28
2.6	Research gaps	32
2.7	Chapter Summary	33
<b>CHAPTER 3</b>	<b>RESEARCH METHODOLOGY</b>	<b>35</b>
3.1	Introduction	35
3.2	Part A: Information gathering, calculation on rated value, field data measurement and data assembly	37
3.2.1	Specification technical data of distribution transformer	39
3.2.2	International standard bodies	40
3.2.3	Rated power losses and hotspot temperature of distribution transformer	43
3.2.3.1	Rated power losses calculation for distribution transformer	43
3.2.3.2	Rated hotspot temperature of distribution transformer	45
3.2.4	Field data measurement of the unbalanced harmonic load from the low voltage distribution network	46
3.2.4.1	Distribution network environment	47
3.2.4.2	Placement of Fluke 1750 power quality logger	48
3.2.5	Assembly of unbalanced harmonic loads data	51
3.2.5.1	Exporting the unbalanced harmonic loads into data storage	52
3.3	Part B: Harmonic current composition, implementation of distribution transformer model and result validation	54

3.3.1	Real power losses based on the unbalanced harmonic loads' composition	56
3.3.2	Thermal distribution transformer model using Finite Element Method (FEM) approach	57
3.3.3	The material properties setting of the thermal distribution transformer model	58
3.3.4	The heat transfer of the thermal distribution transformer model	62
3.3.4.1	The boundary condition (b.c) settings	62
3.3.4.2	The heat source on the specific LV winding location	63
3.3.4.3	The heat transfer and multiphysics coupling solution study	64
3.3.5	The mesh and HST evaluation region of the thermal distribution transformer model	65
3.3.6	IEEE HST mathematical model using IEEE standard	66
3.3.7	Results validation between IEEE and FEM	68
3.4	Part C: Expression of premature failure condition by mathematical formula derivation and estimation of real lifetime of the distribution transformer	69
3.4.1	Mathematical expression of the distribution transformers' premature failure condition	71
3.4.2	Proposed HST of premature failure mathematical expression	72
3.4.3	Results validation between IEEE, FEM, and derived polynomial function	73
3.5	Real lifetime estimation of distribution transformer	74
3.6	Chapter summary	76
<b>CHAPTER 4</b>	<b>RESULTS AND DISCUSSIONS</b>	<b>77</b>
4.1	Introduction	77
4.2	Comparison of measured harmonic data with MS 1555:2002 (IEC 61000-3-4)	78
4.2.1	THDI range at the peak level	78
4.2.2	THDI range at the average level	80
4.2.3	THDI range at the low level	82

4.3	LV winding eddy current load losses ( $P_{ec}$ )	84
4.4	HST at every insulation temperature class system ( $\theta_{HS}$ )	87
4.4.1	HST at 130 insulation temperature class ( $\theta_{HS-130}$ )	88
4.4.2	HST at 150 insulation temperature class ( $\theta_{HS-150}$ )	91
4.4.3	HST at 180 insulation temperature class ( $\theta_{HS-180}$ )	95
4.4.4	HST at 200 insulation temperature class ( $\theta_{HS-200}$ )	98
4.4.5	HST at 220 insulation temperature class ( $\theta_{HS-220}$ )	102
4.5	Results validation	106
4.5.1	Validation between IEEE and FEM	106
4.5.2	Validation between IEEE, FEM, and derived polynomial function	111
4.6	HST of premature failure at every insulation temperature class system ( $\theta_{HSpre}$ )	118
4.6.1	HST of premature failure at 130 insulation temperature class ( $\theta_{HSpre-130}$ )	119
4.6.2	HST of premature failure at 150 insulation temperature class ( $\theta_{HSpre-150}$ )	122
4.6.3	HST of premature failure at 180 insulation temperature class ( $\theta_{HSpre-180}$ )	124
4.6.4	HST of premature failure at 200 insulation temperature class ( $\theta_{HSpre-200}$ )	127
4.6.5	HST of premature failure at 220 insulation temperature class ( $\theta_{HSpre-220}$ )	130
4.7	Real lifetime estimation of the distribution transformer	134
4.7.1	Real lifetime estimation at 130 insulation temperature class	134
4.7.2	Real lifetime estimation at 150 insulation temperature class	135
4.7.3	Real lifetime estimation at 180 insulation temperature class	136

4.7.4	Real lifetime estimation at 200 insulation temperature class	137
4.7.5	Real lifetime estimation at 220 insulation temperature class	138
4.8	Chapter summary	139
<b>CHAPTER 5</b>	<b>CONCLUSION AND RECOMMENDATIONS</b>	<b>143</b>
5.1	Conclusion	143
5.2	Recommendations	145
<b>REFERENCES</b>		<b>147</b>
<b>APPENDIX A</b>		<b>159</b>
<b>APPENDIX B1</b>		<b>164</b>
<b>APPENDIX B2</b>		<b>169</b>
<b>APPENDIX B3</b>		<b>175</b>
<b>APPENDIX B4</b>		<b>178</b>
<b>APPENDIX C</b>		<b>182</b>
<b>LIST OF PUBLICATIONS</b>		<b>184</b>

## LIST OF TABLES

TABLE NO.	TITLE	PAGE
Table 2.4	The extracted details remarks from the age assessment reports	31
Table 3.1	Specification of distribution transformer at the substation	40
Table 3.2	Current distortion limits for systems rated 120 V through 69 kV	41
Table 3.3	Stage 1 current emission values for simplified connection equipment	42
Table 3.4	Recommended temperature rise limits over ambient temperature when loading beyond nameplate rating for dry type distribution transformer	46
Table 3.5	Material properties for copper	60
Table 3.6	Material properties for iron	60
Table 3.7	Material properties for air	60
Table 3.8	Constants for lifetime equation	75
Table 4.1	Data comparison for (19% < THDI < 22%)	79
Table 4.2	Data comparison for (16% < THDI < 18%)	81
Table 4.3	Data comparison for (12% < THDI < 15%)	83
Table 1.1	$\Theta_{HS-130}$ similarity percentage of a derived polynomial function to IEEE and FEM	113
Table 1.5	$\Theta_{HS-150}$ similarity percentage of a derived polynomial function to IEEE and FEM	114
Table 1.6	$\Theta_{HS-180}$ similarity percentage of a derived polynomial function to IEEE and FEM	115
Table 1.7	$\Theta_{HS-200}$ similarity percentage of a derived polynomial function to IEEE and FEM	116
Table 1.8	$\Theta_{HS-220}$ similarity percentage of a derived polynomial function to IEEE and FEM	117
Table C.1	Summary of premature failure of distribution transformer	183

## LIST OF FIGURES

<b>FIGURE NO.</b>	<b>TITLE</b>	<b>PAGE</b>
Figure 2.1	Transformer primary (solid lines) and secondary (dashed lines) winding currents for unbalanced linear and nonlinear loads	14
Figure 2.2	The transformer hotspot temperature versus the load factor of the transformer	16
Figure 2.3	The transformer remaining life versus load factor of the transformer	16
Figure 2.4	Graph of residual life of the insulation of ideal and target (studied) distribution transformer.	30
Figure 3.1	Flowchart of overall research's activities	36
Figure 3.2	Flowchart of research methodology by Part A	38
Figure 3.3	500 kVA distribution transformer in the substation chamber	39
Figure 3.4	The distribution network environment	47
Figure 3.5	Placement of 1750 power quality logger at LV network	48
Figure 3.6	Fluke 1750 three-phase power quality logger	49
Figure 3.7	Power logger connection setup at the substation	50
Figure 3.8	Wiring connection diagram of current clamps and voltage clips on power quality logger	50
Figure 3.9	Power Fluke 1750 – desktop monitor connection for online monitoring	51
Figure 3.10	Scope snapshot of recorded data from the substation	52
Figure 3.11	Snapshot of recorded harmonics data from the substation	52
Figure 3.12	Sample of unbalanced harmonic current in the data storage file	53
Figure 3.13	Flowchart of research methodology by Part B	55
Figure 3.14	The 2D cross-section of the dry type geometry transformer model	58
Figure 3.15	The copper material for the LV winding domain of the transformer	59

Figure 3.16	The iron material for the core domain of the transformer	59
Figure 3.17	The air material for the coolant domain of the transformer	59
Figure 3.18	The heat transfer Neumann boundary condition of the core	62
Figure 3.19	The heat transfer boundary of the LV winding	63
Figure 3.20	The heat source domain of the LV winding	64
Figure 3.21	The final discretised mesh of the thermal distribution transformer model	66
Figure 3.22	The HST mathematical model for the distribution transformer	68
Figure 3.23	Flowchart of research methodology by Part C	70
Figure 3.24	Result of $R^2$ trend line testing of linear, exponential, and polynomial regression function	72
Figure 3.25	Example of HST result graph	73
Figure 4.1	Graph of $P_{ec}$ losses (W) versus load (pu) at THDI peak-level	85
Figure 4.2	Graph of $P_{ec}$ losses (W) versus load (pu) at THDI average-level	85
Figure 4.3	Graph of $P_{ec}$ losses (W) versus load (pu) at THDI low-level	85
Figure 4.4	Comparison in $P_{ec}$ losses (W) in each of THDI level	86
Figure 4.5:	Polynomial quadratics' correlation coefficient, $R^2$ for $P_{ec}$ losses (W) at pu loading	87
Figure 4.6	$\theta_{HS-130}$ at THDI peak-level from FEM thermal distribution transformer model	89
Figure 4.7	$\theta_{HS-130}$ at THDI average-level from FEM thermal distribution transformer model	89
Figure 4.8	$\theta_{HS-130}$ at THDI low-level from FEM thermal distribution transformer model	90
Figure 4.9	$\theta_{HS-150}$ at THDI peak-level from FEM thermal distribution transformer model	92
Figure 4.10	$\theta_{HS-150}$ at THDI average-level from FEM thermal distribution transformer model	93
Figure 4.11	$\theta_{HS-150}$ at THDI low-level from FEM thermal distribution model	93

Figure 4.12	$\theta_{HS-180}$ at THDI peak-level from FEM thermal distribution model	96
Figure 4.13	$\theta_{HS-180}$ at THDI average-level from FEM thermal distribution model	96
Figure 4.14	$\theta_{HS-180}$ at THDI low-level from FEM thermal distribution model	97
Figure 4.15	$\theta_{HS-200}$ at THDI peak-level from FEM thermal distribution model	99
Figure 4.16	$\theta_{HS-200}$ at THDI average-level from FEM thermal distribution model	100
Figure 4.17	$\theta_{HS-200}$ at THDI low-level from FEM thermal distribution model	100
Figure 4.18	$\theta_{HS-220}$ at THDI peak-level from FEM thermal distribution model	103
Figure 4.19	$\theta_{HS-220}$ at THDI average-level from FEM thermal distribution model	103
Figure 4.20	$\theta_{HS-220}$ at THDI low-level from FEM thermal distribution model	104
Figure 4.21	$\theta_{HS-130}$ comparison in FEM and IEEE approach for THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	107
Figure 4.22	$\theta_{HS-150}$ comparison in FEM and IEEE approach for THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	108
Figure 4.23	$\theta_{HS-180}$ comparison in FEM and IEEE approach for THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	109
Figure 4.24	$\theta_{HS-200}$ comparison in FEM and IEEE approach for THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	110
Figure 4.25	$\theta_{HS-220}$ comparison in FEM and IEEE approach for THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	111
Figure 4.26	$\theta_{HS-130}$ comparison in FEM, IEEE and derived polynomial function for THDI peak-level (a), THDI average-level (b) and THDI low-level (c).	112
Figure 4.27	$\theta_{HS-150}$ comparison in FEM, IEEE and derived polynomial function for THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	113

Figure 4.28	$\theta_{HS-180}$ comparison in FEM, IEEE and derived polynomial function for THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	114
Figure 4.29	$\theta_{HS-200}$ comparison in FEM, IEEE and derived polynomial function for THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	116
Figure 4.30	$\theta_{HS-220}$ comparison in FEM, IEEE and derived polynomial function for THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	117
Figure 4.31	$\theta_{HSpre-130}$ at THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	121
Figure 4.32	$\theta_{HSpre-150}$ at THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	124
Figure 4.33	$\theta_{HSpre-180}$ at THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	127
Figure 4.34	$\theta_{HSpre-200}$ at THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	130
Figure 4.35	$\theta_{HSpre-220}$ at THDI peak-level (a), THDI average-level (b) and THDI low-level (c)	133
Figure 4.36	Real lifetime by THDI peak-level, THDI average-level and THDI low-level at 130 insulation temperature class	135
Figure 4.37	Real lifetime by THDI peak-level, THDI average-level and THDI low-level at 150 insulation temperature class	136
Figure 4.38	Real lifetime by THDI peak-level, THDI average-level and THDI low-level at 180 insulation temperature class	137
Figure 4.39	Real lifetime by THDI peak-level, THDI average-level and THDI low-level at 200 insulation temperature class	138
Figure 4.40	Real lifetime by THDI peak-level, THDI average-level and THDI low-level at 220 insulation temperature class	139

## LIST OF ABBREVIATIONS

AC	-	Alternating Current
CPU	-	Central Processing Unit
DGA	-	Dissolve Gas Analysis
DP	-	Degree of Polymerization
EC	-	Eddy Current
EV	-	Electric Vehicle
FCM	-	Fuzzy C-Means
FEM	-	Finite Element Method
HST	-	Hotspot Temperature
LV	-	Low Voltage
MQ	-	Family of Gas Sensor
PCC	-	Point of Common Coupling
PEV	-	Plug-In Electric Vehicle
PQ	-	Power Quality
PSO	-	Particle Swarm Optimization
PV	-	Photovoltaic
RBF	-	Radial Basis Function
RMS	-	Root Mean Square
T1	-	Transformer 1
T2	-	Transformer 2
TDD	-	Total Demand Distortion
THD	-	Total Harmonic Distortion
THDV	-	Total Harmonic Distortion Voltage
THDI	-	Total Harmonic Distortion Current
WHF	-	Two Dimensional

## LIST OF SYMBOLS

$F_{HL}$	-	Harmonic Loss Factor
$F_{HLe c}$	-	Harmonic Loss Factor for Eddy Current
$F_{HLo s l}$	-	Harmonic Loss Factor for Other Stray Part
$F_{HL} P_{ec} P_{ec}$	-	Corrected Real Eddy Current Power Load Loss
$\beta$	-	Real Load Factor
$P_{NL}$	-	No Load Losses
$P_{LL}$	-	Load Losses
$P_T$	-	Total Power Losses
$P_{LL} (pu)$	-	Per Unit Value of Load Losses
$P_{LL}^{rated} (pu)$	-	Rated Per Unit Value of Load Losses
$P_{LL}^{rated}$	-	Rated Load Losses
$P_{I^2 R}^{rated}$	-	Rated Ohmic Losses
$P_{tosl}^{rated}$	-	Rated Total Other Stray Losses
$P_{osl}^{rated}$	-	Rated Other Stray Losses
$P_{ec}^{rated}$	-	Rated Eddy Current Losses
$P_{I_2}$	-	Power Loss at Secondary Side of Transformer
$K$	-	Constant gain
$I_1$	-	Current at Primary Side of Transformer
$I_2$	-	Current at Secondary Side of Transformer
$R_1$	-	Resistance at Primary Side of Transformer
$R_2$	-	Resistance at Secondary Side of Transformer
$h$	-	Harmonic order
$I_h$	-	Harmonic Current
$\mu_r$	-	Relative permeability
$\sigma$	-	Electrical conductivity
$C_p$	-	Heat capacity at constant pressure
$\varepsilon$	-	Relative permittivity
$\rho$	-	Density
$k$	-	Thermal conductivity
$\gamma$	-	Ratio of specific heat

$b.c$	-	Boundary Condition
$n$	-	Boundaries Vector
$q$	-	Conductive Heat Flux
$q_0$	-	Convection Heat Flux
$T$	-	Temperature
$T_0$	-	Initial Temperature
$Q$	-	Heat Source
$Q_{ted}$	-	Thermo Elastic Damping
$Q_e$	-	Electromagnetic Heat Source
$P_0$	-	Power Losses
$V$	-	Volume
$d_z$	-	Thickness of the Geometry
$u$	-	Thermal Heat Coefficient
$\theta_{HS-rated}$	-	Rated Hottest Spot Temperature
$\theta_{HS}$	-	Hottest-spot Winding Temperature
$\theta_a$	-	Ambient Temperature
$\Delta\theta_{HS,r}$	-	Rated Hottest-Spot Temperature Rise Over Ambient
$\Delta\theta_{HS}$	-	Hottest-Spot Temperature Rise Over Ambient
$\theta_{HS-130}$	-	HST at 130 insulation temperature class
$\theta_{HS-150}$	-	HST at 150 insulation temperature class
$\theta_{HS-180}$	-	HST at 180 insulation temperature class
$\theta_{HS-200}$	-	HST at 200 insulation temperature class
$\theta_{HS-220}$	-	HST at 220 insulation temperature class
$\theta_{HSpre-130}$	-	HST of premature failure at 130 insulation temperature class
$\theta_{HSpre-150}$	-	HST of premature failure at 150 insulation temperature class
$\theta_{HSpre-180}$	-	HST of premature failure at 180 insulation temperature class
$\theta_{HSpre-200}$	-	HST of premature failure at 200 insulation temperature class
$\theta_{HSpre-220}$	-	HST of premature failure at 220 insulation temperature class
$L$	-	Per Unit Load
$m$	-	Empirical Constant
$t_{Life}$	-	Expected Lifetime of Transformer
$exp$	-	Base of Natural Logarithms

## LIST OF APPENDICES

<b>APPENDIX</b>	<b>TITLE</b>	<b>PAGE</b>
Appendix A	Power losses at every THDI level	161
Appendix B1	HST results from FEM thermal distribution transformer model	166
Appendix B2	HST results from IEEE HST mathematical distribution transformer model	172
Appendix B3	Mathematical expression for HST premature failure assessment at LV winding	178
Appendix B4	HST results comparison from IEEE, FEM and derived polynomial function	181
Appendix C	Summary of premature failure of distribution transformer	185

# CHAPTER 1

## INTRODUCTION

### 1.1 Research background

Ever since the evolution of the power electronics technologies to replace the conventional alternating current (AC) electrical system, Malaysia as a developing country is not exceptional in utilizing those technologies to improve its system towards the country's development. Upon that matter, good quality of the electricity power is expected to be drawn along the distribution networks. Unfortunately, the ideal state of the power could not be ideally obtained due to the undesired power quality event such as the harmonics. Harmonics distortion is the most prominent power quality problem in electrical power distribution networks. International standard bodies such as the Institute of Electrical and Electronics Engineers, IEEE defined harmonics as the frequency components that are integer multiples of the fundamental line frequency.

The harmonics mainly originated from the nonlinear loads in the electrical distribution equipment which the frequency variations are mainly involved. The nonlinear load is defined as a load where the steady-state wave shape does not follow the wave shape of the applied voltage [1]. Other than the distorted power sinusoidal wave shape, the problems that might be happened due to the nonlinear harmonics loads include the elevation of the power losses and overheated the distribution transformer, poor power factor condition that causes users to pay the penalty fee, disturbance in the smoothness of massive production at industrial sites and many other bothersome issues within the network.

Based on the above problems, other crucial aspects are the electrical equipment's safety and lifetime. This hence mainly refers to the distribution transformer. In any electrical system network, a distribution transformer is a vital

component of the distribution system, which enable the utility provider to deliver power to its customers. It supplies voltage throughout the four wires cables to the electricity consumer, which usually requires high demand. Thus, making the distribution transformer the most expensive equipment in the electricity delivery system. Upon that matters, it is vital to ensure the durability and lifetime expectancy of the distribution transformer and its best performance to be preserved. In order to do this, it is best to explicit the possible root cause of any probability failure in the transformer at the earlier stage to avoid the massive loss due to the breakdown of the transformer. In [2], the author stated that the top ranking in the distribution transformer failure cases was caused by the transformer's excessive heat. The statement is strongly supported by the group of previous works that most agreed that the heat is the primary source of the failure in the distribution transformer [3–16]. Other than that, the authors also came to the mutual finding that most failures are happened at the low voltage side winding (LV) of the transformer compared to the core or other parts in the transformer. Elsewhere, the failure is said to frequently happen due to the degradation of the winding's insulation [17-28]. Nevertheless, the harmonics were not much being appointed or focused as the source of the excessive heat in that particular works.

Despite that, the impacts of the harmonics towards the distribution transformer are being highlighted in the numerous previous works, with most having emphasized the impact from the harmonic currents and having neglected the harmonic voltages due to its insignificance in the analysis [29-37]. The harmonic currents are said to be the root in the induction of the additional power losses and elevation in the average temperature rise and hotspot temperature of the transformer's LV winding. This is highly supported in [37], where the author had clarified that the harmonic currents had caused the 17% increment in the temperature rise at the LV winding and only caused the 3% increment at the HV winding. However, from the mentioned past works, another drawback is that less attention was paid to the actual condition of the unbalanced harmonics loads. Only a few authors opted to illustrate the impacts from the view of unbalanced harmonics loads condition [38-46]. Without illustrating the actual operation of the LV network, in which the current in each phase is expected to be imbalanced as the supply depends on the load needs, the accuracy of the results can

then be disputed. Thus, to get a precise outcome of any research problem, this unbalanced condition shall be considered and analysed thoroughly without exception.

Other than the actual harmonics loads condition, the behaviour of the harmonics loads also needs to be carefully observed, as it can indicate any possibility of premature failure at the transformer. Additionally, the behaviour shall cover the order of the harmonics ( $h_{th}$ ), the individual spectrum of the harmonics ( $I_h$ ) in which finally brought to the generation of the harmonics distortion level produced during the operation of the network, which is also known as total harmonic distortion (THD). On the topic to preserve the performance and the lifetime of the transformer, abundance methods are being proposed to observe and understand the behaviour of the harmonics loads in the transformer [47-59] and their contributions to the temperature rise and HST that may cause failure inside the transformer [60-67]. However, based on their results, the ambiguities were still there because not many authors came with the exact classification of the harmonic behaviour, especially on the THD that represents the several loads' distortion condition from the consumer. This is by means, the harmonic behaviour towards the power losses and hotspot temperature of the transformer should be determined and analysed according to the specific loads status and the actual operation timing of the loads which either the loads are generating low, intermediate or high harmonic distortion at that particular time. From this exact classification, the particular condition of the premature failure of the transformer shall be achieved.

The final part is the premature failure condition of the transformer due to the unbalanced harmonics loads. This is vital since prevention is indeed better than cure. It is highly recommended to protect the transformer at the earlier stage of any premature failure before the failure worsens until the unwanted massive breakdown becomes unavoidable. Since last 2011 up to the year 2020, many published research papers related upon endeavour in detecting and analysing the premature failure of the transformer. There are broad methods, including the model simulation covering numerical and analytical analysis [68-72], power quality collected data assessment [73-77], laboratory testing, and maintenance activities [78-81]. However, despite the advantages in each finding, there are still rooms for improvement that can be made in the analysis. First of all, only limited papers had put the influence of the harmonic

range or harmonic classification into the premature failure of the transformer. Secondly, none of the specific location on the winding was declared whenever they had traced any sign of the premature failure from their output results. This has made their methods impractical when there is a high necessity to trace the suspected problem from a specific view. This is important to avoid waste in cost and energy to replace the whole transformer unit with the new one. Secondly, there is a high necessity in choosing the most efficient technique to obtain the most accurate result. Based on studies, researchers have agreed that the Finite Element Method (FEM) from the numerical analysis is the most accurate, efficient, reliable and relevant up to recently to solve any simple and even complex problem in any condition compared to other methods [82-85]. Aside from the previously mentioned papers, this can also be seen in numerous published papers that are prominently related to the solution of the problems in transformer [86-91]. Last but not least is lacking in using the international standard as the reference for the premature failure condition. This is by means, other than using the formulation guide in the standard, the limit stated in the standard also can be beneficial as a benchmark of any evaluation analysis work.

Hence, it comes to the consideration in this research to utilize the FEM and combine it with the selected international standard limit as the reference of the premature failure condition of the transformer. The designed thermal transformer model using FEM is expected to generate the value of hotspot temperature (HST) in the LV winding of the three-phase transformer under unbalanced harmonics conditions throughout the simulation. Then the HST value is compared to the standard limit to check the compliance of the HST towards the limit. As for the limit compliance reference, the best reference to be referred to in harmonics behaviour towards heating the transformer is the guide solution from the well-established and trustworthy IEEE standard. For every type of temperature, the related standard such as IEEE Std. C57.134-2013 [92] and IEEE Std. C57.96-2013 [93] have already provided the guidelines and set the limit to be the reference for any study related to the distribution transformer's temperature. In the actual practice of the distribution transformer, if any temperature value exceeds the limit, the transformer is said to be in a risky state and need to be alert for any failure or tripped. This fact can hence be beneficial in clarifying the premature failure condition of the distribution transformer due to the harmonics.

In order to validate the results proposed in this thesis, the HST results from both thermal distribution transformer modelling using FEM [94] and HST mathematical modelling using IEEE Std C57.110-2018 standard [95] are compared. The modelling using the IEEE standard can be done because, in the mentioned standard, the committee had established the hotspot temperature (HST) calculation concerning the non-sinusoidal load currents for both liquid immersed-type and dry-type of power and distribution transformer.

Thus the main focus of this research is to propose an early detection of premature failure expression at the distribution transformer by improving the analysis of power losses concerning the unbalanced harmonic loads towards the hot spot temperature of the transformer. Hence, the percentage of the harmonic current loads that contribute to the final hot spot temperature is classified and presented. Also, for any hotspot temperature that has exceeded the standard limit, the percentage of that particular unbalanced harmonic current loads towards the hotspot is expressed as an indication of the early detection of premature distribution transformer failure.

## **1.2 Problem statement**

Generally, the harmonic current loads gradually impact the ideal performance of the distribution transformer when they increase the power losses and HST, which lead to the possible failure inside the winding of the distribution transformer. Hence, some of the related problems to be solved in this thesis are listed as follows:

- i. The excessive unbalanced harmonic loads currents elevate the total power losses and increase the hotspot temperature in the LV winding. This can cause damage and breakdown of the distribution transformer if no preventive measure has been taken at the earlier stage [37]. In the network operation between commercial loads and voltage supply, lack of attention had been given to the relationship between the unbalanced harmonics loads to the power losses and hotspot temperature of the

transformer to observe any premature failure that could be occurred in the transformer [43].

- ii. The harmonics current distortion (THDI) is often treated as the distortion percentage, which is calculated from one whole day instead of particularly measured at a specific real-time within the day in observing its impact towards the distribution transformer's LV winding. When considering the power losses and hotspot temperature of the winding in the distribution transformer, no harmonic current distortion from specific hours is highlighted in the previous in order to explicitly recognize its behaviour towards the premature failure of the winding [63]. Additionally, most of the previous works cited in this research focused on the higher value of THDI instead of paying attention to the lower value to analyse its impact on the distribution transformer [64-66]. Hence, this brought to the hypothesis that the failure's causes upon the harmonic distortion can only be known once the distribution transformers are either already damaged or its expectancy lifetime had dramatically dropped, as the premature failure in the distribution transformer could not be traced at an earlier stage.
- iii. The existing methods to detect the premature failure of distribution transformers remain ambiguous in the findings. This upon lacking in utilizing the mathematical function to vividly express the final findings for a better understanding of the proposed solution [70], [73], [75], [77]. Plus, when dealing with failure in the distribution transformer, it is also important to perform the real lifetime of the transformer in order to observe the impact of the failure on the lifetime expectancy of the transformer. Thus, with the comprehensive expression of the findings, the analysis of the real lifetime estimation of the transformer shall be improved.

### **1.3 Research objectives**

Based on the previously mentioned problems in Section 1.2, here are the listed three main objectives to be implemented for this research to reflect those arisen problems accordingly.

- i. To propose an improved analysis in power losses of distribution transformer to detect the premature failure of the transformer by considering the relationship between unbalanced harmonic current from the loads towards power losses and HST of the transformer.
- ii. To enhance the examination of the HST behaviour on the LV windings by employing the power losses under different THDI levels onto the FEM thermal distribution transformer model to identify the premature failure condition of the LV windings under such particular circumstances.
- iii. To develop a new HST mathematical expression for premature failure condition assessment based on HST upon per unit loadings, which to be assessed on the LV windings and evaluate the real lifetime estimation of the distribution transformer.

### **1.4 Research scopes**

In accountability to implement the abovementioned objectives in Section 1.3, the following scopes are hence shall be covered in this research.

- i. All harmonic data are measured and collected for one week with 10 minutes intervals using a power quality data logger at the substations interconnected to commercial buildings.

- ii. The measured and collected harmonic data for this research mainly comes from the detected problematic transformer at a substation that supply electricity to commercial load building.
- iii. The harmonic data for this research is extracted and assembled according to three different hours within the load operation of the selected day. The three different hours are named as the peak hour, average hour and low hour.
- iv. The harmonic current orders that being considered for this research are the odd harmonics orders, which start from 1<sup>st</sup> until 19<sup>th</sup> ( $I_1$  until  $I_{19}$ ).
- v. The THDI value being analysed for the research finding ranges between 12% to 22%.
- vi. The computation of the HST value is intended on the specified LV winding of the distribution transformer model.
- vii. The applications of Power analyse software, COMSOL Finite Element Method software, MATLAB software and Microsoft Excel are used to simulate the power flow harmonics analysis throughout the model of the distribution transformer.
- viii. FEM thermal distribution transformer model in COMSOL is developed to classify the condition of the hotspot temperature of the LV winding due to the unbalanced harmonic current loads.
- ix. The premature failure condition of the distribution transformer is determined by referring to the maximum hottest spot temperature loading above rating standard limits in [93].

- x. The results are validated by comparing with the HST obtained from the IEEE HST mathematical model, which is modelled using the guidelines from [95].

## **1.5 Research contributions**

Prior to the statements and explanations from the previous sections above, here come the lists of contributions that shall be gained throughout the findings in this research.

- i. The final finding in this research summarized the HST condition of the LV winding by considering the possibility of different levels of the THDI that might occur in the network.
- ii. The proposed method had considered the unbalanced current loads due to the harmonic to be the adding value for this research. The finding in this research is hence convincible to be the reference to the early detection of a premature failure of the distribution transformer. Additionally, the generated premature failure expression allows to observe and analyse the insulation deterioration condition of the LV winding from each phase to decide the suitable counter measure regarding the condition. This hence will ease the diagnostic action on the transformer and replace the tedious, laborious and yet costly repair and maintenance for the whole one unit of the transformer.
- iii. The analysis in this research covered the whole types of insulation temperature classes that might be used in designing a distribution transformer for the low voltage network.
- iv. The lifetime analysis of the transformer under nonlinear loads is improved by the implementation of the proposed method from this thesis. Not limited only to observing the impact of the THDI on the

lifetime, the proposed method provides a coherent view of the real condition inside the transformer that contributes to the impact.

- v. The application of FEM as the acknowledged efficient numerical method and the regulation of the aforementioned standards has improved the reliability, robustness, result accuracy, practicality, and cost effective, which benefitted to achieve the objectives from this research.

## **1.6 Thesis outlines**

This thesis is organized into five chapters. The introduction in Chapter 1 is comprised of research background, problem statements, research objectives, research scopes, research contributions and thesis outline. The literature review in Chapter 2 reviews previous related research works dominantly on harmonics and its impact on the transformer. Several selected publications are presented rigorously to expose the effectiveness and research gaps that are beneficial in the development of the proposed premature failure determination in distribution transformers. Chapter 3 explains the entire sequences in this research, including the harmonics data measurement and assembly from the site, designation and simulation of the distribution transformer, derivation of the premature failure function, and estimation of the real distribution transformer's lifetime. The designed distribution transformer model, which is verified based on remodelling the similar research problem using guidelines from the selected international standards, are also presented in this chapter. The results and discussion in Chapter 4 report the data collection, simulation results, discussions and validations of the HST behaviour under the unbalanced harmonic influence, the proposed HST at premature failure condition of the transformer and affected expectancy lifetime of the transformer. Ultimately, the conclusion in Chapter 5 summarizes the entire works in this thesis and proposes several recommendations that can be implemented in the future.

## REFERENCES

- [1] D. Committee, I. Power, and E. Society, “IEEE Std 519-2014, IEEE Recommended Practice and Requirements for Harmonic Control in Electric Power Systems,” *IEEE Std 519-2014 (Revision IEEE Std 519-1992)*, vol. 2014, pp. 1–29, 2014.
- [2] R. Singh and A. Singh, “Causes of failure of distribution transformers in India,” in *2010 9th Conference on Environment and Electrical Engineering, IEEEIC 2010*, 2010, pp. 388–391, doi: 10.1109/IEEEIC.2010.5489987.
- [3] J. Li, T. Jiang, and S. Grzybowski, “Hot spot Temperature Models Based on Top-oil Temperature for Oil Immersed Transformers,” *2009 IEEE Conf. Electr. Insul. Dielectr. Phenom.*, pp. 55–58, 2009, doi: 10.1109/CEIDP.2009.5377876.
- [4] A. Skillen, A. Revell, H. Iacovides, and W. Wu, “Numerical prediction of local hot-spot phenomena in transformer windings,” *Appl. Therm. Eng.*, vol. 36, pp. 96–105, 2012, doi: 10.1016/j.applthermaleng.2011.11.054.
- [5] M. T. Villén, J. Letosa, A. Nogués, and R. Murillo, “Procedure to accelerate calculations of additional losses in transformer foil windings,” *Electr. Power Syst. Res.*, vol. 95, pp. 85–89, 2013, doi: 10.1016/j.epsr.2012.08.006.
- [6] W. Sun, L. Yang, D. Feng, X. Zhao, and J. Li, “A New Accelerated Thermal Aging Test for Over-Loading Condition Transformer,” no. June, pp. 19–22, 2016.
- [7] N. Technology, “Distribution Transformer Failure Rate Prediction Model Based on Multi-Source Information,” no. 1, pp. 944–947, 2016.
- [8] D. Transformers and U. T. S. Ide, “Distribution Transformer Failure in India Root Causes and Remedies existing as at the,” no. Icimia, pp. 106–110, 2017.
- [9] I. M. Sari, A. Tryollinna, A. Dwita, P. Sudin, and D. D. Permata, “Through fault current effects on distribution transformer and prevention actions using backup protection : Case study of Kelapa Gading transformer,” pp. 247–251, 2017.

- [10] G. Liang and S. Li, "A Probabilistic Maintenance Scheme Evaluation Method for Transformer based on Failure Rate," pp. 90–93, 2017, doi: 10.1109/ICISCE.2017.29.
- [11] S. Solanki, R. Jangid, G. Srivastava, P. Sharma, and R. Chaturvedi, "International Journal of Trend in Scientific Research and Development ( IJTSRD ) Hot Spot Temperature Analysis of Transformer using FEM on COMSOL," pp. 1289–1295, 2018.
- [12] C. AJ, M. A. Salam, Q. M. Rahman, F. Wen, S. P. Ang, and W. Voon, "Causes of transformer failures and diagnostic methods – A review," *Renew. Sustain. Energy Rev.*, vol. 82, no. July, pp. 1442–1456, 2018, doi: 10.1016/j.rser.2017.05.165.
- [13] M. Ali, "Transient Analysis of a Distribution Transformer using ATP-EMTP," no. 1, 2018.
- [14] K. Hong and G. Lin, "State classification of transformers using nonlinear dynamic analysis and Hidden Markov models," *Measurement*, vol. 147, p. 106851, 2019, doi: 10.1016/j.measurement.2019.106851.
- [15] A. Tariku, "Distribution Transformer Failure Study and Solution Proposal in Ethiopia," pp. 1–5, 2020.
- [16] D. P. Rommel, D. Di Maio, and T. Tinga, "Electrical Power and Energy Systems Transformer hot spot temperature prediction based on basic operator information," *Electr. Power Energy Syst.*, vol. 124, no. June 2020, p. 106340, 2021, doi: 10.1016/j.ijepes.2020.106340.
- [17] S. A. Deokar and L. M. Waghmare, "Impact of power system harmonics on insulation failure of distribution transformer and its remedial measures
- [18] D. Cai, J. Tang, and J. Li, "The evaluation of thermal endurance of cast-resin dry-type transformer insulation structure," *China Int. Conf. Electr. Distrib. CICED*, no. Ciced, pp. 5–6, 2012, doi: 10.1109/CICED.2012.6508446.
- [19] G. P. Lopes, F. Napolitano, C. A. Nucci, and A. Borghetti, "22 nd International Conference on Electricity Distribution Paper 1484 "A Procedure to Evaluate the Risk of Failure of Distribution Transformers Insulation due to Lightning Induced Voltages" 22 nd International Conference on Electricity Distribution," no. June, pp. 10–13, 2013.

- [20] S. D. Flora, M. K. Kumari, and J. S. Rajan, "A new approach to study the effects of copper sulphide on electric stress distribution in paper oil insulation of transformers," no. June, pp. 198–202, 2014.
- [21] F. Tao, J. Li, C. Wei, and A. E. Samples, "Thermal Ageing Effect on the Failure Time of Oil- Paper Insulation at Combined AC-DC Voltage," no. June, pp. 19–22, 2016.
- [22] A. K. S, "Determination of Electrical Breakdown Strength of Insulating Presspapers Used for Power and Distribution Transformers," pp. 2566–2570, 2018.
- [23] A. A. Burym, P. V Rysev, D. V Rysev, and V. S. Serdyuk, "Failure Testing of Single-Phase Voltage Transformers of Distribution Networks Due to Discharge Phenomena in Insulation," no. November, pp. 13–15, 2018.
- [24] T. Bavisha, K. Aniruthaan, and S. Usa, "Withstand capability of transformers under very fast transients," in *2017 3rd International Conference on Condition Assessment Techniques in Electrical Systems, CATCON 2017 - Proceedings*, 2018, vol. 2018-Janua, pp. 320–325, doi: 10.1109/CATCON.2017.8280237.
- [25] A. A. Burym, P. V. Rysev, D. V. Rysev, V. S. Serdyuk, and E. A. Sidorova, "Failure Testing of Single-Phase Voltage Transformers of Distribution Networks Due to Discharge Phenomena in Insulation," *12th Int. Sci. Tech. Conf. "Dynamics Syst. Mech. Mach. Dyn. 2018*, no. November, pp. 13–15, 2019, doi: 10.1109/Dynamics.2018.8601469.
- [26] C. Boonseng, "Electrical Insulation Testing and DGA Analysis for the Diagnosis of Insulation Faults and Failures in 24 MVA Transformers for Distribution Systems," no. Cmd, pp. 70–73, 2020.
- [27] R. Soni, P. Chakrabarti, Z. Leonowicz, M. Jasiński, K. Wieczorek, and V. Bolshev, "Estimation of life cycle of distribution transformer in context to furan content formation, pollution index, and dielectric strength," *IEEE Access*, vol. 9, pp. 37456–37465, 2021, doi: 10.1109/ACCESS.2021.306355
- [28] D. Azizian, "Temperature Prediction in Cast-Resin Transformer Due to Non-Linear Loads," *J. Electr. Syst.*, vol. 3, pp. 238–249, 2014.
- [29] I. Iskender and A. Najafi, "Evaluation of Transformer Performance Under Harmonic Load Based on 3-D Time Stepping Finite Element Method," *2014 16th Int. Conf. Harmon. Qual. Power*, pp. 224–228, 2014, doi: 10.1109/ICHQP.2014.6842827.

- [30] G. C. Jaiswal, M. S. Ballal, and D. R. Tutakne, "Impact of power quality on the performance of distribution transformer," *IEEE Int. Conf. Power Electron. Drives Energy Syst. PEDES 2016*, vol. 2016-Janua, pp. 1–5, 2017, doi: 10.1109/PEDES.2016.7914344.
- [31] H. F. M. Mantilla, A. Pavas, and I. C. Durán, "Aging of distribution transformers due to voltage harmonics," *2017 3rd IEEE Work. Power Electron. Power Qual. Appl. PEPQA 2017 - Proc.*, pp. 1–5, 2017, doi: 10.1109/PEPQA.2017.7981649.
- [32] E. Cazacu, M. C. Petrescu, V. Ionita, and L. Petrescu, "Nonsinusoidal load current effect on the electrical and thermal operating parameters of oil-filled power distribution transformers," *Proc. Int. Conf. Harmon. Qual. Power, ICHQP*, vol. 2018-May, pp. 1–6, 2018, doi: 10.1109/ICHQP.2018.8378838.
- [33] L. Jiang and J. Meng, "Research on additional loss of line and transformer in low voltage distribution network under the disturbance of power quality," pp. 364–369, 2018.
- [34] D. Wan, F. Qi, M. Zhao, L. Mao, X. Duan, and Y. Liu, "An Improved Method for Calculating Power Transmission Equipment Loss and Hot Spot Temperature in Distribution Network under Harmonic Disturbance," *2019 3rd*
- [35] D. Wan, M. Zhao, X. Duan, H. Zhou, L. Mao, and K. You, "Life Assessment Study on Distribution Electric Power Transmission Equipment Based on Harmonic Modified Hot Spot Temperature Calculating Model," *2019 3rd IEEE Conf. Energy Internet Energy Syst. Integr. Ubiquitous Energy Netw. Connect. Everything, EI2 2019*, pp. 138–141, 2019, doi: 10.1109/EI247390.2019.9061954.
- [36] D. Wan, L. Zhang, M. Zhao, H. Zhou, S. Peng, and T. Peng, "Calculation Method of Hot Spot Temperature of Distribution Power Transmission Equipment Insulation Winding Based on Eddy Current Loss Density Distribution," *2019 3rd IEEE Conf. Energy Internet Energy Syst. Integr. Ubiquitous Energy Netw. Connect. Everything, EI2 2019*, pp. 2750–2753, 2019, doi: 10.1109/EI247390.2019.9062046.
- [37] M. V Athul, G. S. Member, P. K. Preetha, and P. S. C. Nair, "Analysis of Star-Star-Delta \_ Utilized Transformer under Balanced and Unbalanced Load Conditions," pp. 1–6, 2015.

- [38] J. Yong and W. Xu, "A Method to Estimate the Impact of Harmonic and Unbalanced Currents on the Ampacity of Concentric Neutral Cables," vol. 31, no. 5, pp. 1971–1979, 2016.
- [39] J. B. Noshahr, "The Estimation of the Influence of Each Harmonic Component in Load Unbalance of Distribution Transformers in Harmonic Loading Condition," 2019.
- [40] P. S. Moses, S. Member, M. A. S. Masoum, and S. Member, "Three-Phase Asymmetric Transformer Aging Considering Voltage-Current Harmonic Interactions , Unbalanced Nonlinear Loading , Magnetic Couplings , and Hysteresis," vol. 27, no. 2, pp. 318–327, 2012.
- [41] C. Lixia and T. Unbalance, "A Study on the Harmonic Contributions of DGs Connected to Unbalanced Power Systems," vol. 1, no. 2, p. 6, 2017.
- [42] B. Ali, A. A. Khan, and I. Siddique, "Analysis of distribution system losses due to harmonics in IESCO," pp. 1–6, 2018.
- [43] K. M. Banjar-nahor and F. Cadoux, "System Modeling and Its Effect on State Estimation in Unbalanced Low Voltage Networks in the Presence of Measurement Errors," pp. 119–124, 2019.
- [44] M. Zhao, D. Wan, H. Zhou, J. Fang, S. Peng, and W. Zhou, "Study on the Influence of Load Imbalance on Current Carrying Capacity of Power Transmission Equipment in Distribution Network," no. 1, pp. 2882–2885, 2019.
- [45] A. Chidurala, T. K. Saha, and N. Mithulananthan, "Harmonic impact of high penetration photovoltaic system on unbalanced distribution networks – learning from an urban photovoltaic network," pp. 485–494, 2015, doi: 10.1049/iet-rpg.2015.0188.
- [46] P. S. Moses, M. A. S. Masoum, and K. M. Smedley, "Harmonic losses and stresses of nonlinear three-phase distribution transformers serving plug-in electric vehicle charging stations," *IEEE PES Innov. Smart Grid Technol. Conf. Eur. ISGT Eur.*, pp. 1–6, 2011, doi: 10.1109/ISGT.2011.5759145.
- [47] T. Dao, B. T. Phung, and T. Blackburn, "Effects of voltage harmonics on distribution transformer losses," *Asia-Pacific Power Energy Eng. Conf. APPEEC*, vol. 2016-Janua, no. September, pp. 633–636, 2012, doi: 10.1109/APPEEC.2015.7380953.

- [48] C. Pan, L. Kong, L. Zhenxin, Q. Zheng, and Z. Wang, "Energy Procedia Analysis Based on Improved Method for Transformer Harmonic Losses," vol. 16, pp. 1845–1851, 2012, doi: 10.1016/j.egypro.2012.01.283.
- [49] S. Taheri, A. Gholami, I. Fofana, and H. Taheri, "Modeling and simulation of transformer loading capability and hot spot temperature under harmonic conditions," *Electr. Power Syst. Res.*, vol. 86, pp. 68–75, 2012, doi: 10.1016/j.epsr.2011.12.005.
- [50] H. I. Zynal and A. A. Yass, "The Effect of Harmonic Distortion on a Three phase Transformer Losses," vol. 3, no. 5, 2012.
- [51] Z. Zainal, S. P. Ang, M. A. Salam, P. J. Weira, and R. Goh, "Impacts of nonlinear loads on a 11 kV distribution network," *Asia-Pacific Power Energy Eng. Conf. APPEEC*, vol. 2015-March, no. March, 2014, doi: 10.1109/APPEEC.2014.7066179.
- [52] C. Ndungu, J. Nderu, L. Ngoo, and P. Hinga, "A Study of the Root Causes of High Failure Rate of Distribution Transformer - A Case Study," *Int. J. Eng. Sci.*, vol. 6, no. 2, pp. 14–18, 2017, doi: 10.9790/1813-0602021418.
- [53] D. Alame, M. Azzouz, and N. C. Kar, "Impact assessment of electric vehicle charging on distribution transformers including state-of-charge," *Midwest Symp. Circuits Syst.*, vol. 2018-Augus, no. 2, pp. 607–610, 2019, doi: 10.1109/MWSCAS.2018.8623966.
- [54] H. Wang, W. Zhou, K. Qian, and S. Meng, "Electrical Power and Energy Systems Modelling of ampacity and temperature of MV cables in presence of harmonic currents due to EVs charging in electrical distribution networks," *Electr. Power Energy Syst.*, vol. 112, no. April, pp. 127–136, 2019, doi: 10.1016/j.ijepes.2019.04.027.
- [55] J. E. C. González, A. M. García, A. del Castillo Serpa, M. del Cisne Carrión González, R. P. M. Vivanco, and K. A. A. Carrión, "Procedure to evaluate the impact in distribution single phase transformers due to insertion of new nonlinear load which changes daily demand graphs," *Energies*, vol. 12, no. 20, 2019, doi: 10.3390/en12203923.
- [56] R. Lamedica, A. Ruvio, P. Fernando, and M. Regoli, "Simulation Modelling Practice and Theory A Simulink model to assess harmonic distortion in MV / LV distribution networks with time-varying non linear loads," *Simul. Model.*

- Pract. Theory*, vol. 90, no. July 2018, pp. 64–80, 2019, doi: 10.1016/j.simpat.2018.10.012.
- [57] J. Yaghoobi, A. Alduraibi, D. Martin, F. Zare, and D. Eghbal, “Electrical Power and Energy Systems Impact of high-frequency harmonics ( 0 – 9 kHz ) generated by grid-connected inverters on distribution transformers ☆,” *Electr. Power Energy Syst.*, vol. 122, no. October 2019, p. 106177, 2020, doi: 10.1016/j.ijepes.2020.106177.
- [58] G. Singh, C. Miller, and W. Howe, “A Framework for Evaluating Harmonic Losses in Distribution Planning,” 2020.
- [59] E. Cazacu, L. Petrescu, and V. Ionita, “Derating of Power Distribution Transformers Serving Nonlinear Industrial Loads,” pp. 90–95, 2017.
- [60] S. A. Deokar and L. M. Waghmare, “Impact of power system harmonics on insulation failure of distribution transformer and its remedial measures,” *ICECT 2011 - 2011 3rd Int. Conf. Electron. Comput. Technol.*, vol. 3, pp. 136–140, 2011, doi: 10.1109/ICECTECH.2011.5941817.
- [61] B. P. Das and Z. Radakovic, “Is transformer kVA derating always required under harmonics? A manufacturer’s perspective,” *IEEE Trans. Power Deliv.*, vol. 33, no. 6, pp. 2693–2699, 2018, doi: 10.1109/TPWRD.2018.2815901.
- [62] S. Bahramara and F. G. Mohammadi, “Optimal sizing of distribution network transformers considering power quality problems of non-linear loads,” vol. 2017, no. June, pp. 2471–2475, 2017, doi: 10.1049/oap-cired.2017.0258.
- [63] A. S. J. Singh, S. Singh, “Impact of Harmonics on Power Transformer Losses and Capacity Using Open DSS,” pp. 1–11, 2019, doi: 10.1515/ijeeps-2018-0349.
- [64] B. Verhelst, J. Rens, and J. Desmet, “Derating method for dry type power transformers based on current distortion parameters,” no. June, pp. 3–6, 2019.
- [65] Y. Wang, Z. Wang, and S. Fang, “Three-Dimensional Magnetic and Temperature Field Coupling Analysis of Dry-Type Transformer Core under Different Excitations,” vol. 95, no. August, pp. 75–89, 2019.
- [66] S. Balci, “Thermal Behavior of a Three Phase Isolation Transformer Under Load Conditions with the Finite Element Analysis,” vol. 24, no. 3, pp. 2189–2201, 2020.

- [67] M. Mikhak-beyranvand, J. Faiz, and B. Rezaeealam, "Thermal analysis and derating of a power transformer with harmonic loads," vol. 14, pp. 1233–1241, 2020, doi: 10.1049/iet-gtd.2019.0703.
- [68] M. Yazdani-Asrami, M. Mirzaie, A. Shayegani Akmal, and S. Asghar Gholamian, "Life estimation of distribution transformers under non-linear loads using calculated loss by 2D-FEM," *Journal of Electrical Systems*, vol. 7, no. 1, pp. 12–24, 2011.
- [69] M. Digalovski, K. Najdenkoski, and G. Rafajlovski, "Impact of current high order harmonic to core losses of three-phase distribution transformer," no. July, pp. 1531–1535, 2013.
- [70] J. Faiz, M. Ghazizadeh, and H. Oraee, "Derating of transformers under non-linear load current and non-sinusoidal voltage – an overview," vol. 9, no. 1, pp. 486–495, 2015, doi: 10.1049/iet-epa.2014.0377.
- [71] P. S. Moses, S. Member, M. A. S. Masoum, S. Member, and K. M. Smedley, "Harmonic Losses and Stresses of Nonlinear Three-Phase Distribution Transformers Serving Plug-In Electric Vehicle Charging Stations," pp. 11–16, 2011.
- [72] A. Abbas, E. Abou, E. L. Zahab, and A. Elbendary, "Thermal Modeling and Ageing of Transformer Under Harmonic Currents," no. June, pp. 15–18, 2015.
- [73] M. N. D. Dang, N. Al-mutawaly, and J. Lepoutre, "From Transmission to Distribution Networks - Harmonic Impacts on Modern Grid," pp. 452–459, 2015.
- [74] C. Lombard and A. P. J. Rens, "Evaluation of system losses due to harmonics in medium voltage distribution networks," *2016 IEEE Int. Energy Conf. ENERGYCON 2016*, 2016, doi: 10.1109/ENERGYCON.2016.7513919.
- [75] P. K. Bl, S. Member, R. Mathew, and S. Member, "Asset management of transformer based on loss of life calculation," 2016.
- [76] J. Singh, "Effect of Harmonics on Distribution Transformer Losses and Capacity," vol. 4, no. 6, pp. 48–55, 2017.
- [77] E. Cazacu, V. Ionita, and L. Petrescu, "Thermal Aging of Power Distribution Transformers Operating under Nonlinear and Balanced Load Conditions Transformer Aging Due to," pp. 92–100, 2018, doi: 10.15598/aece.v16i1.2701.

- [78] M. I. Ridwan, M. R. Samsudin, and Y. Z. Yang Ghazali, "Reliability analysis of premature failed 11/0.433kV hermetically sealed distribution transformers," *2011 IEEE Colloq. Humanit. Sci. Eng. CHUSER 2011*, no. Chuser 2011, pp. 321–326, 2011, doi: 10.1109/CHUSER.2011.6163742.
- [79] J. Zhu, T. Chen, Q. Fu, and S. Cheng, "Detection of early failures within traction transformers based on Gaussian-PSO," *2015 3rd Int. Conf. Electr. Power Equip. - Switch. Technol. ICEPE-ST 2015*, pp. 488–491, 2015, doi: 10.1109/ICEPE-ST.2015.7368323.
- [80] T. Dewangan and P. Patel, "Prediction of Distribution Transformer Premature Failures," *Int. J. Res. Appl. Sci. Eng. Technol.*, vol. 5, no. V, pp. 1450–1455, 2017.
- [81] T. Dewangan and P. Patel, "Prevention of Distribution Transformer Premature Failures," vol. 6, no. 3, pp. 305–308, 2017.
- [82] M. Amrhein and P. T. Krein, "Induction machine modeling approach based on 3-D magnetic equivalent circuit framework," *IEEE Trans. Energy Convers.*, vol. 25, no. 2, pp. 339–347, 2010, doi: 10.1109/TEC.2010.2046998.
- [83] A. S. Mohammadi and J. P. Trovao, "A Comparison of Different Models for Permanent Magnet Synchronous Machines: Finite Element Analysis, D-Q Lumped Parameter Modeling, and Magnetic Equivalent Circuit," *IEEE Int. Symp. Ind. Electron.*, vol. 2019-June, pp. 197–202, 2019, doi: 10.1109/ISIE.2019.8781540.
- [84] S. Piltyay, A. Bulashenko, Y. Herhil, and O. Bulashenko, "FDTD and FEM simulation of microwave waveguide polarizers," *ATIT 2020 - Proc. 2020 2nd IEEE Int. Conf. Adv. Trends Inf. Theory*, pp. 357–363, 2020, doi: 10.1109/ATIT50783.2020.9349339.
- [85] B. Kidd, "Scaled Magnetic Circuit Equations," vol. 56, no. 10, 2020.
- [86] R. Escarela-perez, J. C. Olivares-galvan, and V. M. Jimenez-mondragon, "Finite Element Analysis of Distribution Transformer under Harmonics Condition : A Review," no. Ropec, 2017.
- [87] J. Wijaya, T. Czaszejko, N. Lelekakis, D. Martin, and D. Susa, "A finite element model for the analysis of steady state heat transfer in disc coil transformer winding," *2012 22nd Australas. Univ. Power Eng. Conf. "Green Smart Grid Syst. AUPEC 2012*, 2012.

- [88] V. Behjat, "A Coupled Thermal-Electromagnetic FEM Model to Characterize the Thermal Behavior of Power Transformers Damaged By Short Circuit Faults," *Int. J. Electr. Energy*, vol. 1, no. 4, pp. 194–200, 2013, doi: 10.12720/ijoe.1.4.194-200.
- [89] N. A. M. Yusoff, K. A. Karim, S. A. Ghani, T. Sutikno, and A. Jidin, "Multiphase transformer modelling using finite element method," *Int. J. Power Electron. Drive Syst.*, vol. 6, no. 1, pp. 56–64, 2015, doi: 10.11591/ijpeds.v6.i1.pp56-64.
- [90] İ. H. Teke, Y. Özüpak, M. S. Mamiş, E. E. B. Thermal, and P. Plant, "Electromagnetic Field and Total Loss Analysis of Transformers by Finite Element Method," *Int. J. Eng. Comput. Sci.*, vol. 8, no. 1, pp. 24451–24460, 2018, doi: 10.18535/ijecs/v8i1.01.
- [91] J. M. Yadav, "Prediction of Hotspot Location in a Power Transformer Considering Stray Losses using FEM," vol. 13, no. 1, pp. 238–244, 2018.
- [92] Transformers Committee, "IEEE Guide for Determination of Hottest-Spot Temperature in Dry-Type Transformers Sponsored by the Transformers Committee IEEE Power and Energy Society," vol. 2013, 2013.
- [93] S. Committee of the IEEE Power and E. Society, "IEEE Guide for Loading Dry-Type Distribution and Power Transformers IEEE," vol. 2013. 2013.
- [94] M. COMSOL, "Heat Transfer Module," Manual, pp. 1–222, 2015.
- [95] T. Committee, I. Power, and E. Society, "IEEE Recommended Practice for Establishing Liquid-Filled and Dry-Type Power and Distribution Transformer Capability When Supplying Nonsinusoidal Load Currents," vol. 2008, no. August. 2018.
- [96] T. Committee, "IEEE Recommended Practice for Establishing Transformer Capability When Supplying Nonsinusoidal Load Currents," vol. 1998. 1998.
- [97] P. S. I. and M. Committee, "IEEE Standard Definitions for the Measurement of Electric Power Quantities Under Sinusoidal, Nonsinusoidal, Balanced, or Unbalanced Conditions." New York, NY 10016-5997, USA: IEEE Power & Energy Society, 2010.
- [98] I. Power and E. Society, "IEEE Guide for Loading Mineral- Oil-Immersed Transformers and Step-Voltage Regulators," vol. 2011, no. March. 2012.

- [99] T. T. C. on P. Quality, "Electromagnetic Compatibility (EMC) - Limits - Limitation of Emission of Harmonic Currents in Low-Voltage Power Supply Systems for Equipment with Rated Current Greater than 16A." 2002.
- [100] M. Yazdani-Asrami, M. Mirzaie, and A. A. S. Akmal, "Investigation on impact of current harmonic contents on the distribution transformer losses and remaining life," *PECon2010 - 2010 IEEE Int. Conf. Power Energy*, pp. 689–694, 2010, doi: 10.1109/PECON.2010.5697668.
- [101] F. Corporation, "Fluke 1750 Three-Phase Power Quality Logger," *Fluke Corporation*, 2021. [Online]. Available: <https://www.fluke.com/en-my/product/electrical-testing/power-quality/1750>.
- [102] U. S. B. Firewire and P. C. I. Card, "1750 Power Recorder Operators Manual," *ReVision*, vol. 49, no. 3, pp. 1–52, 2003.

## LIST OF PUBLICATIONS

### Journal

1. Z.I.M.Yassin, D.M.Said, N.Ahmad, NN Nik Abd Malik, H.Abdullah. “Impact Of Unbalanced Harmonic Loads Towards Winding Temperature Rise Using Fem Modeling.” Indonesian Journal Of Electrical Engineering And Informatics. Vol.8, No.2, June 2020, pp. 409-418. (**Indexed by SCOPUS**)

### Proceedings/Conference

1. Zaris I.M.Y., Dalila M.S.\*, Nasarudin A, Md Pauzi A. “Analysis on The Effect of Distribution Capacitors Operation Towards Total Harmonic Distortions (THD) in Distribution Network Test System.” 6th Conference On Emerging Energy & Process Technology. November 2017,pp. 1-5
2. Z. I. M. Yassin, D. M. Said , N. Ahmad, N. Rosmin and F.Salim. “Review on Energy Saving Analysis of Harmonic Suppression in a Distribution Network.” Conference on Emerging Energy and Process Technology (CONCEPT2015) 15-16 December 2015.